

Analytical Results for Hard-Scattering Production of Heavy Quarks

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1. Introduction
2. $d\sigma(pp \rightarrow c\bar{c}X) / dy_c c_T dc_T dy_{\bar{c}} \bar{c}_T d\bar{c}_T$
3. $d\sigma(pp \rightarrow c\bar{c}X) / d\Delta\phi d\Delta y$
4. $d\sigma(pp \rightarrow cX) / dy_c c_T dc_T$
5. Conclusion

Why study analytical formulas for heavy quark production in pp collisions

- Knowledge of heavy quark production in pp collisions provide insight to guide our intuition
- Analytical formulas summarize important features and factors in the collision process
- Similar analysis in light hadron production lead to new insights and new results

The log-log plot of σ_{inv} and c_T (jet)

(i) in the lower c_T region,

the slope gives n ,

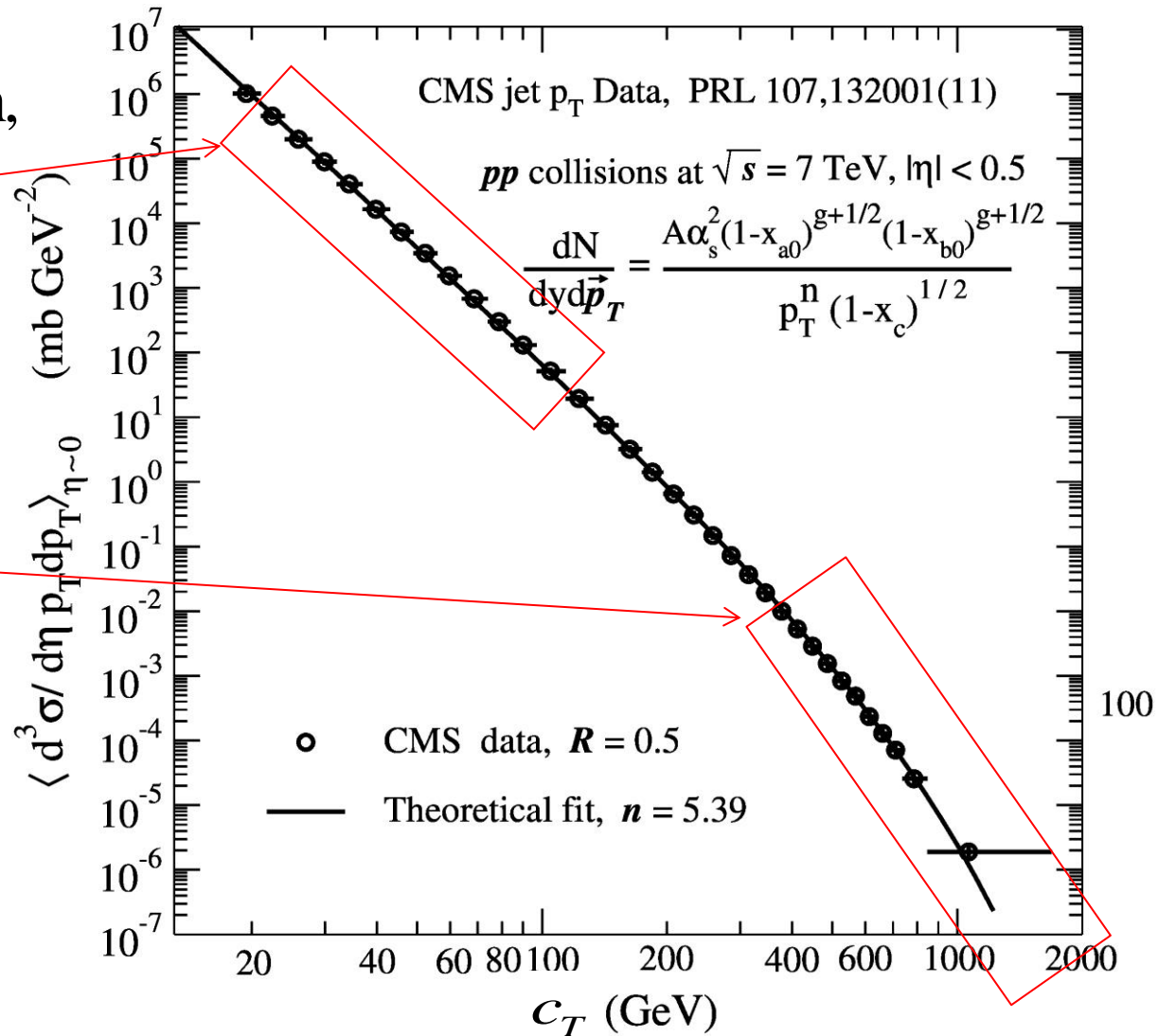
$$\frac{d(\ln \sigma_{\text{inv}})}{d(\ln c_T)} = -n,$$

