

Effect of Coriolis force on Electrical Conductivity: A Non-Relativistic Description

Ashutosh Dwibedi

Collaborators- Cho Win Aung, Jayanta Dey, Sabyasachi Ghosh

Department of Physics
Indian Institute of Technology Bhilai

ashutoshd@iitbhilai.ac.in

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Introduction

- In off-central or peripheral HIC, a huge magnetic field as well as angular velocity can be created [2, 3].

F. Becattini, F. Piccinini, and J. Rizzo Phys. Rev. C 77, 024906

$\Rightarrow \sqrt{s_{NN}} = 200\text{GeV}$ and $L_0 = 5 \times 10^5 \hbar$ at an impact parameter $b = 5 \text{ fm}$.

Even 0.01% angular momentum(ang. mom.) transfer $\Rightarrow 10^3 \hbar$ ang. mom. of QGP

- This implies QGP must have a high average vorticity.

Question:

- Can the transport coefficients of QGP be modified in the presence of rotation?

In this presentation, we will answer this question in a non-relativistic setup.

Formalism

Non-Relativistic Frame Transformation:

Operator connection from **inertial** to **rotating frame**:

$$\left(\frac{d}{dt} \right) \equiv \left(\frac{d}{dt} \right)' + \vec{\Omega} \times . \quad (1)$$

Using the Eq. (1) one gets the following important identity:

$$\vec{a} = \vec{a}' + 2(\vec{\Omega} \times \vec{v}') + \vec{\Omega} \times (\vec{\Omega} \times \vec{r}') + \dot{\vec{\Omega}} \times \vec{r}', \quad (2)$$

Coriolis force = $-2m(\vec{\Omega} \times \vec{v}')$,

Centrifugal force = $-m \vec{\Omega} \times (\vec{\Omega} \times \vec{r}')$,

Euler force = $-m(\dot{\vec{\Omega}} \times \vec{r}')$.

Our set-up:

A non-relativistic single-component fluid rotating with angular velocity $\vec{\Omega} = \text{const.}$

$\vec{\Omega} = \text{const.}$ makes Euler force zero.

Formalism(contd...)

- In our analysis, we will ignore the centrifugal force as if it were not there(added in the backup slides).

$$\vec{F}_{Lor} = q(\vec{v} \times \vec{B}) \text{ and } \vec{F}_{Cor} = 2m(\vec{v} \times \vec{\Omega})$$

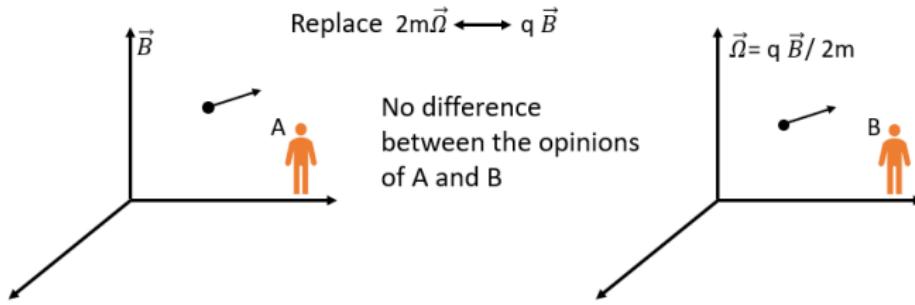


Figure: Motion under finite magnetic fields and rotation

Formalism(contd...)

- To see the statistical effects \Rightarrow Boltzmann Transport Equation(BTE)
- Out of eqbm. \Rightarrow transport coefficients of the medium
- Navier-Stokes Theory \Rightarrow Dissipative flows = Transport coefficients \times Driving force
- Our Interest: Charge current : $J_i = \sigma_{ij} \tilde{E}_j$
- Kinetic theory definition of j_i :

$$j_i = q g \int \frac{d^3 \vec{p}}{(2\pi)^3} v_i \delta f , \quad (3)$$

- Assumption: Total distribution (f) = local eqbm. distribution (f_0) + deviation δf ,

$$f^0 = \frac{1}{\exp \left\{ \frac{E - \mu(\vec{r}, t) - \vec{u}(\vec{r}, t) \cdot \vec{p}}{T(\vec{r}, t)} \right\} + 1} , \quad (4)$$

- f obeys the Boltzmann Transport Equation(BTE).

