

The performance of BM@N spectrometer

BMN collaboration

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1 Introduction

BM@N (baryonic matter at Nuclotron) is the first experiment operational at the ion-accelerating complex Nuclotron/NICA, studying interactions of relativistic ion beams of heavy ions with fixed targets [1] in the energy range of high densities of baryonic matter [2]. At the Nuclotron energies, the density of nucleons in a fireball created by two colliding heavy nuclei is 3-4 times higher than the nuclear saturation density[3]. In addition, these energies are high enough to study strange mesons and (multi)-strange hyperons produced in nucleus-nucleus collisions close to the kinematic threshold [4, 5]. The primary goal of the experiment is to constrain parameters of the equation of state (EoS) of high-density nuclear matter. Studies of the excitation function of strange particle production below and near to the kinematical threshold make it possible to distinguish hard behaviour of the EoS from the soft one [6].

The Nuclotron will provide the experiment with beams of a variety of particles, from protons to gold ions, with kinetic energy in the range from 1 to 6 GeV/nucleon for light ions with Z/A ratio of ~ 0.5 and up to 4.5 GeV/nucleon for heavy ions with Z/A ratio of ~ 0.4 .

The BM@N detector is a forward spectrometer covering the pseudorapidity range $1.6 \leq \eta \leq 4.4$. Schematic view of the BM@N setup is shown in Fig. 1. The description of the spectrometer subsystems is organised in a “downstream beam” order. The details for all subsystems are given in a corresponding sections below.

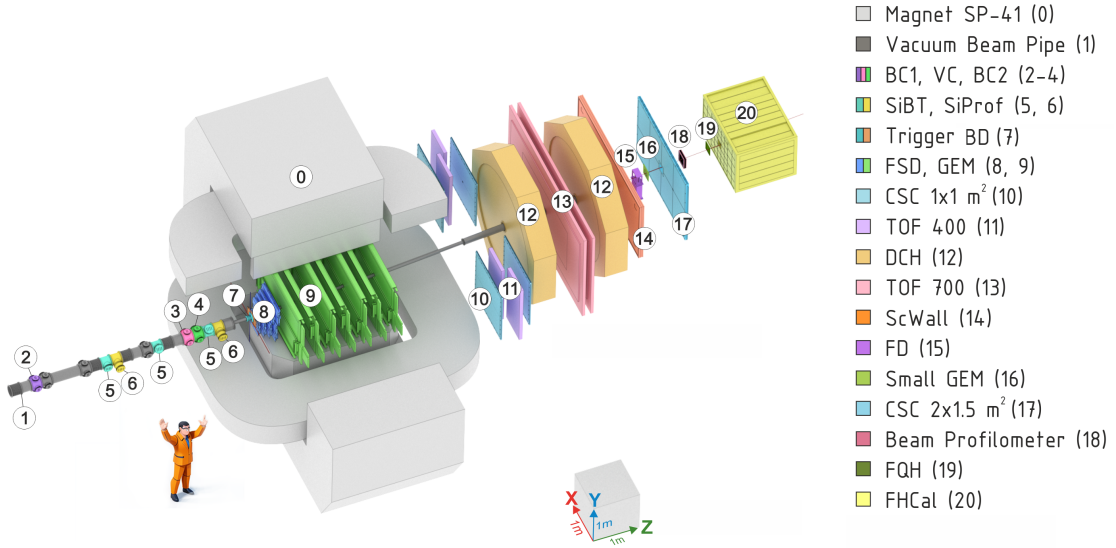


Figure 1: Schematic view of BM@N setup in RUN8.

2 Beamline

2.1 Beam transport

The BM@N experiment is part of the NICA complex (see Fig. 2), located on the extracted beam from the Nuclotron in the target hall.

Electronic string source of the highly-charged ions "KRION-6", provides heavy ions of Au^{31+} (up to 2×10^9 per pulse with a pulse repetition rate of 10 Hz) and delivers them into the HILac.

The main tasks of the booster are as follows:

- accumulation of ions at an injection energy of 2.5×10^9 $^{197}Au^{31+}$ ions;
- effective acceleration of incompletely stripped ions, which is possible due to the ultrahigh vacuum in the beam chamber;
- formation of the required phase volume of the beam using an ECS at an energy of 65 MeV/n;
- acceleration of heavy ions to the energy required for their efficient stripping;
- fast (single-lap) extraction of the accelerated beam for its injection into the Nuclotron.

The Nuclotron SC proton synchrotron has three operation modes:

- Acceleration of heavy ions for storage in the collider.
- Acceleration of polarized protons and deuterons for feeding the collider.
- Acceleration of both polarized and unpolarized protons and deuterons and heavy ions for internal target experiments or slow extraction to fixed target experiments.

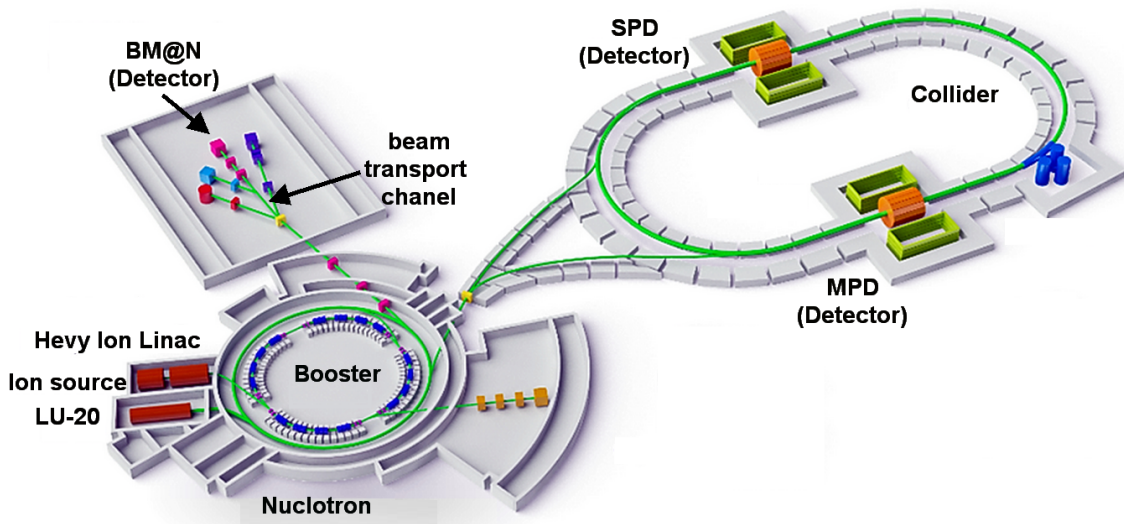


Figure 2: Complex NICA.

The beam extracted from the Nuclotron is transported to the BM@N experimental area over a distance of about 110 m by a set of dipole magnets and quadrupole lenses. At the entrance of the BM@N setup the position and direction of the beam are already close to those required to bring the beam to the target, and only relatively small adjustments are needed in order to provide final steering of the beam. These corrections are performed by a pair of dipole magnets, VKM and SP-57, which allow bending in vertical and horizontal planes and have maximum current 250A and 600A respectively. The centers of these magnets are positioned at approximately 7.7 and 5.7 m from the target (Fig. 3). In addition, a doublet of quadrupole lenses, 1k200 and 2k200, each having the maximum current of 2500A, allows optimal focusing of the beam on the target. The corresponding position of their centers is at about 12.5 and 10.0 m upstream of the target.

The target is located inside the analyzing magnet SP-41, therefore, after passing through the target, the beam ions are deflected by the magnetic field of SP-41 (maximum current 2000A, $Bd = xxx$ Tm). It should be noted that for experiments with heavy ions it is essential to enclose the beam transport channel in vacuum, including the part that goes through the analysing magnet. This requirement combined with precise placement of the tracking detectors inside the SP-41 does not allow quick reconfiguration of the detectors for different beam momenta, making it necessary to adjust the magnetic field of the analysing magnet depending on the choice of the beam momentum. Studies of the Xe + CsI collisions during the 2022-2023 run were performed at beam energies of 3.0 GeV/n and 3.8 GeV/n, and the current of the SP-41 was set to 1395 and 1720 A respectively.

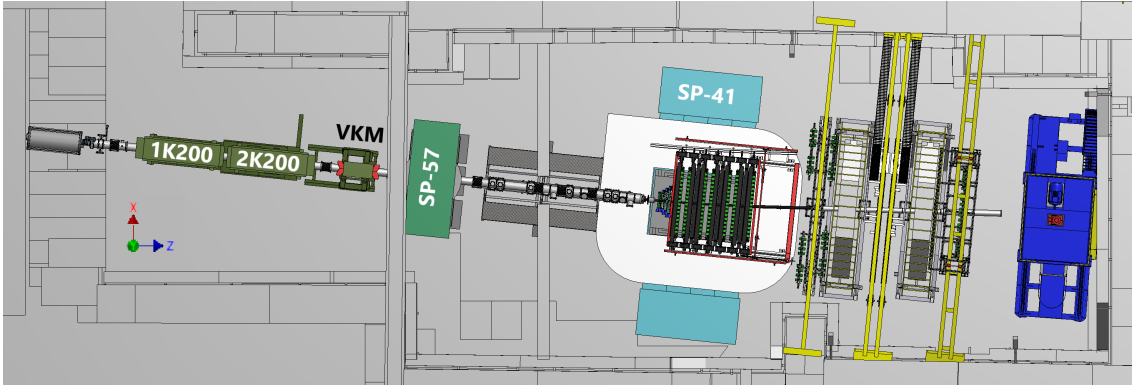


Figure 3: Magnetic elements of the BM@N setup.

59 2.2 Vacuum beam pipe

60 A vacuum beam pipe was integrated into the experimental setup in order to minimize the amount
 61 of scattering material on the way of heavy ion beam. The beam pipe has continuous vacuum, but
 62 in terms of components and material of the tube it can be subdivided into four large parts: the first
 63 section covers the region upstream of the magnet SP-57 and within the magnet itself, the second
 64 section goes up to the target, the third section is placed inside the analyzing magnet SP-41 and the
 65 last section is located after the analyzing magnet. Vacuum in the entire beam pipe at the BM@N
 66 setup is achieved by a single roots pump installed upstream of the 1K200 quadrupole lens. The
 67 pressure maintained during the experiment is at the level of 10^{-4} Torr. With the exception of the
 68 third part, the configuration of vacuum pipe and its components were designed, manufactured and
 69 tested by LLC Vacuum systems and technologies (Belgorod, Russia). ISO-K vacuum standard is
 70 accepted for flange connections, however, significant fraction of the components was custom made
 71 in order to meet limitations posed by aperture of the magnets and geometry of the detectors.

72 The first part of the beam pipe is designed to create vacuum in the area of beam transport
 73 through 1K200 and 2K200 quadrupole lenses and through corrective magnets VKM and SP-57.
 74 This part of the vacuum pipe is made of stainless steel, has length of 11.7 m and outer diameter
 75 200mm. Two slide gates are installed in this section, one in the front of the 1K200 lense and
 76 another after the VKM magnet. The vacuum level is monitored by two vacuum gauges, the data
 77 from which are recorded in the slow control system.