(ii) in the very high c_T

region, the bending of

the curve gives g ,

$$\frac{d^2(\ln \sigma_{\text{inv}})}{d(\ln c_T)^2} \approx g.$$



Tsallis distribution can describe LHC p_T distributions

Tsallis distribution

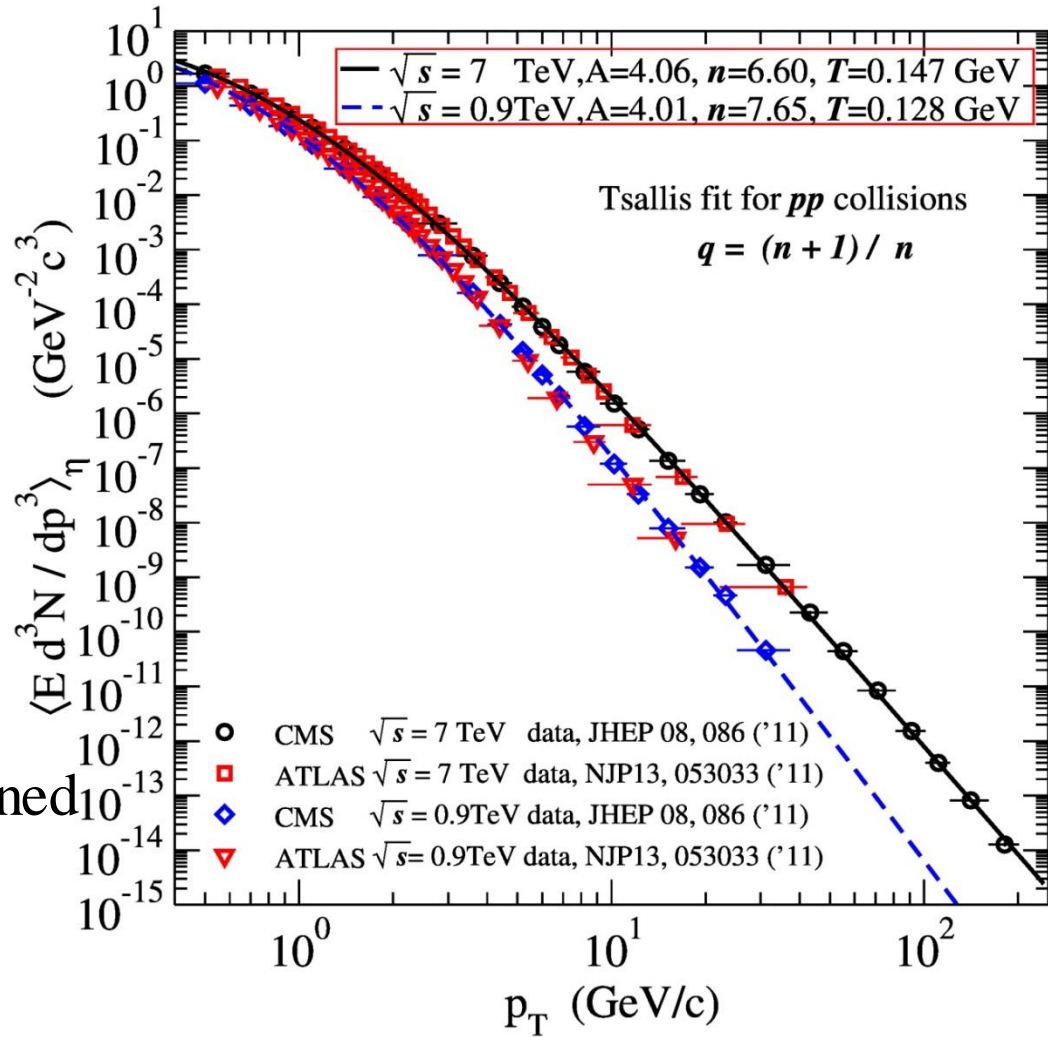
$$E \frac{d\sigma}{d^3 p} = \frac{A}{\left(1 + \frac{m_T - m}{nT}\right)^n}$$

$$m_T = \sqrt{m_\pi^2 + p_T^2}$$

can describe the hadron p_T
spectra in pp collisions at
LHC in the central rapidity region.

Good Tsallis fits have been obtained

$$\begin{cases} \text{for } \sqrt{s} = 7 \text{ TeV, } n = 6.60 \\ \text{for } \sqrt{s} = 0.9 \text{ TeV, } n = 7.65 \end{cases}$$



Wong and Wilk, ActaPhysPol.B43,2047(2012)

In terms of analytical expressions for the hard scattering integral, we provide evidences that

hadron production at $\eta \approx 0$ in high-energy pp and $\bar{p}p$ collisions is dominated by hard scattering over essentially the whole p_T region