Formalism(contd...)

- BTE in Relaxation Time Approximation (RTA) :

$$\frac{\partial f}{\partial t} + \vec{v} \cdot \frac{\partial f}{\partial \vec{r}} + \vec{F}_{\text{ext}} \cdot \frac{\partial f}{\partial \vec{p}} = -\frac{\delta f}{\tau_c}. \quad (5)$$

- External forces in different scenarios are different.

- Our BTE will be:

$$\frac{\partial f}{\partial t} + \vec{v} \cdot \frac{\partial f}{\partial \vec{r}} + [q\vec{E} + 2m(\vec{v} \times \vec{\Omega})] \cdot \frac{\partial f}{\partial \vec{p}} = -\frac{\delta f}{\tau_c}. \quad (6)$$

- We ignore terms: $\frac{\partial u_i}{\partial x_j}$, $\frac{\partial T}{\partial x_i}$, $\frac{\partial \mu}{\partial x_i}$

Eq (6) will become,

$$[q\vec{E} + 2m(\vec{v} \times \vec{\Omega})] \cdot \frac{\partial f^0 + \delta f}{\partial \vec{p}} = -\frac{\delta f}{\tau_c}. \quad (7)$$

- In Eq. (7) keeping terms of order δf :

$$\Rightarrow \frac{\partial f^0}{\partial E} \vec{v} \cdot (q\vec{E}) + 2m(\vec{v} \times \vec{\Omega}) \cdot \frac{\partial \delta f}{\partial \vec{p}} = -\frac{\delta f}{\tau_c}. \quad (8)$$

Formalism(contd...)

Solving Eq. (8) for δf

- Ansatz: $\delta f = -\vec{p} \cdot \vec{F}\left(\frac{\partial f^0}{\partial E}\right)$

$$\vec{F} = \alpha \hat{e} + \beta \hat{\omega} + \gamma (\hat{e} \times \hat{\omega})$$

$$\tilde{E} = \tilde{E} \hat{e}, \quad \tilde{\Omega} = \Omega \hat{\omega}$$

α, β, γ are unknown constants

- Substituting δf in Eq. (8):

$$\left(\frac{q\tilde{E}}{m} - 2\Omega\gamma \right) \hat{e} + 2\gamma\Omega(\hat{\omega} \cdot \hat{e})\hat{\omega} + 2\alpha\Omega(\hat{e} \times \hat{\omega}) = \frac{\alpha}{\tau_c} \hat{e} + \frac{\beta}{\tau_c} \hat{\omega} + \frac{\gamma}{\tau_c} (\hat{e} \times \hat{\omega}). \quad (9)$$

- Following linear eq.s to solve:

$$\frac{q\tilde{E}}{m} - \frac{\gamma}{\tau_\Omega} = \frac{\alpha}{\tau_c}, \quad \frac{\gamma}{\tau_\Omega} (\hat{\omega} \cdot \hat{e}) = \frac{\beta}{\tau_c}, \quad \frac{\alpha}{\tau_\Omega} = \frac{\gamma}{\tau_c}, \quad (10)$$

$$\tau_\Omega \equiv \frac{1}{2\Omega}.$$

Formallism(contd...)

Eq. 10 can be simplified as:

$$\alpha = \frac{\tau_c \left(\frac{q\tilde{E}}{m} \right)}{1 + \left(\frac{\tau_c}{\tau_\Omega} \right)^2}, \quad \gamma = \frac{\tau_c \left(\frac{\tau_c}{\tau_\Omega} \right) \left(\frac{q\tilde{E}}{m} \right)}{1 + \left(\frac{\tau_c}{\tau_\Omega} \right)^2}, \quad \beta = \frac{\tau_c \left(\frac{\tau_c}{\tau_\Omega} \right)^2 (\hat{\omega} \cdot \hat{\mathbf{e}}) \left(\frac{q\tilde{E}}{m} \right)}{1 + \left(\frac{\tau_c}{\tau_\Omega} \right)^2}. \quad (11)$$

- See two time scales τ_c and τ_Ω (more about this later).