78 The second part of the beam pipe serves to create vacuum in the region between the SP-57
 79 magnet and the target node located inside the SP-41 magnet. This part of the beam pipe is xxx
 80 m long and also has outer diameter 200mm. It includes vacuum boxes containing beam detectors
 81 described in the next section: two 3-way boxes for profilometers, three 3-way boxes for silicon
 82 tracker and three 6-way boxes for trigger counters BC1, BC2 and VC. All boxes located outside
 83 the magnetic field of the analyzing magnet SP-41 are made of stainless steel, while the vacuum
 84 pipe components, which have to be close to the target and therefore placed in the magnet, are
 85 made of aluminum: compensator and three boxes for profilometer, Si beam tracker and BC2.
 86 Bending of the beam ion trajectories by the magnetic field leads to a deflection from a straight line
 87 resulting in a few mm displacement in X direction at the target location. During the assembly of
 88 vacuum elements of the beam pipe, an adjustment is carried out in order to compensate for this
 89 deflection. For that purpose the corresponding groves for O-rings of the vacuum boxes are made
 90 slightly wider than dictated by the ISO standard and allow slight off-center shifts of the vacuum
 91 pipe components. The target flange assembly is also made of aluminum as well as an ISO240 to
 92 66 mm vacuum adapter for connection with the vacuum tube of the third section.

93 The third part of the beam pipe is 4.5 m long and made of carbon fiber by so-and-so producer.
 94 The entire carbon pipe consists of four straight segments of different lengths connected to each
 95 other by flangeless carbon fiber connections, which provide possibility to align sections at slight
 96 angles with respect to each other as shown in Fig. 4 and 5. The rotation angles were evaluated
 97 by the simulation of the 4.5 AGeV (???) gold ions trajectories in the magnetic field of SP-41 at
 98 current xxx A. The carbon beam pipe is suspended on two supports also made of carbon fiber and
 99 installed on two lower GEM detectors, the one closest to the target and the most downstream. The
 100 supports have adjustment units for precise positioning of the carbon beam pipe on the beam axis
 101 (Fig. 5). The carbon beam pipe was designed to sustain vacuum up to 10^{-4} Torr. In the straight
 102 segments the thickness is about 1 mm, while in flangeless connections it reaches 2 mm.

103 The fourth part of the beam pipe provides vacuum volume along the beam trajectory through

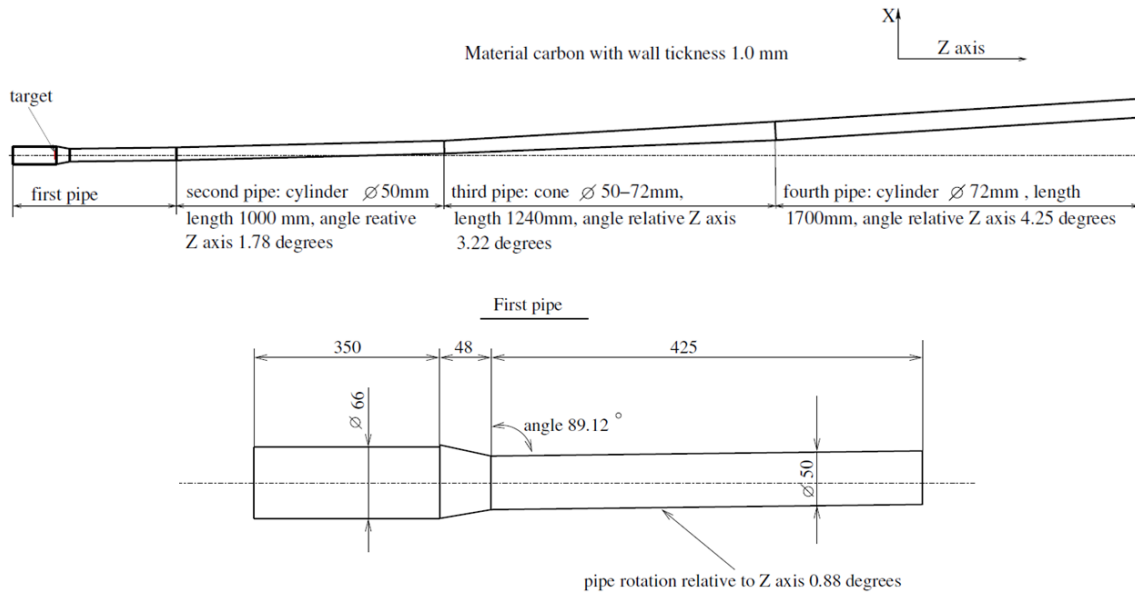


Figure 4: Technical design of the carbon beam pipe.

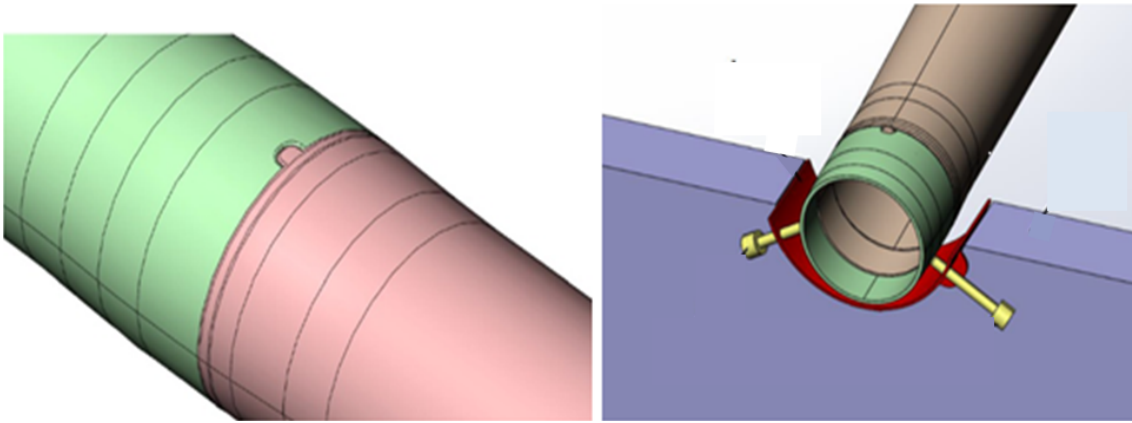


Figure 5: 3D models of the dismountable flangeless connection (left) and the support scheme of the carbon beam pipe in the GEM beam hole (right).

104 the outer tracker system. The pipes and flanges of this section as well as connection to the carbon
 105 beam pipe are made from aluminum (Fig. 6). It has overall length of about 3.2 m (?) and consists
 106 of three straight segments 1.2, 0.96 and 1.0 meter long, made from tube with outer diameter of
 107 125 mm and wall thickness of xx mm. At the end of this section, the overall vacuum line is closed
 108 by a 100 μ m thick titanium membrane installed in ... (?) after the adapter for a diameter of 150
 109 mm.

110 2.3 Target station

111 The target station is located at the end of the second beam pipe section. It is designed to provide a
 112 possibility to insert a target in the beam line inside the vacuum volume and to interchange several
 113 targets without breaking the vacuum. The model and photo of the target station are presented
 114 in (Fig. 7). An aluminum flange of 240 mm in diameter serves as a holder of the target assembly
 115 elements and as an adapter between the beam pipe upstream of the target station and the first
 116 section of the carbon beam pipe. On the outer part of this flange, four pneumatic cylinders are
 117 installed providing capability to move in and out of the beam four target frames interchangeably.
 118 The pneumatic cylinders are produced by FESTO and allow remote operation. An optocoupler
 119 sensor is used in order to control the target position via a special electronic module.

120 The part of the target assembly placed inside the vacuum can be divided into three components:
 121 1) Centering frame, which fits into the inner part of the first section of the carbon beam pipe.
 122 2) Four petals, in which the targets themselves are installed. In the normal state, all petals are
 123 leaning against the side surface of the beam pipe.



Figure 6: Carbon beam pipe connected by a flange to aluminum beam pipe in the BM@N setup.

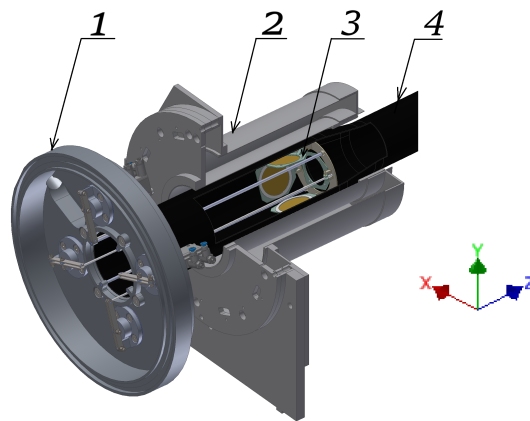


Figure 7: 3D model of target station. 1. Aluminum flange target station. 2. Barrel detector. 3. four targets. 4. Carbon beam pipe.

124 3) Carbon fiber retaining pins, 300mm long and 3mm in diameter.

125 In the run with the Xe beam, three disk targets about 3.2 cm in diameter were used: CsI
 126 1.75mm thick, CsI 0.85 mm thick, and Ge 1.02mm thick. One frame of the target assembly was
 127 left empty and was used to evaluate the background level caused the particles interactions with
 128 the structural elements of the target station.

129 2.4 Magnetic field of the analysing magnet

130 The dipole magnet SP-41 with large acceptance is used in the spectrometer as analysing magnet for
 131 measurement of momenta of produced particles and beam fragments. In the course of preparation
 132 of the magnet for the BM@N experiment, significant upgrade was done in 2012-2013 from SP-41
 133 initial configuration used in ~~the~~ experiments with a streamer chamber. In particular, the hole
 134 for a photcamera in the upper pole was filled with steel in order to improve the uniformity of
 135 the magnetic field, and the distance between the poles was increased by about 30 cm in order to
 136 provide space required by the GEM chambers of the BM@N. The dimensions of the SP-41 pole in
 137 the **horizontal direction** and in the direction along the beam is about 1.4 and 2.5 m, respectively,
 138 while the vertical distance between the upper and lower poles after the upgrade is 1.06 m (Fig. 8).
 139 **In the BM@N setup the magnet is roughly centered on the beam line, in the horizontal plane the**
 140 **beam axis goes through the magnet close to the center of the poles, while vertically the beam axis**
 141 **is shifted closer to the lower pole by about 40 mm.** The leading edge of the pole defines the origin
 142 of the z axis, and, correspondingly, the target is installed inside the SP-41 magnet at this position
 143 ~~along the beam.~~ The target station is described in more detail in the chapter Targets.

144 Determination of the momentum of the produced particles requires detailed knowledge of the
 145 value and orientation of the magnetic field of the analysing magnet. After the upgrade of ~~the~~
 146 SP-41, the measurement of its field was performed by means of planar and 3D Hall probes [7]. In
 147 addition, the shape of the field was calculated by the TOSCA code using known configuration of
 148 the yoke and coils material. Prior to the run with Xe beam, ~~in Spring 2022,~~ the measurement of the
 149 magnetic field was repeated with a goal to obtain the field map for a wider X, Y, Z range and with

150 smaller steps. The measurements with 3D Hall probes covered $(-156, +145 \text{ cm})$, $(-38, +54 \text{ cm})$,
 151 $(-162, +439 \text{ cm})$ and were performed in $(126 \times 47 \times 241)$ points in X, Y, Z coordinates respectively,
 152 allowing one to construct the field map on a $2.4 \times 2.0 \times 2.5 \text{ cm}^3$ three-dimensional grid (Fig. 8).
 153 During simulation and event reconstruction, the magnetic field components in a particular (x, y, z)
 154 point are calculated by linear interpolation over eight neighboring measured nodes.