C. Y. Wong, G. Wilk, Acta Phys. Pol. B 43, 2047 (2012)

C. Y. Wong, G. Wilk, Phys. Rev. D87, 114007 (2013)

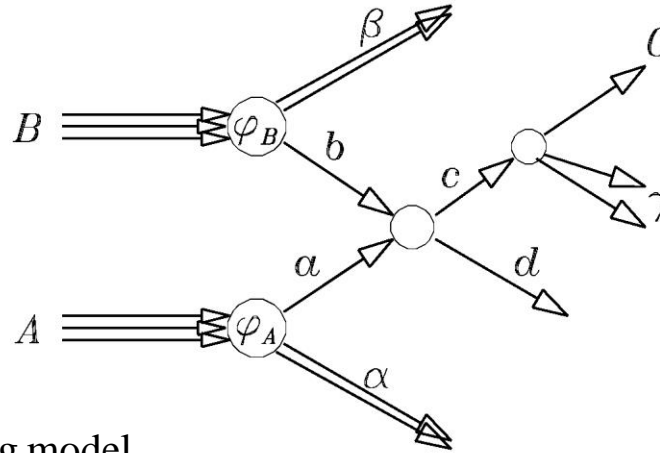
C. Y. Wong, G. Wilk, arXiv:1309.7330

C. Y. Wong, G. Wilk, L. J. L. Cirto, and C. Tsallis; EPJ Web of Conf.90, 04002 (2015)

L.J. L. Cirto, C. Tsallis, C.Y. Wong, G. Wilk, arXiv:1409.3278

C. Y. Wong, G. Wilk, L.J.L. Cirto, C. Tsallis, Phys. Rev. D91, 114027 (2015)

Relativistic hard-scattering model



Cross section in the hard - scattering model

$$d\sigma(AB \rightarrow c\bar{c}X) = \sum_{ab} K_{ab} \int dx_a d\vec{a}_T dx_b d\vec{b}_T G_{a/A}(x_a, \vec{a}_T) G_{b/B}(x_b, \vec{b}_T) d\sigma(ab \rightarrow c\bar{c})$$

where K_{ab} is the K - factor.

$$d\sigma(ab \rightarrow c\bar{c}) = \frac{\hat{s}}{2\pi} \frac{d\sigma(ab \rightarrow c\bar{c})}{dt} \frac{d^3c}{E_c} \frac{d^3\bar{c}}{E_{\bar{c}}} \delta^4(a+b-c-\bar{c}),$$

Therefore,

$$\frac{E_c E_{\bar{c}} d\sigma(AB \rightarrow c\bar{c}X)}{d^3c d^3\bar{c}} = \sum_{ab} K_{ab} \int dx_a d\vec{a}_T dx_b d\vec{b}_T G_{a/A}(x_a, \vec{a}_T) G_{b/B}(x_b, \vec{b}_T) \frac{\hat{s}}{2\pi} \frac{d\sigma(ab \rightarrow c\bar{c})}{dt} \delta^4(a+b-c-\bar{c}).$$

$$\frac{d\sigma(AB \rightarrow c\bar{c}X)}{dy_c d\vec{c}_T dy_{\bar{c}} d\vec{v}_T} = \sum_{ab} K_{ab} \int dx_a d\vec{a}_T dx_b d\vec{b}_T G_{a/A}(x_a, \vec{a}_T) G_{b/B}(x_b, \vec{b}_T) \frac{\hat{s}}{2\pi} \frac{d\sigma(ab \rightarrow c\bar{c})}{dt} \delta^4(a+b-c-\bar{c}).$$

$$\hat{s} = (a+b)^2 = x_a x_b s, \quad s = (A+B)^2.$$

Relativistic hard-scattering model

Assume $G_{a/A}(x_a, \vec{a}_T) = G_{a/A}(x_a) \frac{e^{-\vec{a}_T^2/2\sigma^2}}{2\pi\sigma^2}$ and weak dependence of $d\sigma(ab \rightarrow c\bar{c})/dt$ on \vec{a}_T and \vec{b}_T , then

$$\int d\vec{a}_T d\vec{b}_T \frac{e^{-\frac{\vec{a}_T^2 + \vec{b}_T^2}{2\sigma^2}}}{(2\pi\sigma^2)^2} \delta^2(\vec{a}_T + \vec{b}_T - \vec{c}_T - (\bar{c})_T) = \frac{e^{-\frac{(\vec{c}_T + (\bar{c})_T)^2}{4\sigma^2}}}{2(2\pi\sigma^2)^2}$$

$$\frac{d\sigma(AB \rightarrow c\bar{c}X)}{dy_c d\vec{c}_T dy_{\bar{c}} d\vec{c}_T} = \sum_{ab} K_{ab} \int dx_a dx_b G_{a/A}(x_a) G_{b/B}(x_b) \frac{\hat{s}}{2\pi} \frac{d\sigma(ab \rightarrow c\bar{c})}{dt} \frac{e^{-\frac{(\vec{c}_T + (\bar{c})_T)^2}{4\sigma^2}}}{2(2\pi\sigma^2)^2} \delta(a_0 + b_0 - c_0 - \bar{c}_0) \delta(a_z + b_z - c_z - \bar{c}_z)$$

$$\delta(a_0 + b_0 - c_0 - \bar{c}_0) \delta(a_z + b_z - c_z - \bar{c}_z) = \frac{1}{s} \delta(x_a - x_{a0}) \delta(x_b - x_{b0}),$$

$$s = (A+B)^2, \quad \hat{s} = (a+b)^2, \quad \hat{s} = x_a x_b s$$

$$\frac{d\sigma(AB \rightarrow c\bar{c}X)}{dy_c d\vec{c}_T dy_{\bar{c}} d\vec{c}_T} = \sum_{ab} K_{ab} [x_{a0} G_{a/A}(x_{a0})] [x_{b0} G_{b/B}(x_{b0})] \frac{1}{2\pi} \frac{d\sigma(ab \rightarrow c\bar{c})}{dt} \frac{e^{-\frac{(\vec{c}_T + (\bar{c})_T)^2}{4\sigma^2}}}{2(2\pi\sigma^2)^2}$$

$$x_{a0} G_{a/A}(x_{a0}) \propto (1-x_{a0})^{g_a}, \quad x_{b0} G_{b/B}(x_{b0}) \propto (1-x_{b0})^{g_b},$$

$$x_{a0} = \frac{m_{cT}}{\sqrt{s}} 2 \cosh \bar{y} \exp\{\Delta y/2\}, \quad x_{b0} = \frac{m_{cT}}{\sqrt{s}} 2 \cosh \bar{y} \exp\{-\Delta y/2\}$$