The Eqs. (11) can be used to get the expression of δf as:

$$\begin{aligned} \delta f &= -\vec{p} \cdot \vec{F} \frac{\partial f^0}{\partial E} \\ &= -\frac{\partial f^0}{\partial E} m \vec{v} \cdot (\alpha \hat{\mathbf{e}} + \beta \hat{\omega} + \gamma (\hat{\mathbf{e}} \times \hat{\omega})) \\ &= -\frac{\partial f^0}{\partial E} \left[\frac{q \tau_c \tilde{E}}{1 + \left(\frac{\tau_c}{\tau_\Omega} \right)^2} \hat{\mathbf{e}} \cdot \vec{v} + \frac{\tau_c \left(\frac{\tau_c}{\tau_\Omega} \right)^2 (\hat{\omega} \cdot \hat{\mathbf{e}}) q \tilde{E}}{1 + \left(\frac{\tau_c}{\tau_\Omega} \right)^2} \hat{\omega} \cdot \vec{v} + \frac{\tau_c \left(\frac{\tau_c}{\tau_\Omega} \right) q \tilde{E}}{1 + \left(\frac{\tau_c}{\tau_\Omega} \right)^2} (\hat{\mathbf{e}} \times \hat{\omega}) \cdot \vec{v} \right] \\ &= -\frac{\partial f^0}{\partial E} \left(\frac{q \tau_c}{1 + \left(\frac{\tau_c}{\tau_\Omega} \right)^2} \right) \left[\delta_{jl} + \left(\frac{\tau_c}{\tau_\Omega} \right)^2 \omega_j \omega_l + \left(\frac{\tau_c}{\tau_\Omega} \right) \epsilon_{ljk} \omega_k \right] \tilde{E}_j v_l. \end{aligned} \quad (12)$$

Formalism(contd...)

Current density:

$$j_i = qg \int \frac{d^3 \vec{p}}{(2\pi)^3} v_i \frac{\partial f^0}{\partial E} \left(\frac{q\tau_c}{1 + \left(\frac{\tau_c}{\tau_\Omega}\right)^2} \right) \left[\delta_{ij} + \left(\frac{\tau_c}{\tau_\Omega}\right)^2 \omega_j \omega_i + \left(\frac{\tau_c}{\tau_\Omega}\right) \epsilon_{ijk} \omega_k \right] \tilde{E}_j v_i . \quad (13)$$

Final expression:

$$j_i = -q^2 g \int \frac{d^3 p}{(2\pi)^3} \frac{\partial f^0}{\partial E} \frac{v^2}{3} \left(\frac{\tau_c}{1 + \left(\frac{\tau_c}{\tau_\Omega}\right)^2} \right) \left[\delta_{ij} + \left(\frac{\tau_c}{\tau_\Omega}\right) \epsilon_{ijk} \omega_k \left(\frac{\tau_c}{\tau_\Omega}\right)^2 \omega_j \omega_i \right] \tilde{E}_j . \quad (14)$$

- Comparing Eq.(14) with $j_i = \sigma_{ij} \tilde{E}_j$

$$\sigma_{ij} = -gq^2 \int \frac{d^3 p}{(2\pi)^3} \frac{\partial f^0}{\partial E} \frac{v^2}{3} \left(\frac{\tau_c}{1 + \left(\frac{\tau_c}{\tau_\Omega}\right)^2} \right) \left[\delta_{ij} + \left(\frac{\tau_c}{\tau_\Omega}\right) \epsilon_{ijk} \omega_k \left(\frac{\tau_c}{\tau_\Omega}\right)^2 \omega_j \omega_i \right] . \quad (15)$$

We can re-express Eq. (15) as follows:

$$\sigma_{ij} = \sigma_0 \delta_{ij} + \sigma_1 \epsilon_{ijk} \omega_k + \sigma_2 \omega_i \omega_j , \text{ with } \sigma_n = \frac{gq^2}{T} \int \frac{d^3 p}{(2\pi)^3} \frac{\tau_c \left(\frac{\tau_c}{\tau_\Omega}\right)^n}{1 + \left(\frac{\tau_c}{\tau_\Omega}\right)^2} \times \frac{v^2}{3} f^0 (1 - f^0) . \quad (16)$$

$\sigma_0, \sigma_1, \sigma_2$ are scalars that make up the conductivity tensor.