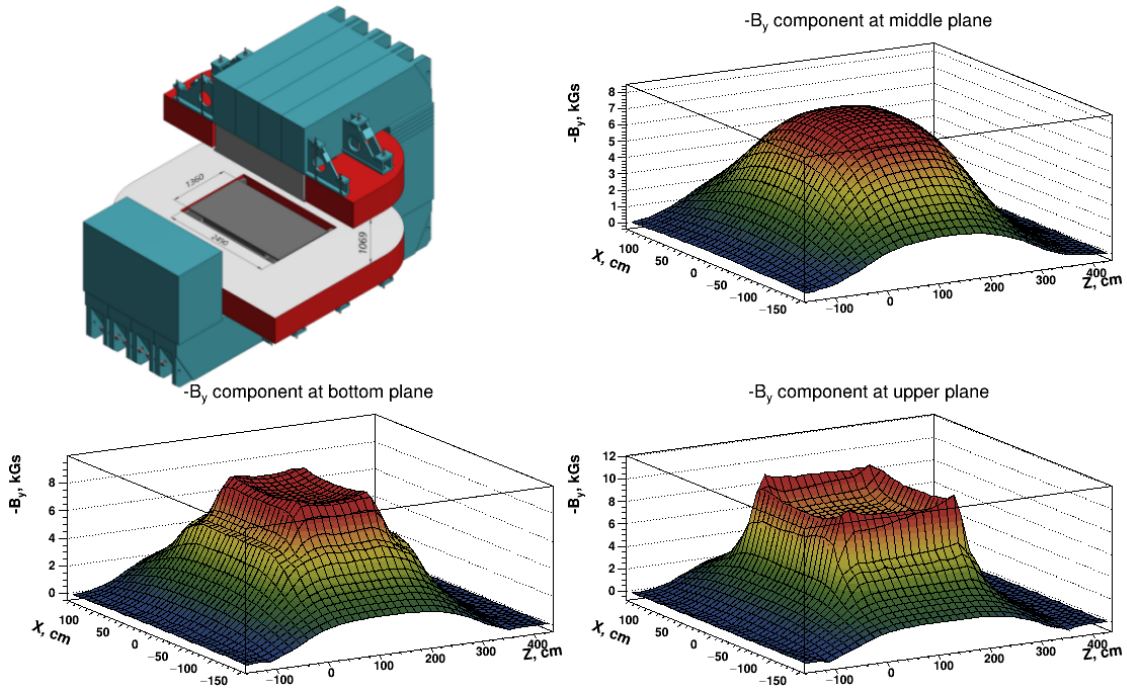


Figure 8: Magnetic field map of the analyzing magnet SP-41.

155 The measurements of the field map was performed for four values of the current: 900, 1300,
 156 1600, and 1900 A.

157 Needed additions:

- 158 1) plot of field V_y versus current with points for 3.0 and 3.8 AGeV settings
 159 2) explanation of "linear interpolation" for a 3D grid

3 Beam and trigger detectors

Fig. 9 shows a schematic layout of the trigger detectors, placed on the beam line. In the target area the multiplicity detectors are also shown as a part of the trigger system.

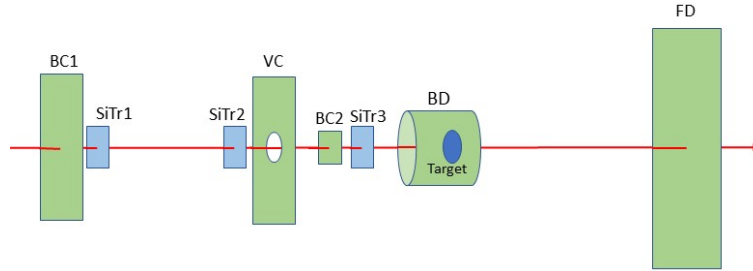


Figure 9: Trigger detectors layout.

Some physical parameters of the beam line detectors are summarized in Table 1.

Aperture of the beam is limited by the 25 mm diameter hole in the scintillation Veto Center (VC), which rejects the beam halo. The hole diameter in VC is chosen to be large enough to accept most of the beam ions, but smaller than the diameter of the target XX mm. Typically, in the 2023 Xe run, 80% of the beam was accepted by the VC. In order to minimize interactions upstream of the target, scintillators and active parts of silicon detectors are located in vacuum, while the photomultiplier tubes of the scintillation counters and the front-end electronics of the silicon detectors are kept in the air with their housings mounted to the flanges of the beam pipe.

Detector	Z position, cm	Active area, mm x mm	Material	Thickness, mm
BC1	-zz	100 x 100	Scint. BC400B	0.25
BC2	-zz	34 x 34	Scint. BC400B	0.15
VC	-zz	113 x 113 (hole 25)	Plastic	4
SiBTr1	-zz	61 x 61	Silicon	0.175
SiBTr2	-zz	61 x 61	Silicon	0.175
SiBTr3	-zz	61 x 61	Silicon	0.175
FD	+zz	150 x 150	Plastic	0.5
Small GEM	+zz	100 x 100		
FQH	+zz	160 x 160	Quartz	4

Table 1: Parameters of beam and fragment detectors.

In all the beam scintillation counters - BC1, BC2 and VC - light from the scintillator is collected by Al-mylar light guides to a pair of photo-multiplier tubes, placed above and below the scintillator. Such orientation of PMT's in BC2 and VC detectors is dictated by the requirement that they should operate in the magnetic field of the analysing magnet, because these counters are located close to the target. Mesh dynode photomultiplier tubes Hamamatsu R2490-07 are used in the detectors BC1 and VC, whereas the BC2 has microchannel plate PMT's Photonis XPM85112/A1 Q400. In addition to beam geometry, the detectors BC1 and BC2 define start time for the time-of-flight system. The requirement to obtain precise time measurement favored the design of BC1 and BC2 with light collection by two PMT's. Both types of photo-multiplier tubes used in these counters have excellent timing characteristics. The signal from each PMT is sent to a fast fan-out module which has time jitter of about 10 ps and preserves high quality of time response. The signal from one output of the fan-out is sent to a TQDC which allows to determine time and amplitude of the pulse. After correction for time walk (slewing), the resolution obtained in 2022 Xe run using the signals from both photo-tubes was found to be 40 ps for BC1 and BC2 individually, and 30 ps for the combined response of the system of two counters. The input in the trigger logic is configured to accept one signal from each of the beam counters, BC1, BC2 and VC. Individual signals from top or bottom PMT's are affected by light collection non-uniformity to a larger degree than a combined signal from two photo-tubes. Therefore, in all counters the signals from top and bottom PMT's are balanced in gain by high-voltage settings, and the signals from the second output of the fan-outs are sent to a passive linear fan-in after which the summed signals are fed to the trigger logic unit. In addition, the summed signals are read-out using TQDC for trigger setting up and monitoring.

193 Upstream the target the beam position is traced by a set of silicon tracker detectors. The
 194 beam tracker system consists of three double-sided silicon strip detectors identical in design. Each
 195 detector has 60 mm by 60 mm active area with orthogonal orientation of p+ and n+ strips on two
 196 sides. These detectors are kept permanently in the beam and provide information about beam
 197 ion trajectory for each event. More detailed description of the beam tracker is given in the next
 198 chapter. In addition to the beam tracker, the beam position and profile can also be measured
 199 by a pair of beam profilometers which are similar in design and parameters to the beam tracker
 200 stations, but have a much courser pitch 1.8 mm in X and Y. The read-out of the profilometers is
 201 organised independently of the main BM@N DAQ in order to facilitate beam tuning at the early
 202 stages of the run. The detectors of the beam profilometers can be moved in and out of the beam
 203 by remotely controlled drivers without breaking the vacuum. During the data accumulation the
 204 detectors of the beam profilometers are positioned outside of the beamline.

205 Trigger detectors sensitive to the multiplicity of particles produced in the interaction include
 206 Barrel detector (BD) and Silicon multiplicity detector (SiMD). These detectors, schematically
 207 shown in Fig. 10, are placed close to the target in order to cover sufficiently large solid angle for
 208 produced particles. The target is situated inside the BD.

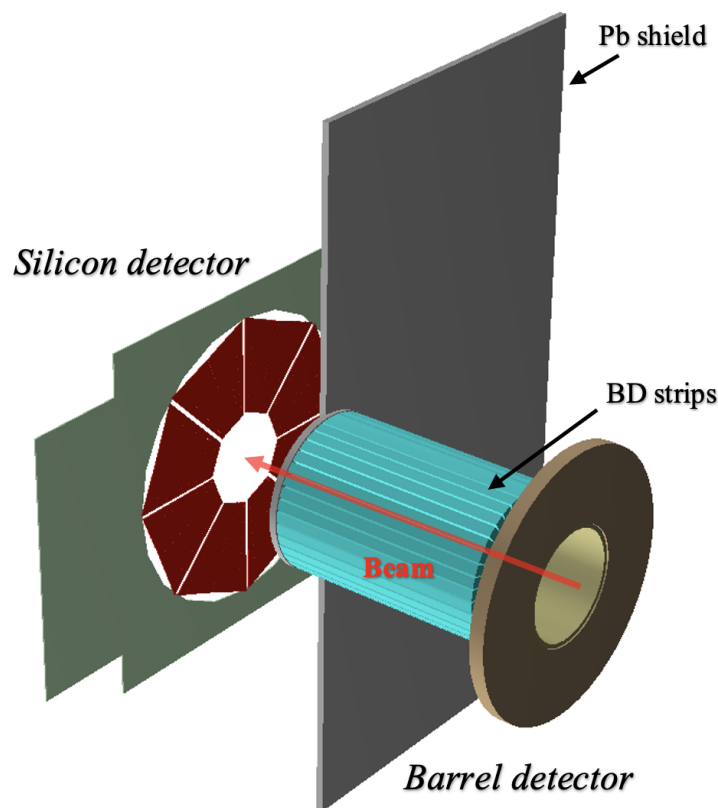


Figure 10: Schematic layout of trigger multiplicity detectors.

209 The Barrel detector is formed by 40 scintillator strips aligned along the beam line and covering
 210 cylindrical surface 90mm in diameter and 150mm long. Each strip of $150 \times 7 \times 7 \text{ mm}^3$ size is
 211 coated with aluminized mylar and viewed from one side by a silicon photo-multiplier of $6 \times 6 \text{ mm}^2$
 212 size (SensL, J-sensL).

213 Downstream analysing magnet the beam goes through the Fragment Detector (FD), Small
 214 GEM chamber and the Forward quartz hodoscope (FQH). These detectors are placed in the air,
 215 the FD is positioned right after the titanium membrane which closes the vacuum pipe line. The
 216 amplitude of the pulse in the FD reflects the charge of the ion passing through the counter. This
 217 amplitude is used in the trigger system in order to distinguish events with and without interactions
 218 in the target. To minimize the background from the interaction within the FD itself, its radiator
 219 has to be thin, while in the X and Y directions the radiator should be wide enough to cover all
 220 the beam ions going through the target without interaction. The radiator material can be chosen
 221 either from scintillator or quartz in experiments with relatively light (up to Xe) or heavy (Au, Bi)
 222 beams respectively. For most of data accumulation in the Xe 2022 run the scintillator radiator was
 223 used, while the quartz radiator was also evaluated in the short period of the run. The radiator was

224 viewed by a single photo-multiplier tube placed about 50 cm below the beam line. Light collection
225 is done by an air light guide made of aluminized mylar. Pulse height resolution of the FD with the
226 scintillator radiator was found to be 5% for Xe peak.

227 In addition to the FD the charge of spectator fragment can be determined by the 4mm thick
228 quartz hodoscope FHQ, located in front of the beam hole in the FHCa. Information from this
229 hodoscope is used in the offline analysis for event selection and determination of event centrality.
230 FHQ amplitude resolution for Xe ions is about 2%. The detailed description of the hodoscope is
231 given in the section "Forward Spectator Detectors".