Relativistic hard-scattering model

$$\delta(a_0 + b_0 - c_0 - \bar{c}_0) \delta(a_z + b_z - c_z - \bar{c}_z) = \frac{1}{\hat{s}} \delta(x_a - x_{a0}) \delta(x_b - x_{b0})$$

$$x_{a0} = \frac{m_{cT}}{\sqrt{s}} 2(\cosh Y) e^{\Delta y/2}, \quad x_{b0} = \frac{m_{cT}}{\sqrt{s}} 2(\cosh Y) e^{-\Delta y/2},$$

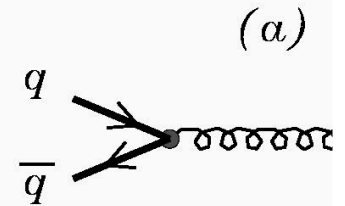
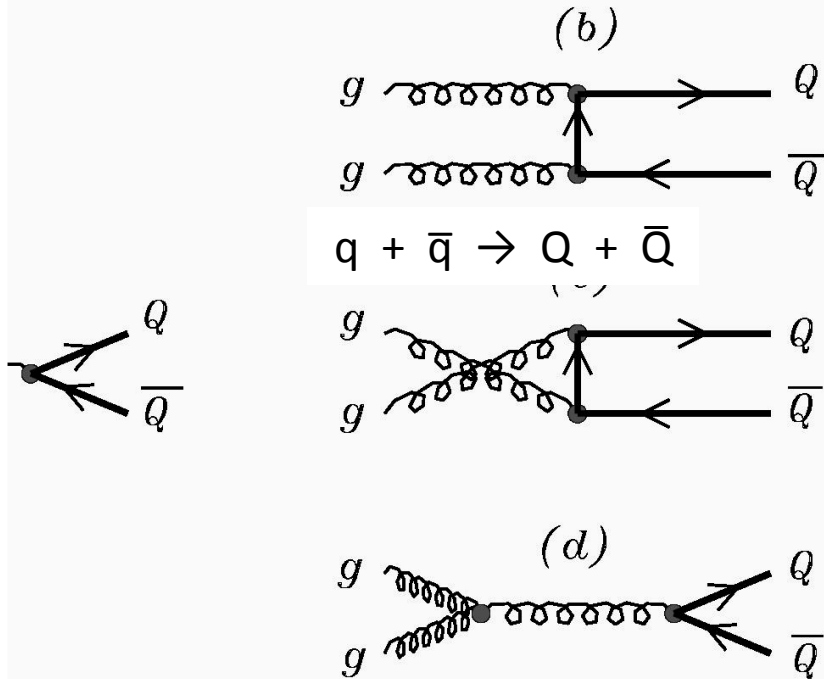
$$Y = \frac{y_c + y_{\bar{c}}}{2}, \quad \Delta y = y_c - y_{\bar{c}}$$

$$\frac{d\sigma(AB \rightarrow c\bar{c}X)}{dy_c d\vec{c}_T dy_{\bar{c}} d\vec{c}_T} = \sum_{ab} K_{ab} x_{a0} G_{a/A}(x_{a0}) x_{b0} G_{b/B}(x_{b0}) \frac{1}{2\pi} \frac{d\sigma(ab \rightarrow c\bar{c})}{dt} \Big|_{x_{a0}, x_{b0}} \frac{e^{-\frac{(\vec{c}_T + \vec{c}_T)^2}{4\sigma^2}}}{2(2\pi\sigma^2)^2}$$

$$\frac{d\sigma(AB \rightarrow c\bar{c}X)}{dy_c d\vec{c}_T dy_{\bar{c}} d\vec{c}_T} \propto K_{ab} (1-x_{a0})^{g_a} (1-x_{b0})^{g_b} \frac{1}{2\pi} \frac{d\sigma(ab \rightarrow c\bar{c})}{dt} \Big|_{x_{a0}, x_{b0}} \frac{e^{-\frac{(\vec{c}_T + \vec{c}_T)^2}{4\sigma^2}}}{2(2\pi\sigma^2)^2}$$

Diagrams for heavy quark production

$$g + \bar{g} \rightarrow Q + \bar{Q}$$



The dominant process is
 $g + \bar{g} \rightarrow Q + \bar{Q}$

What is $d\sigma(gg \rightarrow c\bar{c})/dt$?