Formalism(contd...)

- σ_n in terms of fermi functions: $\sigma_n = \frac{\sqrt{m\pi}gq^2}{2\pi^2\sqrt{2}} \frac{\tau_c \left(\frac{\tau_c}{\tau_\Omega}\right)^n}{1 + \left(\frac{\tau_c}{\tau_\Omega}\right)^2} T^{\frac{3}{2}} f_{3/2}(A)$, $A = e^{\mu/T}$.
- fermi functions: $f_j(A) = \frac{1}{\Gamma(j)} \int_0^\infty \frac{x^{j-1} dx}{A^{-1}e^x + 1}$
- Let's define the following:

$$\begin{aligned}\sigma_{||} &= \sigma_0 = \frac{g\sqrt{mq^2}}{(2\pi)^{3/2}} \tau_c T^{\frac{3}{2}} f_{3/2}(A), \\ \sigma_{\perp} &= \sigma_0 + \sigma_2 = \frac{g\sqrt{mq^2}}{(2\pi)^{3/2}} \frac{\tau_c}{1 + \left(\frac{\tau_c}{\tau_\Omega}\right)^2} T^{\frac{3}{2}} f_{3/2}(A), \\ \sigma_{\times} &= \sigma_1 = \frac{g\sqrt{mq^2}}{(2\pi)^{3/2}} \frac{\tau_c \left(\frac{\tau_c}{\tau_\Omega}\right)}{1 + \left(\frac{\tau_c}{\tau_\Omega}\right)^2} T^{\frac{3}{2}} f_{3/2}(A).\end{aligned}\tag{17}$$

Results and Discussion:

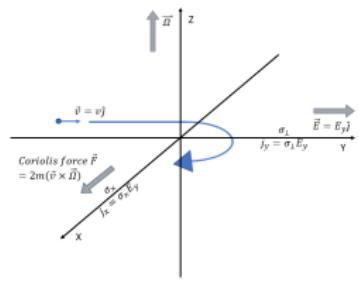


Figure: perpendicular conduction

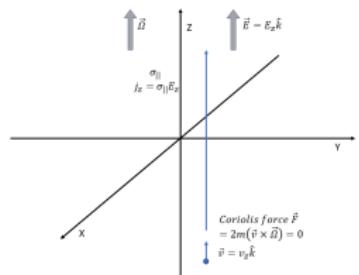


Figure: parallel conduction

For $\vec{\Omega} = \Omega\hat{k}$:

$$[\sigma] = \begin{pmatrix} \sigma_0 & \sigma_1 & 0 \\ -\sigma_1 & \sigma_0 & 0 \\ 0 & 0 & \sigma_0 + \sigma_2 \end{pmatrix}.$$

$\sigma_0 \equiv \sigma_{\perp} = \sigma_{yy} = \sigma_{xx}$, $\sigma_0 + \sigma_2 \equiv \sigma_{||} = \sigma_{zz}$,
and $\sigma_1 \equiv \sigma_x = \sigma_{xy}$

Non-Zero Coriolis force in XY-plane \Rightarrow
 $j_x = \sigma_{xy}E_y = \sigma_x E_y$, $j_y = \sigma_{yy}E_y = \sigma_{\perp} E_y$

No Coriolis force in Z-direction \Rightarrow
 $j_z = \sigma_{zz}E_z = \sigma_{||} E_z$

Discussion(contd...)