232 The Small GEM detector is positioned between the FD and FHQ and used to monitor the
233 position, shape and spot size of the beam downstream the analysing magnet. The detector has
234 three GEM foils. Its active area covers 10 cm×10 cm in X and Y, with 256 strips in each coordinate
235 oriented perpendicular to each other.

4 Silicon Beam Tracker

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The Beam Tracker (SiBT) is located inside the vacuum beam pipe, directly in the beam of charged relativistic nuclei upstream of the target. BT consists of three coordinate planes (SiBT1, SiBT2, SiBT3) based on silicon double-sided strip detectors (DSSD). The main purpose of the beam tracker is the following physical tasks:

- measurement of the trajectory of xenon nuclei (^{124}Xe) that pass through all three BT planes, the target (CsI) and satisfy the conditions of trigger logic;
- restoration in the target plane (X-Y) of the coordinates of the primary vertex of the trigger nucleus;
- information about the coordinates of the nucleus track in the area $BT1 \div BT3$ is involved in the reconstruction of the reaction plane;
- in the mode of beam adjustment and aiming the beam at the target, SiBT performs the function of a profilometer, the current information about the shape and position of the beam relative to the target is displayed on the monitors “On Line Monitor”.

Each coordinate plane consists of one double-sided strip detector containing 128 strips on each side. Strips from different sides are arranged orthogonally and form a two - coordinate (X-Y) measuring system ($128p^+ \times 128n^+ = 16384\text{points}$). The dimensions of the Si-crystal of the detector are $(63 \times 63 \times 0.175)\text{mm}^3$, the active area is $(61 \times 61)\text{mm}^2$, the strip pitch is $470 \mu\text{m}$. The thickness of each DSSD silicon detector is $175 \mu\text{m}$ and is chosen as the minimum possible, taking into account the requirements of planar technology on silicon wafers of high-resistance silicon n-FZ-Si with a diameter of 4” (100 mm). The minimum allowable thickness of the detector was chosen based on the following considerations:

- the minimum amount of matter in the beam of heavy nuclei reduces the correlated background;
- the minimum volume of the active region of the detector (the region of the space charge of the detector) reduces the number of radiation defects per strip (less dark current, less noise in the registration channel);
- a large value of ionization losses $\Delta E = 245\text{MeV}/175\mu\text{m}/\text{Si}$ for Xe ($3.8\text{GeV}/n$) allows one to effectively detect nuclei with a high signal-to-noise ratio ($S/N > 150$) in case of radiation damage to detectors.

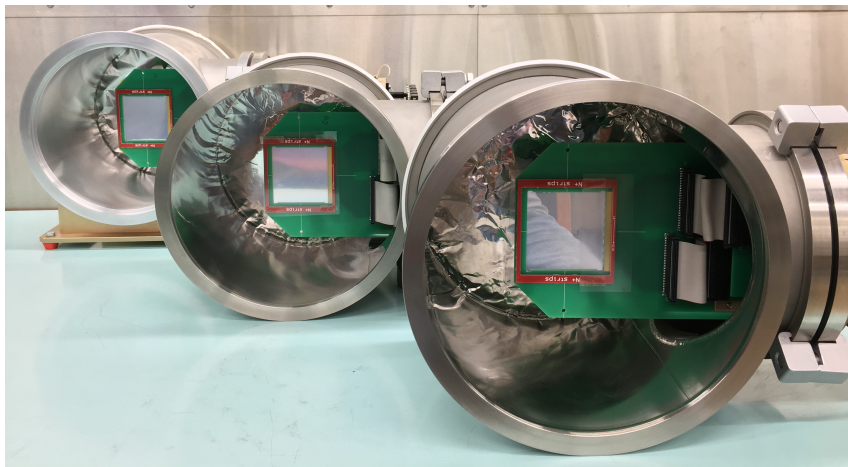


Figure 11: Three stations BT1, BT2, BT3 of the beam tracker of the BM@N experiment with detectors and FEE electronics, 256 channels, view along the beam (p^+ side of the strips).

Figure 15 shows three vacuum stations with internal coordinate planes based on silicon DSSD detectors installed inside. The positions of the coordinate system of the detectors of each plane relative to the geometrical axis of the beam pipe were measured using a NORGAU NVM II-5040D

270 video meter with an accuracy of $\pm 50 \mu\text{m}$. Structurally, the detectors are assembled on printed
 271 circuit boards with Au-contact pads, which are connected by ultrasonic bonding with Al-plated
 272 strips on the DSSD surface. The signals from the detector strips (256 strips) are sent via connectors
 273 on the board and flat cables to vacuum connectors (4 connectors) mounted on the vacuum flange.
 274 On the flange are placed 256 channel front-end-electronics (FEE) for 128p^+ strips and for 128n^+
 275 strips. The detector electronics in this case is practically outside the zone of radiation damage and
 276 is available for testing and replacement of blocks without requiring depressurization of the beam
 277 pipe.

278 Figure 16 shows a block diagram of the integrated circuit VATA64HDR16.2 (IDEAS, Norway)
 279 with a large dynamic range ($-20\text{pC} \div +50\text{pC}$) for 64 channels of signal registration from detectors.

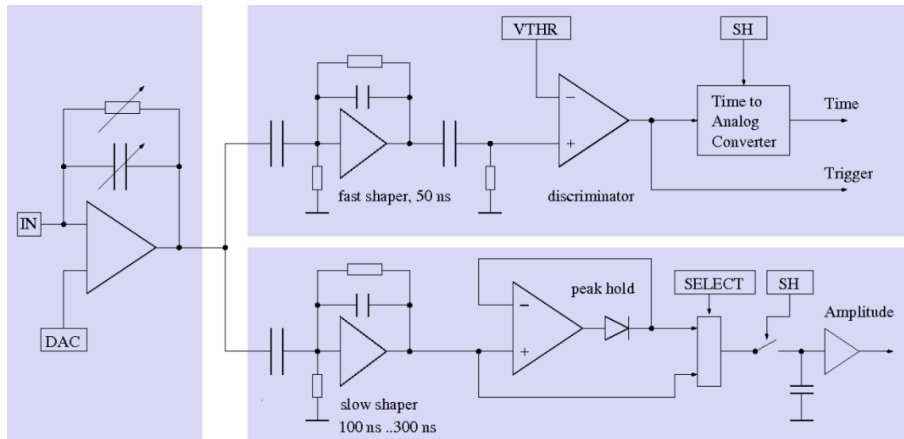


Figure 12: Block diagram of the VATA64HDR16.2 chip for the detector electronics of the beam tracker.

280 According to the signal "external trigger - SH", the values of signal amplitudes from 64 detector
 281 strips are stored on the memory capacitors and then in sequential reading mode through an analog
 282 multiplexer, the signals are transmitted to the ADC to convert analog signals into digital. The
 283 main parameters of the ASIC are given in Table 3.

Number of channels	64
Input charge (dynamic range)	$-20\text{pC} \div +50\text{pC}$ (charge from 124Xe (3.8 AGeV) in $175 \mu\text{m}$ is 11 pC)
Read-out signal generation time	50ns, 100ns, 150ns, 300ns. Programming
Trigger	1 trigger output (Trigger-OR)
Trigger signal generation time	50ns
Noise	ENC = 1fC without load
Adjustable trigger threshold	External + 4-bit threshold trim-DAC/ch.
Gain	2-gain settings programmable
Exit	Analog multiplexed output 64 pulse height samples, serial output Differential current and voltage output
Power consumption per ASIC	960mW max. depending on settings
Nutrition	+2.5V, -2.5V

Table 2: Main parameters - VATA64HDR16.2

284 Figure 13 shows the dependence of the dark current of the Si detectors for three stations SiBT1,
 285 SiBT2, SiBT3 (three colors) on the exposure time to the beam of Xe nuclei (3.8 GeV/n). The fast
 286 component reflects the ionization current only in the presence of a beam, and the slow component
 287 (substrate under the fast one) integrates the accumulated radiation defects and reflects the constant
 288 (slowly increasing in time) dark current of the detector. The amount of radiation damage of the
 289 detectors corresponds to the number of $\text{Xe}(3.8 \text{ GeV/n})$ ions passing through the detector planes,
 290 equal to $N_{\text{Xe}(3.8 \text{ GeV/n})} = 4.44 \times 10^{10}$.

291 Figure ?? shows the working position of three stations of the beam tracker on the vacuum beam
 292 pipe of the BM@N channel. Each of the following SiBT stations following along the beam is rotated
 293 relative to the previous one by an angle of 30° . Rotation of stations relative to each other is done to

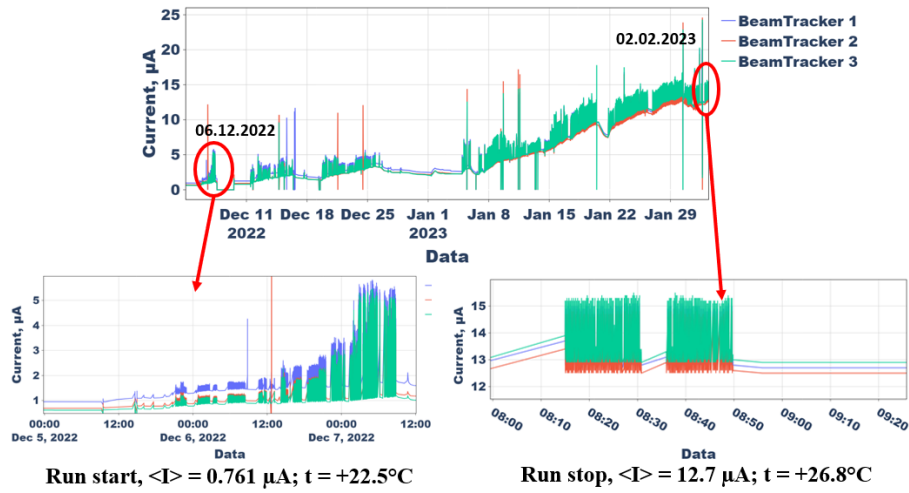


Figure 13: Chronicle of changes in the dark current of silicon detectors at stations SiBT1, SiBT2, SiBT3 in case of radiation damage during the session (from 06.12.2022 to 02.02.2023).

294 suppress false (“ghost”) hits from simultaneous tracks, because the two-coordinate system in each
 295 plane (SiBT1÷SiBT3) is orthogonal. The arrows indicate the two-dimensional cross sections of
 296 the beam of Xe nuclei (3.8 GeV/n) measured by the corresponding stations SiBT1, SiBT2, SiBT3
 297 and presented in the “On Line Monitor” mode.