Gluck, Owen, Reya gives (PRD17,2324(1978))

$$\frac{d\sigma(gg \rightarrow Q\bar{Q})}{dt} = \frac{\pi\alpha^2}{64s^2} \left[12M_{ss} + \frac{16}{3}M_{tt} + \frac{16}{3}M_{uu} + 6M_{st} + 6M_{su} - \frac{2}{3}M_{tu} \right]$$

$$M_{ss} = \frac{4}{s^2}(t - M^2)(u - M^2)$$

$$M_{tt} = \frac{-2}{(t - M^2)^2} \left[4M^4 - (t - M^2)(u - M^2) + 2M^2(t - M^2) \right]$$

$$M_{uu} = \frac{-2}{(u - M^2)^2} \left[4M^4 - (u - M^2)(t - M^2) + 2M^2(u - M^2) \right]$$

$$M_{st} = \frac{4}{s(t - M^2)} \left[M^4 - t(s + t) \right]$$

$$M_{su} = \frac{4}{s(u - M^2)} \left[M^4 - u(s + u) \right]$$

$$M_{tu} = \frac{-4M^2}{(t - M^2)(u - M^2)} \left[4M^2 + (t - M^2) + (u - M^2) \right]$$

What is $\frac{d\sigma(gg \rightarrow c\bar{c})}{dt}$?

$$\frac{d\sigma(gg \rightarrow c\bar{c})}{dt} = \frac{\pi\alpha_s^2}{256 m_{cT}^4 \cosh^4 \bar{y}} \left\{ \frac{12}{\cosh^2 \bar{y}} + \frac{64}{3} \cosh 2\bar{y} - 24 \right. \\ \left. + \frac{m_c^2}{m_{cT}^2} \left(\frac{64}{3} + \frac{24 \sinh^2 \bar{y}}{\cosh^2 \bar{y}} - \frac{8}{3} \right) \right. \\ \left. + \frac{m_c^4}{m_{cT}^4} \left(-\frac{64}{3} \frac{\cosh 2\bar{y}}{\cosh^2 \bar{y}} + \frac{8}{3} \frac{1}{\cosh^2 \bar{y}} \right) \right\}$$

$\frac{d\sigma(gg \rightarrow c\bar{c})}{dt}$ depends on $m_c, m_{cT} = \sqrt{m_c^2 + c_T^2}$, and \bar{y} .

$$\frac{d\sigma(AB \rightarrow c\bar{c}X)}{dy_c d\bar{c}_T dy_v d\bar{c}_T} = \sum_{ab} K_{ab} x_{a0} G_{a/A}(x_{a0}) x_{b0} G_{b/B}(x_{b0}) \frac{1}{2\pi} \frac{d\sigma(ab \rightarrow c\bar{c})}{dt} \Big|_{x_{a0}, x_{b0}} \frac{e^{-\frac{(\bar{c}_T + \bar{c}_T)^2}{4\sigma^2}}}{2(2\pi\sigma^2)^2}$$

Two particle correlation for the production of a $c\bar{c}$ pair :

$$\frac{d\sigma(AB \rightarrow c\bar{c}X)}{dy_c d\bar{c}_T dy_v d\bar{c}_T} \sim AK_{ab} (1-x_{a0})^{g_a} (1-x_{b0})^{g_b} e^{-\frac{(\bar{c}_T + \bar{c}_T)^2}{4\sigma^2}} \\ \times \frac{\pi\alpha_s^2}{256 m_{cT}^4 \cosh^4 \bar{y}} \left\{ \frac{12}{\cosh^2 \bar{y}} + \frac{64}{3} \cosh 2\bar{y} - 24 + \frac{m_c^2}{m_{cT}^2} \left(\frac{64}{3} + \frac{24 \sinh^2 \bar{y}}{\cosh^2 \bar{y}} - \frac{8}{3} \right) + \frac{m_c^4}{m_{cT}^4} \left(-\frac{64}{3} \frac{\cosh 2\bar{y}}{\cosh^2 \bar{y}} + \frac{8}{3} \frac{1}{\cosh^2 \bar{y}} \right) \right\}$$

$$x_{a0} = \frac{m_{cT}}{\sqrt{s}} 2(\cosh \bar{y}) e^{\Delta y/2}, \quad x_{b0} = \frac{m_{cT}}{\sqrt{s}} 2(\cosh \bar{y}) e^{-\Delta y/2},$$

$$\bar{y} = \frac{y_c + y_v}{2}, \quad \Delta y = y_c - y_d$$

This is the formula for the away-side ridge for the production of a $c\bar{c}$ pair.

C- \bar{C} Angular correlations

$$\frac{d\sigma(AB \rightarrow c\bar{c}X)}{dy_c d\bar{c}_T dy_v d\bar{c}_T} = \sum_{ab} K_{ab} x_{a0} G_{a/A}(x_{a0}) x_{b0} G_{b/B}(x_{b0}) \frac{1}{2\pi} \frac{d\sigma(ab \rightarrow c\bar{c})}{dt} \Big|_{x_{a0}, x_{b0}} e^{-\frac{(\bar{c}_T + \bar{c}_T)^2}{4\sigma^2}} \frac{1}{2(2\pi\sigma^2)^2}$$

Change variables: $(y_c, y_d) \rightarrow (\bar{y}, \Delta y)$

$$\bar{y} = \frac{y_c + y_d}{2}, \quad \Delta y = y_c - y_d$$

$$y_c = \bar{y} + \frac{\Delta y}{2}, \quad y_d = \bar{y} - \frac{\Delta y}{2},$$

$$d\bar{c}_T = c_T dc_T d\phi_c, \quad d\bar{c}_T = \bar{c}_T d\bar{c}_T d\phi_{\bar{c}}$$

$$d\phi_c d\phi_{\bar{c}} = d\phi_c d\Delta\phi, \quad \Delta\phi = \phi_{\bar{c}} - \phi_c$$