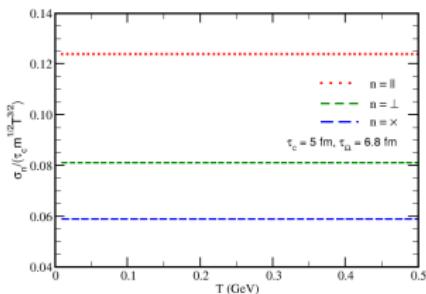


Figure: $\sigma_{\text{normalized}}$ vs T , $\mu = 0$

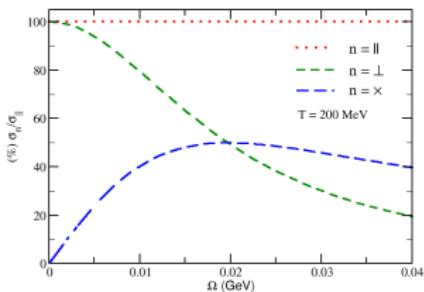


Figure: $\sigma / \sigma_{||}$ vs Ω , $\mu = 0$

For $\mu \rightarrow 0$

$$\begin{aligned}\sigma_{||} &= 0.29g \frac{\sqrt{mq^2}}{(2\pi)^{3/2}} \tau_c T^{\frac{3}{2}} \zeta(3/2), \\ \sigma_{\perp} &= 0.29g \frac{\sqrt{mq^2}}{(2\pi)^{3/2}} \frac{\tau_c}{1 + \left(\frac{\tau_c}{\tau_\Omega}\right)^2} T^{\frac{3}{2}} \zeta(3/2), \\ \sigma_{\times} &= 0.29g \frac{\sqrt{mq^2}}{(2\pi)^{3/2}} \frac{\tau_c \left(\frac{\tau_c}{\tau_\Omega}\right)}{1 + \left(\frac{\tau_c}{\tau_\Omega}\right)^2} T^{\frac{3}{2}} \zeta(3/2),\end{aligned}\quad (18)$$

$$\sigma_{zz} = \sigma_{||} \propto \tau_c,$$

$$\sigma_{xx} = \sigma_{yy} = \sigma_{\perp} \propto \tau_{\perp} = \frac{\tau_c}{1 + \left(\frac{\tau_c}{\tau_\Omega}\right)^2},$$

$$\sigma_{xy} = \sigma_{\times} \propto \tau_x = \frac{\tau_c \left(\frac{\tau_c}{\tau_\Omega}\right)}{1 + \left(\frac{\tau_c}{\tau_\Omega}\right)^2},$$

$$\sigma_{\perp} (\Omega \rightarrow 0 \text{ or } \tau_\Omega \rightarrow \infty) = \sigma_{||},$$

$$\sigma_{\times} (\Omega \rightarrow 0 \text{ or } \tau_\Omega \rightarrow \infty) = 0.$$

- We explored the equivalence nature of the Lorentz force and the Coriolis force in transport phenomena.
- The microscopic quantity- the deviation from the equilibrium distribution, is guessed with three unknown constants.
- The deviation is found by substituting it in the relaxation time approximated Boltzmann equation with the Coriolis force term.
- Then, it is used to obtain the microscopic expression of current density and is compared with the macroscopic definition of current density to get the conductivity tensor.

References

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Thank you!

All the organizers, the collaborators and the audiences.

Backups

Inclusion of Centrifugal Force: To see the effect of Centrifugal Force on the current, one may add the centrifugal force as a force term in the LHS of Eq. (7) as follows:

$$\begin{aligned} [q\vec{E} + 2m(\vec{v} \times \vec{\Omega}) - m\vec{\Omega} \times (\vec{\Omega} \times \vec{r})] \cdot \frac{\partial f}{\partial \vec{p}} &= -\frac{\delta f}{\tau_c}, \\ [q\vec{E} - m\vec{\Omega} \times (\vec{\Omega} \times \vec{r})] \cdot \frac{\partial f^0}{\partial \vec{p}} + 2m(\vec{v} \times \vec{\Omega}) \cdot \frac{\partial f^0 + \delta f}{\partial \vec{p}} &= -\frac{\delta f}{\tau_c}, \\ [q\vec{E} - m((\vec{\Omega} \cdot \vec{r})\vec{\Omega} - \Omega^2 \vec{r})] \cdot \frac{\partial f^0}{\partial \vec{p}} + 2m(\vec{v} \times \vec{\Omega}) \cdot \frac{\partial f^0 + \delta f}{\partial \vec{p}} &= -\frac{\delta f}{\tau_c}, \\ [q\vec{E} - m((\vec{\Omega} \cdot \vec{r})\vec{\Omega} - \Omega^2 \vec{r})] \cdot \frac{\partial f^0}{\partial E}(\vec{v} - \vec{u}) + 2m(\vec{v} \times \vec{\Omega}) \cdot \frac{\partial f^0}{\partial E}(\vec{v} - \vec{u}) + 2m(\vec{v} \times \vec{\Omega}) \cdot \frac{\partial \delta f}{\partial \vec{p}} &= -\frac{\delta f}{\tau_c}. \end{aligned} \quad (19)$$

Since conductivity (in general, any transport coefficient) is independent of the fluid velocity, we will put $\vec{u} = 0$ in the Eq. (19) to get:

$$\begin{aligned} [q\vec{E} - m((\vec{\Omega} \cdot \vec{r})\vec{\Omega} - \Omega^2 \vec{r})] \cdot \frac{\partial f^0}{\partial E} \vec{v} + 2m(\vec{v} \times \vec{\Omega}) \cdot \frac{\partial f^0}{\partial E} \vec{v} + 2m(\vec{v} \times \vec{\Omega}) \cdot \frac{\partial \delta f}{\partial \vec{p}} &= -\frac{\delta f}{\tau_c}, \\ [q\vec{E} - m((\vec{\Omega} \cdot \vec{r})\vec{\Omega} - \Omega^2 \vec{r})] \cdot \frac{\partial f^0}{\partial E} \vec{v} + 2m(\vec{v} \times \vec{\Omega}) \cdot \frac{\partial \delta f}{\partial \vec{p}} &= -\frac{\delta f}{\tau_c}. \end{aligned} \quad (20)$$

Backups

Let us assume that, $\delta f = -\vec{p} \cdot \vec{F}(\frac{\partial f^0}{\partial E})$ with $\vec{F} = \alpha \hat{e} + \beta \hat{\omega} + \gamma (\hat{e} \times \hat{\omega})$, where $\vec{E} = \tilde{E} \hat{e}$, $\vec{\Omega} = \Omega \hat{\omega}$, and α, β, γ are unknown constants. The Eq.(20) with the substitution of δf becomes:

$$[\frac{q\vec{E}}{m} - ((\vec{\Omega} \cdot \vec{r})\vec{\Omega} - \Omega^2 \vec{r}) + 2(\vec{F} \times \vec{\Omega})] \cdot \frac{\partial f^0}{\partial E} \vec{v} = \frac{1}{\tau_c} \vec{F} \cdot \left(\vec{v} \frac{\partial f^0}{\partial E} \right). \quad (21)$$

We have three linearly independent vectors, i.e., \hat{e} , $\hat{\omega}$, and $\hat{\omega} \times \hat{e}$. One may, without loss of generality, assume that $\hat{\omega} = \hat{k}$, $\frac{\hat{e} \times \hat{\omega}}{|\hat{e} \times \hat{\omega}|} = \hat{j}$, and $\frac{(\hat{e} \times \hat{\omega}) \times \hat{\omega}}{|\hat{e} \times \hat{\omega}|} = \frac{\hat{\omega} \times (\hat{\omega} \times \hat{e})}{|\hat{e} \times \hat{\omega}|} = \hat{i}$, where \hat{i} , \hat{j} , and \hat{k} are the unit vectors along X, Y, and Z axes, respectively. Now we will express the expression of centrifugal force in terms of the linear combination of \hat{e} , $\hat{\omega}$, and $\hat{e} \times \hat{\omega}$.