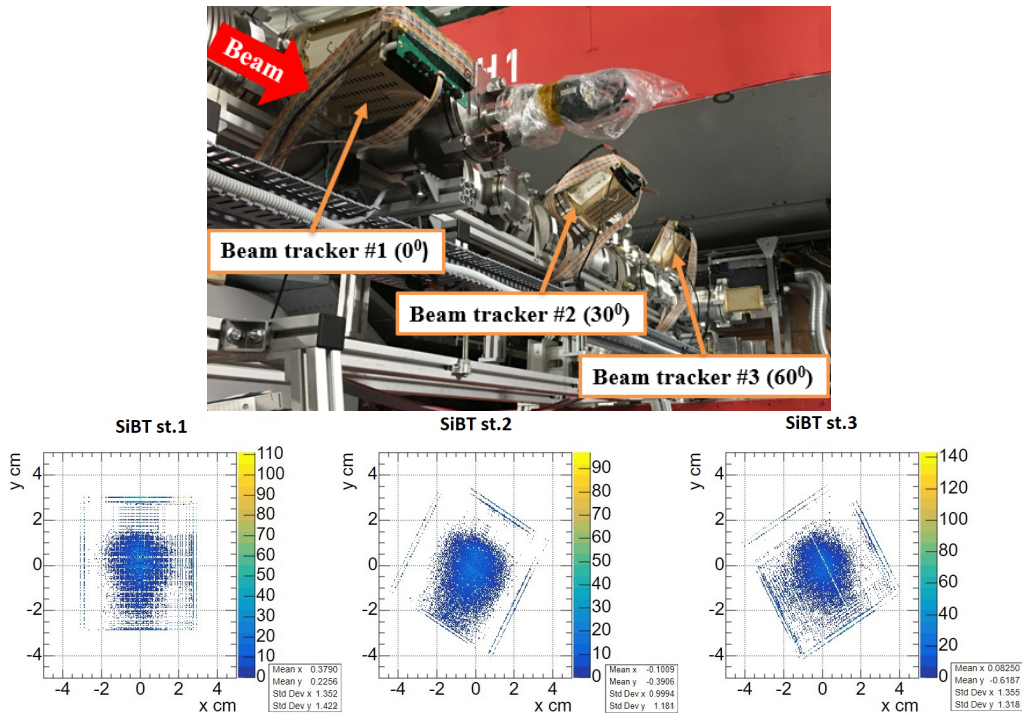


Figure 14: Operating position of three stations of the beam tracker on the vacuum beam pipe of the BM@N channel and two-dimensional beam profiles of Xe (3.8 GeV/n) nuclei measured by the corresponding BT stations.

298 The beam profiles shown in Figure 17 were obtained using the MBT trigger: counters BC1 and
 299 BC2 fired + VC not fired + FD not fired. The hole diameter VC is 25 mm, the average standard
 300 deviations of the X and Y coordinates for the profiles are 0.4878 cm and 0.5989 cm, respectively.
 301 The beam width can be estimated as $3 \times \text{Std}(X) = 1.463$ cm along the X axis and $3 \times \text{Std}(Y) =$
 302 1.797 cm along the Y axis.

5 Silicon Beam Tracker v2

As already mentioned in the previous section, the main task of the Silicon Beam Tracker (SiBT) is to measure the beam ion trajectory in each event and determine primary vertex coordinates and impact angle of the beam projectile. The tracker consists of three stations each of which utilizes a double-sided silicon strip detector (DSSD) with dimensions $(63 \times 63 \times 0.175)mm^3$. DSSD planes are cut from high-resistance mono-crystalline silicon obtained by the Float Zone method. The thickness $175 \mu m$ was chosen as the minimum possible, taking into account the limitations of the planar technology applied to 4" (100 mm) wafers. The minimum thickness of the planes allows not only to reduce the amount of material in the beam, but also to decrease the volume of space charge region of the detector and thus to lower the noise caused by the radiation defects per strip, which is very important considering that the detectors are exposed to heavy ion beams of high intensity.



Figure 15: Three stations SiBT1, SiBT2, SiBT3 with detectors and FEE electronics, view along the beam (p^+ side of the strips).

The active area in each of the detectors is $(61 \times 61)mm^2$, and the pitch between strips is $470 \mu m$ on both, p^+ and n^+ , sides resulting in total 2×128 readout channels. The strips on two sides are oriented orthogonally with respect to each other. The silicon plate in the SiBT1 detector is positioned inside the beam pipe such that the strips are aligned along the X and Y axes, whereas the plates of the SiBT2 and SiBT3 detectors are rotated azimuthally by 30 and 60 degrees respectively.

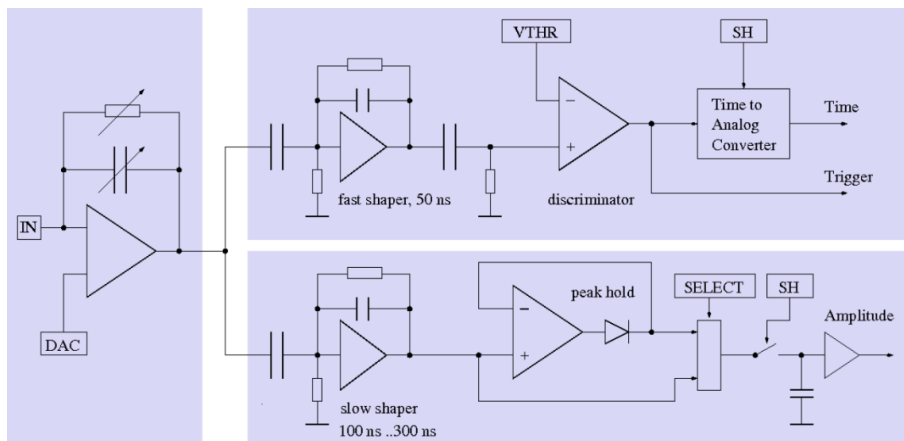


Figure 16: Block diagram of the VATA64HDR16.2 chip for the detector electronics of the beam tracker.

Figure 15 shows three vacuum stations with DSSD coordinate planes installed inside. The positions of the coordinate system of each DSSD plane relative to the geometrical axis of the beam pipe were measured using a NORGAV NVM II-5040D video meter with an accuracy of $\pm 50 \mu m$. Structurally, the detectors are assembled on printed circuit boards with gold contact pads,

325 which are connected by ultrasonic bonding with Al-plated strips on the DSSD surface. The signals
 326 from the detector strips in four groups of 64 channels are sent via flat cables to vacuum connectors
 327 (4 connectors) fixed in the vacuum flange. The front-end-electronics (FEE) for 128 p⁺ and 128 n⁺
 328 strips is mounted on the flange outside the vacuum volume. The detector electronics in this case
 329 is practically outside of high radiation zone and is available for testing and, if needed, replacement
 330 without breaking the vacuum in the beam pipe.

331 Figure 16 shows a block diagram of the integrated circuit VATA64HDR16.2 (IDEAS, Norway),
 332 chosen for the FEE because of its large dynamic range ($-20pC \div +50pC$) suitable for operation
 333 with beams of highly ionizing heavy ions. For example, charge in the input signal caused by 3-4
 334 GeV/nucleon Xe ion going through a 175 μm layer of silicon is 11 pC.

335 The ASIC VATA64HDR16.2 accepts up to 64 input channels, therefore, four of the chips are
 336 used in each of the SiBT stations. After passing through pulse shapers, at the time defined by
 337 "external trigger - SH", the values of signal amplitudes from 64 strips are stored on the mem-
 338 ory capacitors. After that, in sequential reading mode using an analog multiplexer, the 64 sig-
 339 nals are transmitted for digitization into a single ADC channel. The main parameters of the
 340 VATA64HDR16.2 chip are given in Table 3.

Number of channels	64
Input charge dynamic range	-20pC \div +50pC
Read-out signal generation time	50ns, 100ns, 150ns, 300ns, programmable
Trigger	1 trigger output (Trigger-OR)
Trigger signal generation time	50ns
Equivalent Noise Charge (ENC)	1fC without load
Adjustable trigger threshold	External + 4-bit threshold trim-DAC/ch.
Gain	2-gain settings, programmable
Output	Single analog multiplexed output of 64 pulse height samples
Power consumption per ASIC	960mW max. depending on settings
Voltage supply	+2.5V, -2.5V

Table 3: Main parameters of VATA64HDR16.2 chip.

341 Figure 17 illustrates three stations of the beam tracker mounted in the vacuum beam pipe of the
 342 BM@N channel. Histograms shown at the bottom part of the figure represent online monitoring
 343 of 2D distribution of beam ion hits in the tracker. Typical RMS of beam profile in the 2023 Xe
 344 run, measured for trigger selected events, i.e. for ions passing through the 2.5 cm dia. hole of the
 345 Veto Counter, was 0.5 cm and 0.6 cm in X and Y coordinates respectively.

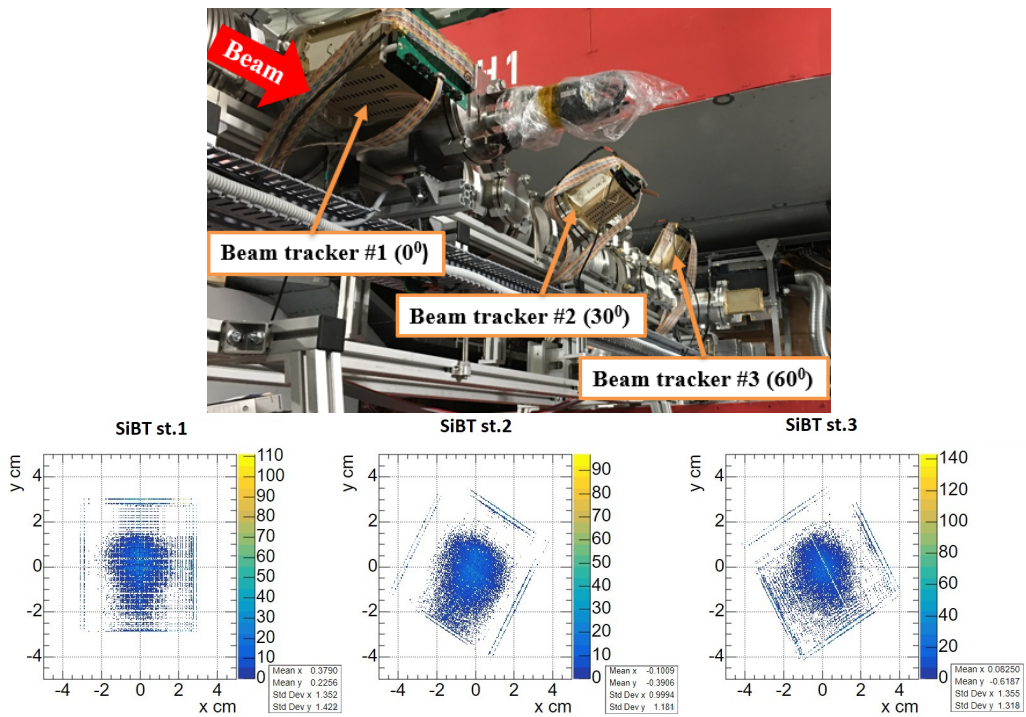


Figure 17: Operating position of three stations of the beam tracker on the vacuum beam pipe of the BM@N channel and two-dimensional beam profiles of Xe ($3.8 \text{ GeV}/n$) nuclei measured by the corresponding BT stations.

6 Forward Silicon Detector

After the completion of the 2018 technical run at the BM@N facility, it was decided to develop and create a new four coordinate planes with an increased aperture in the front of the GEM chambers - Forward Silicon Detector (FSD). The new FSD design was supposed to increase the efficiency of particle detection and the accuracy of the primary vertex reconstruction for central interactions in the 2022–2023 run with the ^{124}Xe beam (3.8 AGeV) interacting with the CsI target (2 % of nuclear interaction length). In addition to increasing the geometric dimensions of the planes, it became necessary to change the design of the planes due to the appearance of a beam vacuum tube on the BM@N channel. The presence of a section of a composite beam tube with a diameter of 50 mm after the target node required the division of the coordinate planes into upper and lower half-planes with the possibility of installing and removing detectors without touching the mounted and adjusted beam pipe.