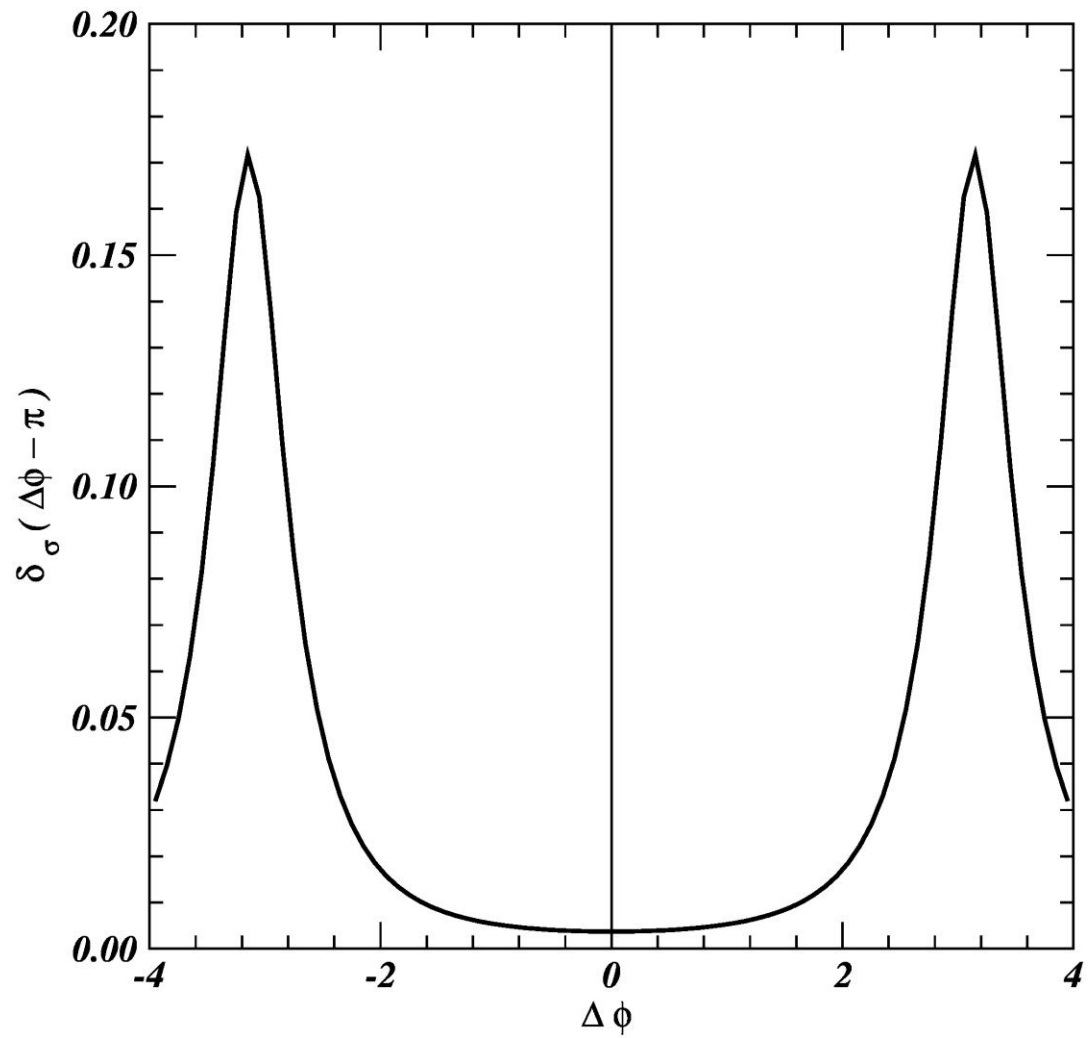
$$\frac{d\sigma(AB \rightarrow c\bar{c}X)}{d\bar{y} d\Delta y c_T d\bar{c}_T \bar{c}_T d\bar{c}_T} \sim AK_{ab} (1-x_{a0})^{g_a} (1-x_{b0})^{g_b} \frac{1}{2\pi} \frac{d\sigma(ab \rightarrow c\bar{c})}{dt} \Big|_{x_{a0}, x_{b0}} e^{-\frac{(\bar{c}_T + (\bar{c})_T)^2}{4\sigma^2}}$$

$$\begin{aligned} \frac{d\sigma(AB \rightarrow c\bar{c}X)}{d\Delta\phi d\Delta y} &\sim A \int d\bar{y} c_T dc_T d\phi_c \bar{c}_T d\bar{c}_T K_{ab} (1-x_{a0})^{g_a} (1-x_{b0})^{g_b} e^{-\frac{(\bar{c}_T + (\bar{c})_T)^2}{4\sigma^2}} \\ &\times \frac{\pi\alpha^2}{256 m_{cT}^4 \cosh^4 \bar{y}} \left\{ \frac{12}{\cosh^2 \bar{y}} + \frac{64}{3} \cosh 2\bar{y} - 24 + \frac{m_c^2}{m_{cT}^2} \left(\frac{64}{3} + \frac{24 \sinh^2 \bar{y}}{\cosh^2 \bar{y}} - \frac{8}{3} \right) + \frac{m_c^4}{m_{cT}^4} \left(-\frac{64}{3} \frac{\cosh 2\bar{y}}{\cosh^2 \bar{y}} + \frac{8}{3} \frac{1}{\cosh^2 \bar{y}} \right) \right\} \\ &\sim A \int d\bar{y} c_T dc_T d\phi_c \bar{c}_T d\bar{c}_T K_{ab} (1-x_{a0})^{g_a} (1-x_{b0})^{g_b} e^{-\frac{(\bar{c}_T + (\bar{c})_T)^2}{4\sigma^2}} \frac{\pi\alpha^2}{256 m_{cT}^4 \cosh^4 \bar{y}} \left\{ \frac{12}{\cosh^2 \bar{y}} + \frac{64}{3} \cosh 2\bar{y} - 24 + \mathcal{O}\left(\frac{m_c^2}{m_{cT}^2}\right) \right\} \end{aligned}$$