$$\begin{aligned} \text{Centrifugal acceleration} &= \Omega^2(\vec{r} - (\hat{\omega} \cdot \vec{r})\hat{\omega}), \\ &= \Omega^2(x\hat{i} + y\hat{j}), \\ &= \Omega^2 \left[x \frac{\hat{\omega} \times (\hat{\omega} \times \hat{e})}{|\hat{e} \times \hat{\omega}|} + y \frac{\hat{e} \times \hat{\omega}}{|\hat{e} \times \hat{\omega}|} \right], \\ &= \frac{1}{4\tau_\Omega^2} \left[-\frac{x}{|\hat{e} \times \hat{\omega}|} \hat{e} + \frac{x(\hat{\omega} \cdot \hat{e})}{|\hat{e} \times \hat{\omega}|} \hat{\omega} + \frac{y}{|\hat{e} \times \hat{\omega}|} \hat{e} \times \hat{\omega} \right]. \end{aligned} \quad (22)$$

Backups

Further one notices $\vec{F} \times \vec{\Omega} = -\gamma\Omega\hat{e} + \gamma\Omega(\hat{\omega} \cdot \hat{e})\hat{\omega} + \alpha\Omega(\hat{e} \times \hat{\omega})$. By equating the coefficients of the linearly independent basis vectors from both sides of Eq. (21), we get the following three equations:

$$\frac{q\tilde{E}}{m} - \frac{\gamma}{\tau_\Omega} - \frac{x}{4\tau_\Omega^2|\hat{e} \times \hat{\omega}|} = \frac{\alpha}{\tau_c}, \quad \frac{\gamma}{\tau_\Omega}(\hat{\omega} \cdot \hat{e}) + \frac{x(\hat{\omega} \cdot \hat{e})}{4\tau_\Omega^2|\hat{e} \times \hat{\omega}|} = \frac{\beta}{\tau_c}, \quad \frac{\alpha}{\tau_\Omega} + \frac{y}{4\tau_\Omega^2|\hat{e} \times \hat{\omega}|} = \frac{\gamma}{\tau_c}. \quad (23)$$

The above equations can be simplified to give:

$$\begin{aligned}\alpha &= \frac{\tau_c \left(\frac{q\tilde{E}}{m} \right)}{1 + \left(\frac{\tau_c}{\tau_\Omega} \right)^2} - \frac{\frac{\tau_c}{\tau_\Omega}}{4\tau_\Omega|\hat{e} \times \hat{\omega}|(1 + (\frac{\tau_c}{\tau_\Omega})^2)} \left(x + \frac{\tau_c}{\tau_\Omega} y \right), \\ \gamma &= \frac{\tau_c \left(\frac{\tau_c}{\tau_\Omega} \right) \left(\frac{q\tilde{E}}{m} \right)}{1 + \left(\frac{\tau_c}{\tau_\Omega} \right)^2} + \frac{\frac{\tau_c}{\tau_\Omega}}{4\tau_\Omega|\hat{e} \times \hat{\omega}|(1 + (\frac{\tau_c}{\tau_\Omega})^2)} \left(-x \frac{\tau_c}{\tau_\Omega} + y \right), \\ \beta &= \frac{\tau_c \left(\frac{\tau_c}{\tau_\Omega} \right)^2 (\hat{\omega} \cdot \hat{e}) \left(\frac{q\tilde{E}}{m} \right)}{1 + \left(\frac{\tau_c}{\tau_\Omega} \right)^2} + \frac{\frac{\tau_c}{\tau_\Omega} \hat{\omega} \cdot \hat{e}}{4\tau_\Omega|\hat{e} \times \hat{\omega}|(1 + (\frac{\tau_c}{\tau_\Omega})^2)} \left(x + \frac{\tau_c}{\tau_\Omega} y \right).\end{aligned} \quad (24)$$