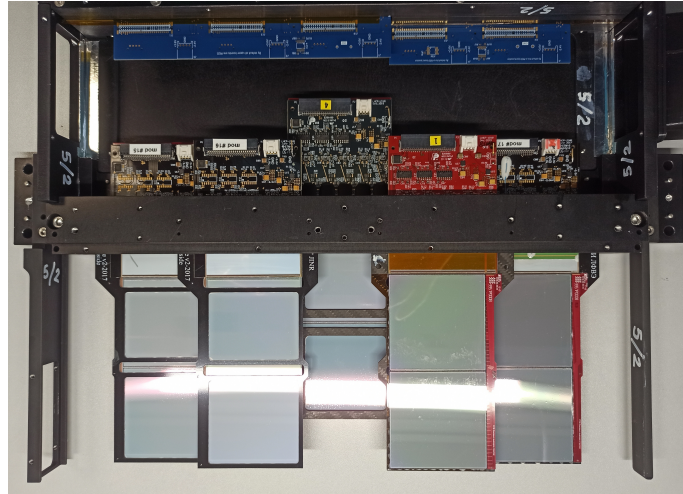


Figure 18: Appearance of the assembled 4 FSD planes (without cables) on the BM@N experiment channel inside the SP-41 analyzing magnet with the beam tube and target assembly installed.

The front part of the FSD central tracker (Fig. 23) is located in a vertical magnetic field of 1 T inside the analyzing magnet SP - 41 at a distance of $Z_1 = 161$ mm (first plane) and $Z_4 = 466$ mm (fourth plane) along the beam after the target. Each of the four silicon coordinate planes consists of two half-planes located perpendicular to the axis of the beam pipe. In the working position, the upper and lower half-planes form a single coordinate system of the plane with active regions overlapping along the Y-coordinate. In the center of each plane there is an insensitive zone in the form of a square with a cross section of 52×52 mm² to accommodate the beam tube. Each half-plane forms an independent coordinate detector with the following systems: coordinate modules based on DSSD, electronics backplane, suspension and precise positioning mechanics, cable patch panel, air cooling, temperature monitors, light and EM shield. The two half-planes of each plane are made structurally so that they are absolutely identical and interchangeable. This design allows the assembly or disassembly of the planes regardless of the installed beam pipe and with a minimum probability of its mechanical damage. The general view of the assembled eight half-planes around the beam tube inside the SP-41 magnet is shown in Fig. 23. The first plane consists of 6 modules of a new type, each module consists of one detector with dimensions of $(93 \times 63 \times 0.32)$ mm³, these are the maximum possible dimensions of a rectangular detector that fit on a Si-FZ wafer with a diameter of $\varnothing 150$ mm. Detectors of this type were developed jointly by ZNTC (Zelenograd) and LHEP JINR and manufactured at ZNTC in 2019–2020. The detector modules for the remaining three coordinate planes consist of two detectors with dimensions $(63 \times 63 \times 0.32)$ mm³, which were previously developed jointly RIMST and LHEP JINR and manufactured on n-FZ-Si wafers with a diameter of $\varnothing 100$ mm at RIMST (Zelenograd) in 2019. The total number of coordinate modules from which four planes are assembled is 48 pieces. Figure 19 shows the position and coordinates of the Si detectors relative to the target and the axis of the beam pipe. The aperture of the four planes in the direction of the Y coordinate is $\pm 15^\circ$ and in the direction of the X coordinate is $\pm 30^\circ$, which allows to cover completely the active area of the five GEM(#3 ÷ #7) planes and the first GEM#1 planes along the beam, #7 FSD detector partially covers 50%.

Table 6 shows the quantitative data of the main functional elements of the coordinate planes that form the front part of the tracker (FSD). Coordinate planes with a spatial resolution better

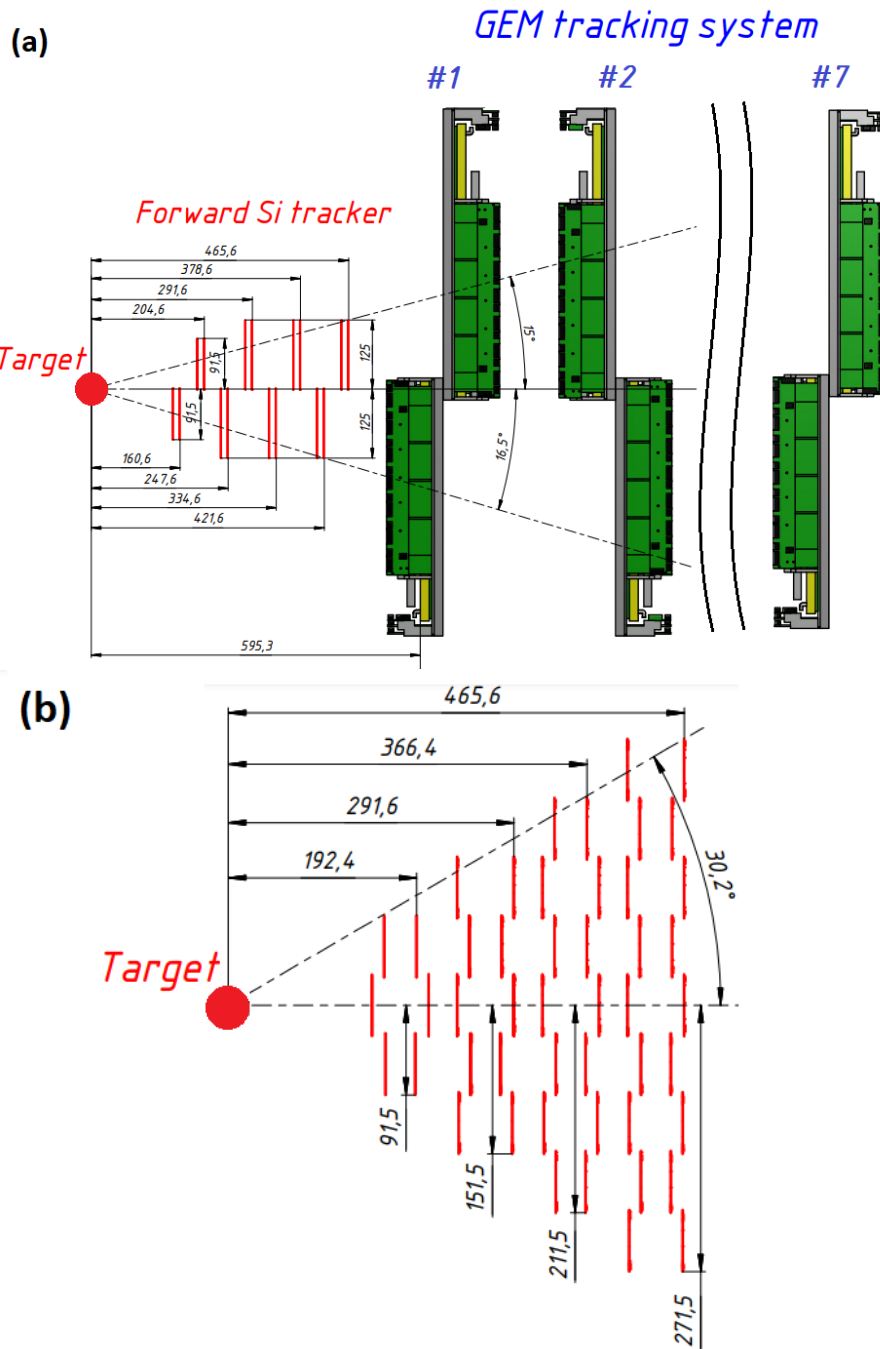


Figure 19: Scheme of the location of the FSD on the channel of the BM@N experiment (in the SP-41 magnet): (a) side view (YOZ), (b) top view (XOZ)

386 than $50 \mu\text{m}$ based on double-sided silicon detectors (DSSD) for detection of minimal ionization
 387 particles (m.i.p.) were first developed and created at JINR within the framework of the BM@N
 388 experiment. Figure 24 shows the external view of the coordinate module, which consists of two
 389 Si-detectors, two detector electronics (FEE) boards. This module has a sensitive detection area
 390 $(186 \times 63) \text{ mm}^2$, 640 coordinate strips on each side and 1280 electronics channels (10 chips, 128
 391 registration channels each).

392 The complete assembly process - testing of modules and planes is carried out on the production
 393 line for assembling LHEP modules. Double-sided silicon detectors (DSSD) and pitch adapters
 394 based on the SOS structure (Silicon on Sapphire) are manufactured at ZNTC (Zelenograd), until
 395 2019, detectors were developed and manufactured at RIMST (Zelenograd) on high-resistance silicon
 396 wafers with a diameter of 100 mm (FZ-Si, n-type, $\rho > 5 \text{ k}\Omega \times \text{cm}$, $\langle 111 \rangle$, $\varnothing 100\text{mm}$). The detectors
 397 have dimensions $(63 \times 63 \times 0.3) \text{ mm}^3$ and contain 640 strips on both sides (p^+ and n^+), the strip
 398 spacing is 95 and 103 μm , respectively, and the angle between the strips is 2.5° . DSSD technology is

Parameters	1st plane	2nd plane	3rd plane	4th plane	Total
Number Si- modules	6	10	14	18	48
Number DSSDs	6 (93 × 63)mm ²	20 (63 × 63)mm ²	28 (63 × 63)mm ²	36 (63 × 63)mm ²	90
Number ASICs ($T \leq +25^\circ$)	60	100	140	180	480
Dissipated power, W	16.86	28.16	39.42	50.69	135.13
Number PAs	12	20	28	36	96
Number FEE PCBs	12	20	28	36	96
Number of channels	7680	12800	17920	23040	53760
Square, m ²	0.035	0.073	0.102	0.132	0.307

Table 4: Main parameters of Forward Silicon Detector BM@N

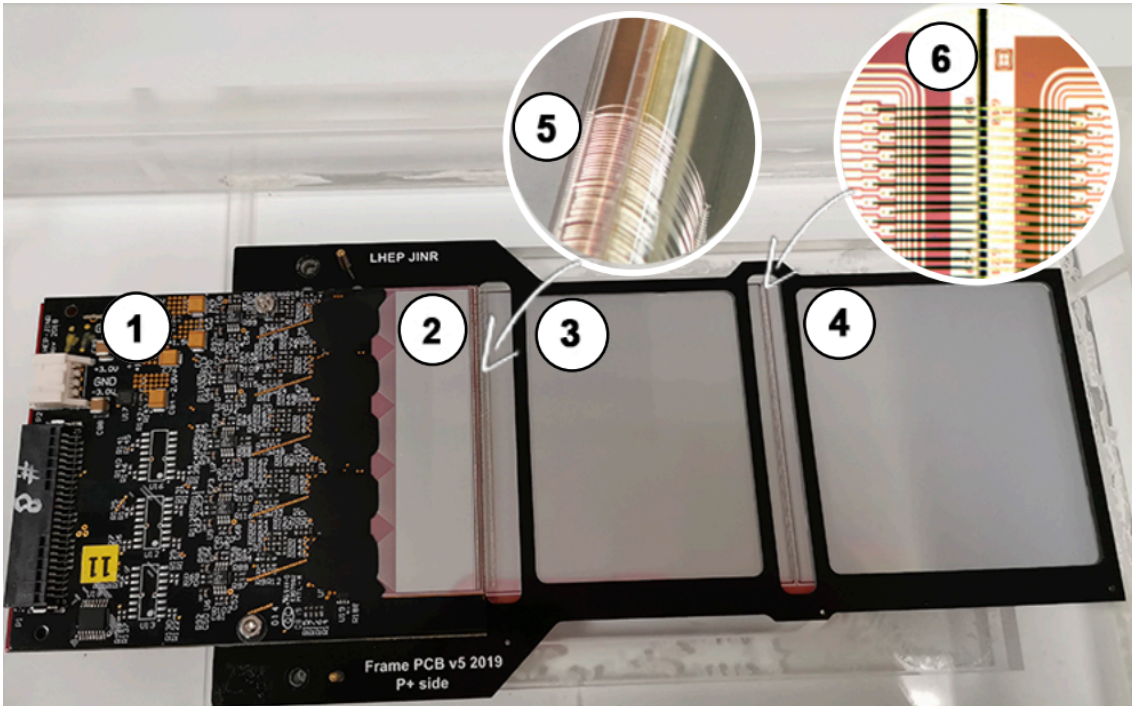


Figure 20: An example of a two-way US - bonding 2 - x DSSD on the FSD BM@N coordinate module