After the integration over c_T, ϕ_c, \bar{c}_T

$$\frac{d\sigma(AB \rightarrow c\bar{c}X)}{d\Delta\phi d\Delta y} \sim A K_{ab} (1-x_{a0})^{g_a} (1-x_{b0})^{g_b} \delta_\sigma(\Delta\phi - \pi) d\bar{y} \frac{\pi\alpha^2}{256 \cosh^4 \bar{y}} \left\{ \frac{12}{\cosh^2 \bar{y}} + \frac{64}{3} \cosh 2\bar{y} - 24 + \mathcal{O}\left(\frac{m_c^2}{m_{cT}^2}\right) \right\}$$

Back-to-back correlation with a Δy ridge on the away side at $\Delta\phi \sim \pi$



Heavy-quark production cross section

$$\frac{E_c E_{\bar{c}} d\sigma(AB \rightarrow c\bar{c}X)}{d^3c d^3\bar{c}} = \sum_{ab} K_{ab} \int dx_a d\bar{a}_T dx_b d\bar{b}_T G_{a/A}(x_a, \bar{a}_T) G_{b/B}(x_b, \bar{b}_T) \frac{\hat{s}}{2\pi} \frac{d\sigma(ab \rightarrow c\bar{c})}{dt} \delta^4(a+b-c-\bar{c}).$$

$$\frac{E_c d\sigma(AB \rightarrow cX)}{d^3c} = \sum_{ab} K_{ab} \int \frac{d^4\bar{c}}{E_{\bar{c}}} dx_a d\bar{a}_T dx_b d\bar{b}_T G_{a/A}(x_a, \bar{a}_T) G_{b/B}(x_b, \bar{b}_T) \frac{\hat{s}}{2\pi} \frac{d\sigma(ab \rightarrow c\bar{c})}{dt} \delta^4(a+b-c-\bar{c}).$$

$$= \sum_{ab} K_{ab} \int dx_a dx_b G_{a/A}(x_a) G_{b/B}(x_b) \frac{e^{-\frac{(\bar{c}_T + \bar{c}_T)^2}{4\sigma^2}}}{2(2\pi\sigma^2)^2} \frac{\hat{s}}{\pi} \frac{d\sigma(ab \rightarrow c\bar{c})}{dt} \delta(\hat{s} + \hat{t} + \hat{u} - m_a^2 - m_b^2 - m_c^2 - m_{\bar{c}}^2)$$

The delta function can be transformed into

$$\delta(\hat{s} + \hat{t} + \hat{u} - m_a^2 - m_b^2 - m_c^2 - m_{\bar{c}}^2) = \frac{\delta(x_a - x_b)}{s \left(x_b - \frac{m_{cT}^2}{x_c s} \right)}$$

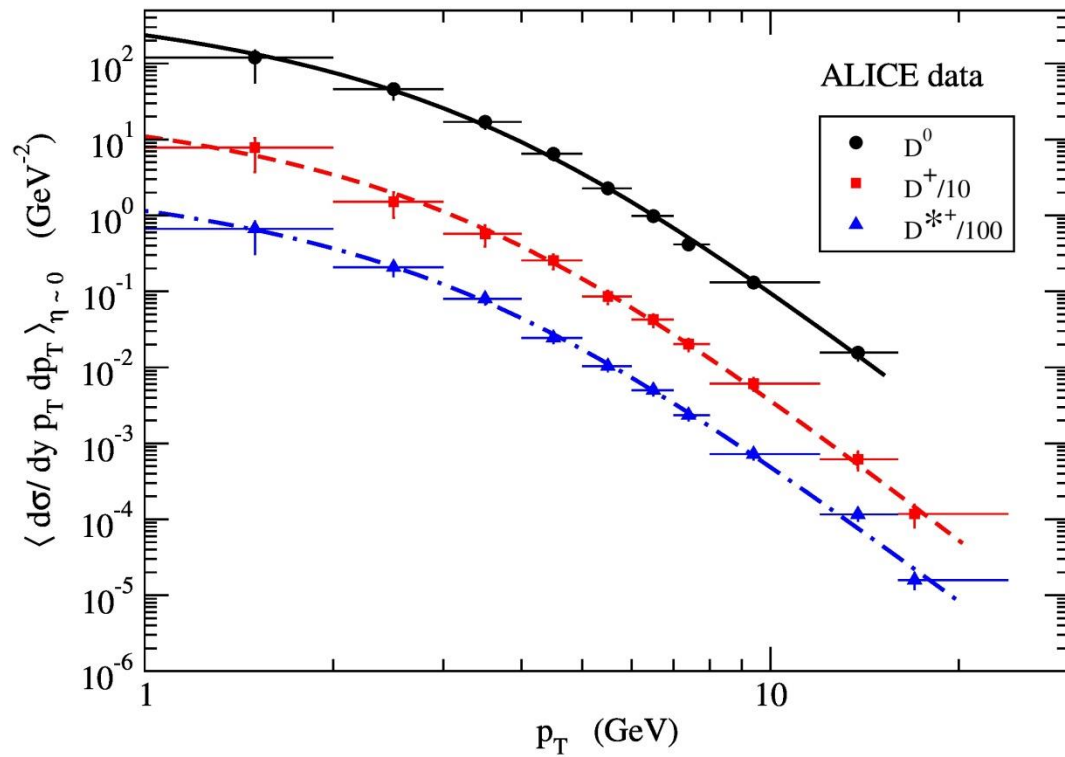
The other integral can be carried out by the saddle point method. We obtain at $y_c \approx 0$