Backups

$$\begin{aligned}\delta f &= -\vec{p} \cdot \vec{F} \frac{\partial f^0}{\partial E} \\ &= -\frac{\partial f^0}{\partial E} m \vec{v} \cdot (\alpha \hat{\mathbf{e}} + \beta \hat{\omega} + \gamma (\hat{\mathbf{e}} \times \hat{\omega})) , \\ &= -\frac{\partial f^0}{\partial E} m \vec{v} \cdot \left[\left[\frac{\tau_c \left(\frac{q \tilde{E}}{m} \right)}{1 + \left(\frac{\tau_c}{\tau_\Omega} \right)^2} - \frac{\frac{\tau_c}{\tau_\Omega}}{4 \tau_\Omega |\hat{\mathbf{e}} \times \hat{\omega}| \left(1 + \left(\frac{\tau_c}{\tau_\Omega} \right)^2 \right)} (x + \frac{\tau_c}{\tau_\Omega} y) \right] \hat{\mathbf{e}} \right. \\ &\quad \left. + \left[\frac{\tau_c \left(\frac{\tau_c}{\tau_\Omega} \right)^2 (\hat{\omega} \cdot \hat{\mathbf{e}}) \left(\frac{q \tilde{E}}{m} \right)}{1 + \left(\frac{\tau_c}{\tau_\Omega} \right)^2} + \frac{\frac{\tau_c}{\tau_\Omega} \hat{\omega} \cdot \hat{\mathbf{e}}}{4 \tau_\Omega |\hat{\mathbf{e}} \times \hat{\omega}| \left(1 + \left(\frac{\tau_c}{\tau_\Omega} \right)^2 \right)} (x + \frac{\tau_c}{\tau_\Omega} y) \right] \hat{\omega} \right. \\ &\quad \left. + \left[\frac{\tau_c \left(\frac{\tau_c}{\tau_\Omega} \right) \left(\frac{q \tilde{E}}{m} \right)}{1 + \left(\frac{\tau_c}{\tau_\Omega} \right)^2} + \frac{\frac{\tau_c}{\tau_\Omega}}{4 \tau_\Omega |\hat{\mathbf{e}} \times \hat{\omega}| \left(1 + \left(\frac{\tau_c}{\tau_\Omega} \right)^2 \right)} (-x \frac{\tau_c}{\tau_\Omega} + y) \right] (\hat{\mathbf{e}} \times \hat{\omega}) \right] ,\end{aligned}\tag{25}$$

Backups

Finally, we have,

$$\delta f = -\frac{\partial f^0}{\partial E} \left(\frac{q\tau_c}{1 + (\frac{\tau_c}{\tau_\Omega})^2} \right) \left[\delta_{jl} + \left(\frac{\tau_c}{\tau_\Omega} \right)^2 \omega_j \omega_l + \left(\frac{\tau_c}{\tau_\Omega} \right) \epsilon_{ijk} \omega_k \right] \tilde{E}_j v_l - m \frac{\partial f^0}{\partial E} \frac{\frac{\tau_c}{\tau_\Omega}}{4\tau_\Omega |\hat{\mathbf{e}} \times \hat{\omega}| (1 + (\frac{\tau_c}{\tau_\Omega})^2)} \\ \left[-\delta_{jl} \left(x + \left(\frac{\tau_c}{\tau_\Omega} \right) y \right) + \omega_j \omega_l \left(x + \left(\frac{\tau_c}{\tau_\Omega} \right) y \right) + \epsilon_{ijk} \omega_k \left(-x \left(\frac{\tau_c}{\tau_\Omega} \right) + y \right) \right] e_j v_l \quad (26)$$

The second term of RHS of Eq. (25) gives a current that is not proportional to the electric field. Hence, it will not contribute to the electrical conductivity components. We may call it a Centrifugal Current (\vec{j}_c):

$$j_{ci} = -mqg \int \frac{d^3 p}{(2\pi)^3} \frac{\partial f^0}{\partial E} \frac{v^2}{3} \frac{\frac{\tau_c}{\tau_\Omega}}{4\tau_\Omega |\hat{\mathbf{e}} \times \hat{\omega}| (1 + (\frac{\tau_c}{\tau_\Omega})^2)}$$

$$\left[-\delta_{ij} \left(x + \left(\frac{\tau_c}{\tau_\Omega} \right) y \right) + \omega_j \omega_i \left(x + \left(\frac{\tau_c}{\tau_\Omega} \right) y \right) + \epsilon_{ijk} \omega_k \left(-x \left(\frac{\tau_c}{\tau_\Omega} \right) + y \right) \right] e_j . \quad (27)$$