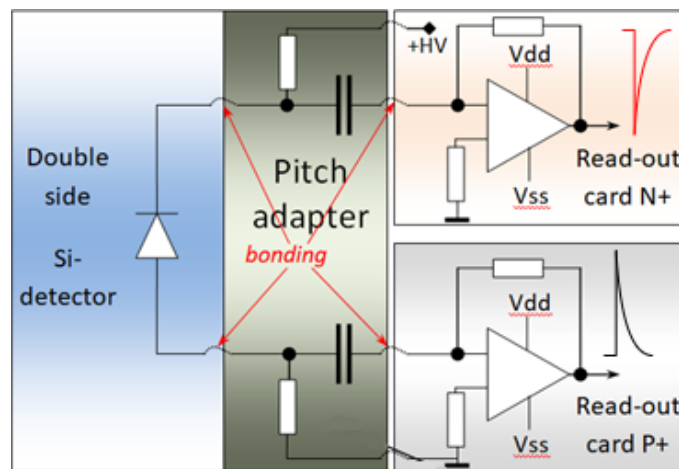


Figure 21: Functional diagram for reading signals from a silicon detector in a coordinate module

399 one of the most complex, because technological processes (growing thermal SiO₂, photolithography,
400 ion implantation, annealing, metallization, etc.) are carried out separately on two sides of silicon
401 wafers and usually with one detector placed on the wafer.

402 The module consists of two DSSDs with a sensitive area of $(63 \times 63) \text{ mm}^2$ each, mounted
 403 on a common frame with an accuracy of $(\pm 20 \mu\text{m})$, where the strips of the same name of one
 404 DSSD are connected to the strips of another DSSD by ultrasonic bonding (US-bonding) with an
 405 Al-wire $\varnothing 25 \mu\text{m}$. The detector topology (DC) does not contain integrated bias resistors and
 406 capacitors for DC decoupling of the strips from the inputs of the readout electronics. The role of
 407 the RC-bias element in the DC circuit is performed by the integrated Pitch-Adapter (PA), it also
 408 performs the matching of the strip pitch (pitch) with the topology of the pads of 128 inputs of
 409 the VATAGP7.2 chip. PA is made on the basis of SOS - structure (Silicon On Sapphire) contains
 410 integral capacitances and resistors. Each PA has 640 RC channels, polysilicon bias resistors are
 411 $1\text{M}\Omega$, and integral capacitors are $120\text{pF}/100\text{V}$. PA-640 integrated circuits manufactured at ZNTC
 412 have low leakage currents (less than $10\text{-}12 \text{ A}/\text{capacitor}/100 \text{ V}$) and an electrical breakdown value
 413 of 150 V , which corresponds to an electrical intensity in the capacitor of more than $3 \text{ MV}/\text{cm}$.

414 After PA, the signals from the p^+ and n^+ strips of the detector are fed to the inputs of a 128-
 415 channel specialized integrated circuit VATAGP7.1 (IDEAS, Norway). The value of the ionization
 416 loss signal (the maximum of the Landau-Vavilov distribution for $300 \mu\text{m}$ silicon) is $2.4 \times 10^3 \text{ e}$ (Q
 417 $= 4 \text{ fK}$, or $\Delta E = 86 \text{ keV}$). Each electronic registration channel consists of: charging amplifier (σ
 418 $= 200 \text{ e}$), shaper ($t_s = 500 \text{ ns}$), memory capacitor and analog multiplexer 128 inputs to 1 output.
 419 On each printed circuit board, 5 microcircuits are mounted, welded into pitch adapters and sealed
 420 with a compound, which register negative polarity signals from 640 n^+ strips and positive polarity
 421 signals from 640 p^+ strips.

422 After assembling the half-planes, for each of them, measurements of the true position of the
 423 detectors were carried out using the NORGAU NVM II-5040D video meter with an accuracy of
 424 $\pm 50 \mu\text{m}$. The coordinates of the detectors and their rotation relative to the outer base points of
 425 the half-plane body were determined. Geodetic markers were subsequently installed on these base
 426 points, the measurement of the position of which in space made it possible to bind the position of
 427 each detector to the common coordinate system of the installation

Plane number	number of modules	number of channels	problem chips, pcs.	problematic channels, pcs.	problematic channels, %
#1 (3×2)	6	7680	0/0	0/ 0	0 / 0
#2 (5×2)	10	12800	0/1	0/ 128	0 / 1
#3 (7×2)	14	17920	0/1	0/ 128	0 /0.71
#4 (9×2)	18	23040	4/8	512/1024	2.2/4.4

Table 5: Number of problem channels of FSD registration before/after session No. 8 BM@N

428 Table 5 shows the data (see Fig. 26) based on the results of tests in space (before the run) and
 429 after the run on the 124Xe beam ($3.8 \text{ GeV}/\text{n}$). Insensitivity on 128 channels=chip (dark bands in
 430 Fig. 14) may indicate the appearance of one of two defects:

- 431 - broken electrical contact in the transmission circuit from the chip (FEE buffer, cross-board
 432 connector, patch panel cable, long ADC-64 cable), this defect can be eliminated;
- 433 - failure of the chip (no programming of the operating mode), breakage of the US - bonding,
 434 this defect is unrecoverable.

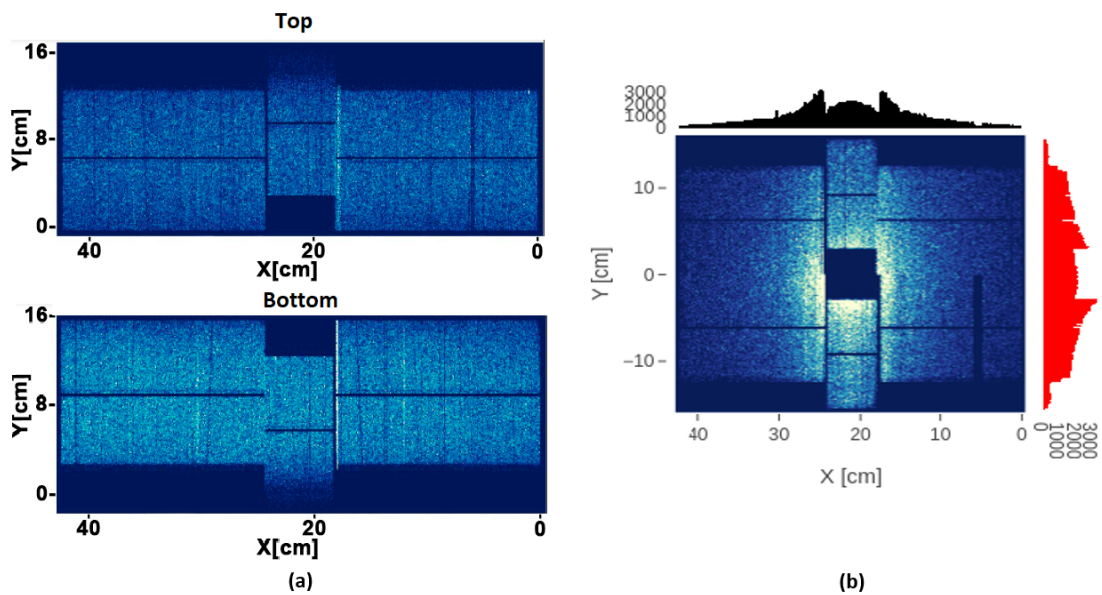


Figure 22: Comparative data on channel occupancy in space tests (a) and in Session BM@N (2022-2023) RUN # 7529 (11.01.2023), $t_c = 25.2^\circ\text{C}$, Target #2 CsI (2%) (b).

7 Forward Silicon Detector v2

Two large tracking detector systems placed inside the analysing magnet are the Forward Silicon Detector (FSD) located right behind the target area, and a set of GEM detectors installed downstream, inside the interpole volume. FSD provides four tracking planes, while the GEM system consists of seven tracking planes. In order to accommodate the beam vacuum pipe going through the setup, each tracking plane in both systems is sub-divided in two half-plane detectors, upper and lower. This section describes the details of the FSD.

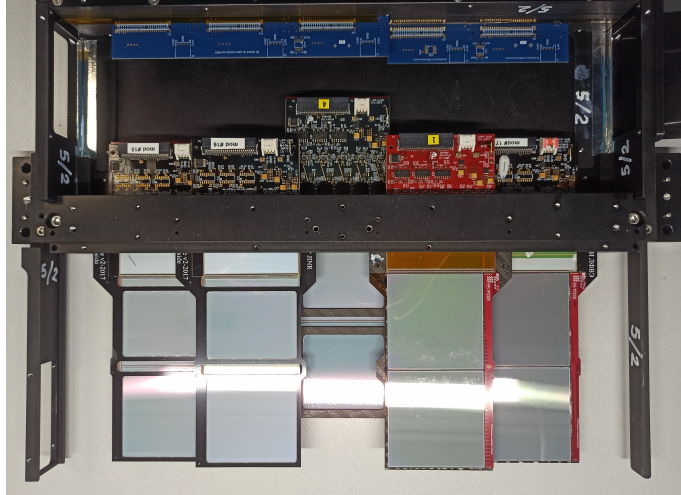


Figure 23: Appearance of the assembled 4 FSD planes (without cables) on the BM@N experiment channel inside the SP-41 analyzing magnet with the beam tube and target assembly installed.

Each half-plane of the FSD forms an independent coordinate detector with the following systems: coordinate modules based on DSSD, electronics backplane, suspension and precise positioning mechanics, cable patch panel, air cooling, temperature monitors, light and EM shield. Top and bottom halves of each plane are made structurally identical and interchangeable. In addition, the design allows vertical shift of the half-planes during the assembly in order to provide possibility to mount / dismount the planes regardless of the installed beam pipe and to minimize probability of its mechanical damage. In the working position, the upper and lower half-planes form a single coordinate system with active regions overlapping along the Y-coordinate. In the center of each plane there is an insensitive $52 \times 52 \text{ mm}^2$ zone (larger ???) which makes room for the beam pipe. The general view of the assembled eight half-planes around the beam tube inside the SP-41 magnet is shown in Fig. 23.

The first plane consists of 6 modules each of which uses one DSSD with dimensions of $(93 \times 63 \times 0.32) \text{ mm}^3$ positioned in such a way that the long side is aligned with the Y coordinate. The detector modules of the remaining three coordinate planes use two $(63 \times 63 \times 0.32) \text{ mm}^3$ DSSD mounted on a common frame with an accuracy of $(\pm 20 \mu\text{m})$, where the strips of the same type of one DSSD are connected to the strips of another DSSD by ultrasonic bonding (US-bonding) with an Al-wire $\varnothing 25 \mu\text{m}$. Figure 19 shows the position and coordinates of the Si detectors relative to the target and the axis of the beam pipe, while Table 6 provides information about the number of modules and electronic components in each FSD plane.