$$\frac{E_c d\sigma(AB \rightarrow cX)}{d^3c} = AK_{ab} (1-x_{a0})^{g_a+1/2} (1-x_{b0})^{g_b+1/2} \frac{1}{\sqrt{x_c}} \frac{d\sigma(ab \rightarrow c\bar{c})}{dt}$$

where $x_{a0} = x_{b0} = 2x_c$, $x_c = \frac{(m_c^2 + c_T^2)^{1/2}}{\sqrt{s}}$

$$\frac{E_c d\sigma(AB \rightarrow cX)}{d^3c} \propto \frac{K_{ab} \alpha_s^2}{m_{cT}^4 \cosh^4 \bar{y}} \left\{ \frac{12}{\cosh^2 \bar{y}} + \frac{64}{3} \cosh 2\bar{y} - 24 + \frac{m_c^2}{m_{cT}^2} \left(\frac{64}{3} + \frac{24 \sinh^2 \bar{y}}{\cosh^2 \bar{y}} - \frac{8}{3} \right) + \frac{m_c^4}{m_{cT}^4} \left(-\frac{64}{3} \frac{\cosh 2\bar{y}}{\cosh^2 \bar{y}} + \frac{8}{3} \frac{1}{\cosh^2 \bar{y}} \right) \right\}$$

The cross section is a mixture of $1/m_{cT}^4$, $1/m_{cT}^6$, $1/m_{cT}^8$.



$$d\sigma/dy p_T dp_T = A/(1+p_T^2/m_0^2)^n / 2$$

	A	n	$m_0(\text{GeV})$
D0	1600	5.8	3.5
D+	780	5.9	3.5
D*+	808	5.7	3.5

K-factor

$$K = \frac{2\pi f(v)}{1 - \exp\{-2\pi f(v)\}} (1 + (C_F \alpha_s)^2),$$

$$f(v) = C_F \alpha_s \left[\frac{1}{v} - v \left(1 - \frac{4\pi}{3}\right) \right]$$

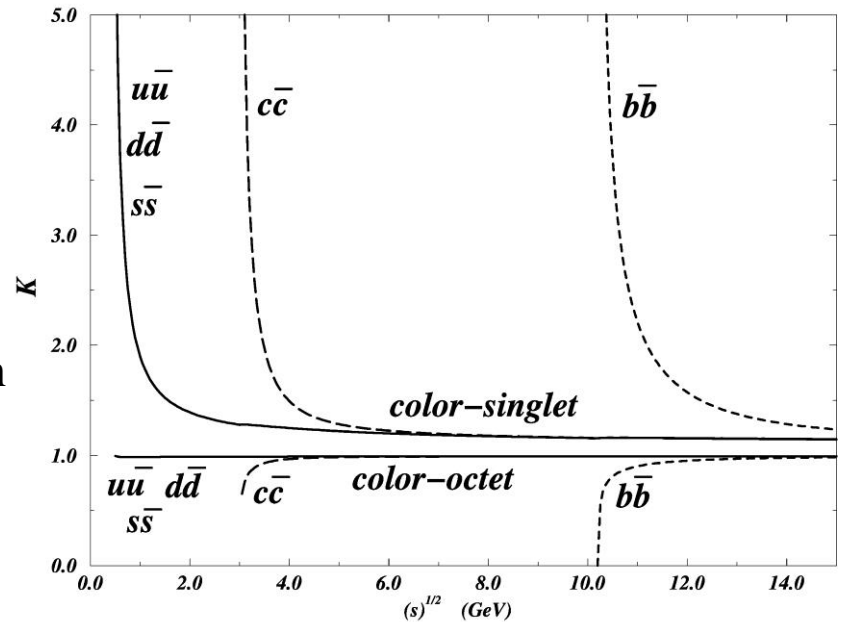
$$C_F = \begin{cases} 4/3 & \text{for color singlet} \\ -1/6 & \text{for color octet} \end{cases}$$

For $c\bar{c}$ final - state interaction by gluon fusion

$$\frac{(\text{color - octet})}{(\text{color - singlet})} = \frac{(d^{abc})^2}{(\delta^{ab})^2} = \frac{5}{2}$$

$$K_{gg} = [5K(\text{octet}) + 2K(\text{singlet})] / 2$$

Chatterjee+Wong, PRC51,2125(1995)



Conclusion

Analytical formulas have been obtained for various heavy-quark production cross sections. They will facilitate future comparisons and physical understanding of the production process.