The $(63 \times 63 \times 0.32) \text{ mm}^3$ and $(93 \times 63 \times 0.32) \text{ mm}^3$ DSSDs were manufactured at RIMST (Zelenograd, Russia) and ZNTC (Zelenograd, Russia) respectively. The detectors were cut from 10" and 15" high-resistance mono-crystalline silicon wafers produced by the Float Zone method ($\rho > 5 \text{ k}\Omega \times \text{cm}$). Each side, p^+ and n^+ , contain 640 strips, the strip spacing is 95 and 103 μm , respectively, and the relative angle between the strips on two sides is 2.5° . The detectors are positioned in such a way that the strips of the p^+ side are aligned with the Y-axis.

Figure 24 shows the external view of the coordinate module with two DSSDs and a demonstration of US-bonding. The diagram of the signal input into FEE is presented in Figure 25. The detector topology (DC) does not contain integrated bias resistors and capacitors for DC decoupling of the strips from the inputs of the readout electronics. The role of the RC-bias element in the DC circuit is performed by the integrated Pitch-Adapter (PA), which also performs the matching of the strip pitch with the pad topology of inputs in the FEE ASIC. Manufactured also at ZNTC, the PAs were made on the basis of Silicon On Sapphire structure. Each PA has 640 RC channels with $1\text{M}\Omega$ polysilicon bias resistors and $120\text{pF}/100\text{V}$ integral capacitors. The PA-640 integrated

Parameters	1st plane	2nd plane	3rd plane	4th plane	Total
Number of Si- modules	6	10	14	18	48
Number of DSSDs	6 (93×63)mm ²	20 (63×63)mm ²	28 (63×63)mm ²	36 (63×63)mm ²	90
Number of ASICs ($T \leq +25^\circ$)	60	100	140	180	480
Dissipated power, W	16.86	28.16	39.42	50.69	135.13
Number of PAs	12	20	28	36	96
Number of FEE PCBs	12	20	28	36	96
Number of channels	7680	12800	17920	23040	53760
Area, m ²	0.035	0.073	0.102	0.132	0.307

Table 6: Main parameters of Forward Silicon Detector BM@N

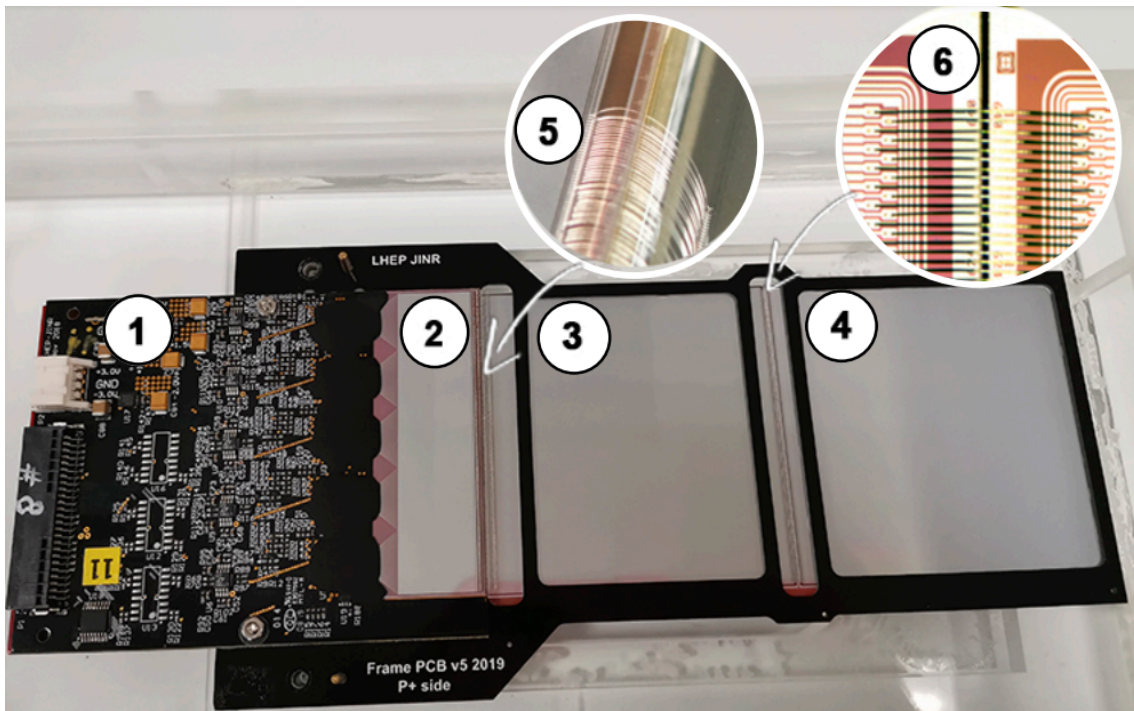


Figure 24: Example of two-way connection US – 2 – x DSSD on the FSD BM@N coordinate module: 1. Read-out electronics. 2. Peach Adapter. 3. DSSD1. 4. DSSD2. 5. Example of US - bonding PA + DSSD1. 6. Example of US - bonding DSSD1 + DSSD2.

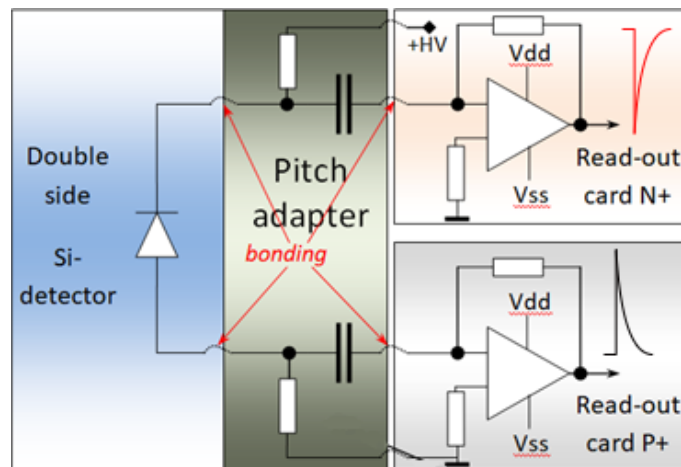


Figure 25: Functional diagram for reading signals from a silicon detector in a coordinate module

475 circuits have low leakage currents (less than 10-12 A/capacitor/100 V) and an electrical breakdown
 476 value of 150 V, which corresponds to electrical intensity in the capacitor of more than 3 MV/cm.

477 After passing the PA, the signals from the p^+ and n^+ strips of the detector are fed to the inputs
 478 of a 128-channel specialized integrated circuit VATAGP7.2 (IDEAS, Norway). (Is it VATAGP7.1
 479 or VATAGP7.2 ???). Each electronic registration channel has a charging amplifier ($\sigma - 200 e$), a
 480 pulse shaper (peaking time $t_s = 500$ ns), and a memory capacitor which stores pulse amplitude at
 481 the trigger time. The ASIC also uses an analog multiplexer channeling 128 inputs to 1 output sent
 482 to the read-out in the DAQ by ADC. Two printed circuit boards are used in each FSD module in
 483 order to accommodate its input signals, one for 640 negative polarity signals from n^+ strips, the
 484 other for 640 positive polarity signals from p^+ strips. Correspondingly, 5 ASICs are mounted on
 485 each PCB, welded into the pitch adapters and sealed with a compound.

486 After the assembly of the modules in a half-plane, the position and rotation angles of every
 487 DSSD with respect to geodetic markers on the half-plane housing is measured using the NORGAU
 488 NVM II-5040D video meter with an accuracy of $\pm 50 \mu\text{m}$. The markers are subsequently used
 489 during the installation in order to bind the position of each detector to the common coordinate
 490 system of the experimental setup.

491 Fig. 26 illustrates distribution of hits in the 4th plane of the FSD observed in the 2023 Xe run.
 492 Dark bands in the distribution indicate insensitive groups of 128 channels (1 chip). Number of
 493 such faulty chips at the end of the run was equal to 0, 1, 1, 8 for the 1st, 2nd, 3rd and 4th planes,
 494 respectively, which corresponds to 0, 1.0, 0.7 and 4.4 % of the channels. This malfunction can be
 495 due to the following reasons: 1) broken electrical contact in the transmission circuit from the chip
 496 (FEE buffer, cross-board connector, patch panel cable, long ADC-64 cable) 2) failure of the chip
 497 (no programming of the operating mode) or breakage of the US-bonding. Defects of the first type
 498 can be repaired, while the failings in the second group are of a permanent nature.

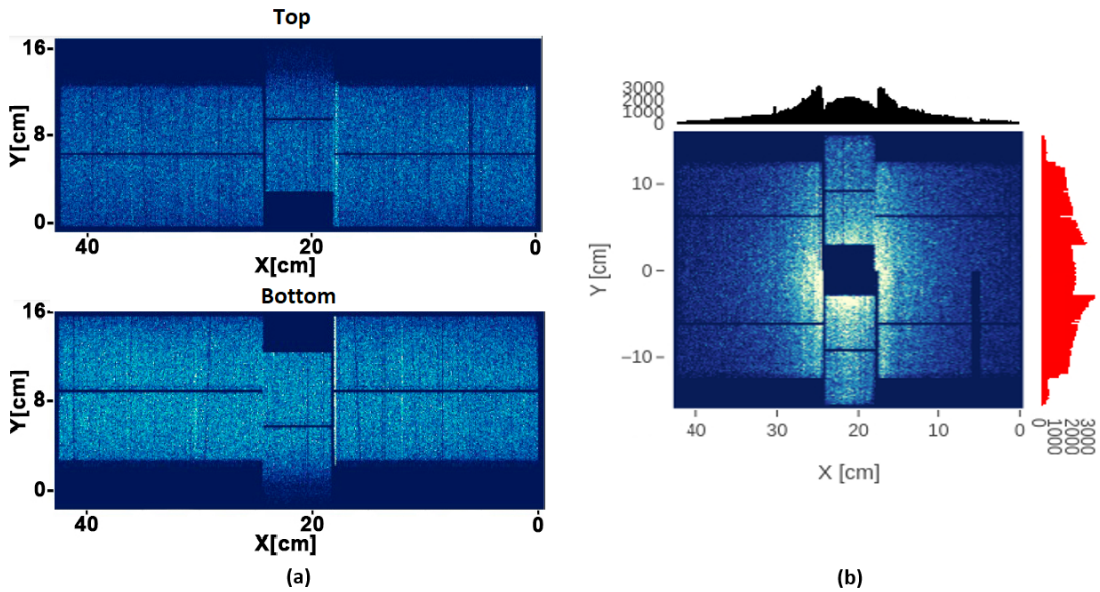


Figure 26: Comparative data on channel occupancy in space tests (a) and in Session BM@N (2022-2023) RUN # 7529 (11.01.2023), $t_c = 25.2^\circ\text{C}$, Target #2 CsI (2%) (b).

8 GEM

Central tracking system is based on triple GEM detectors. Detectors are located inside the analysing magnet SP-41 downstream the FwdSi detectors. Due to the design features of the BM@N channel, in order to cover the maximum possible acceptance within the aperture size of the analysing magnet, the GEM detectors have been designed with two different active area sizes: $163 \times 45 \text{ cm}^2$ and $163 \times 39 \text{ cm}^2$.

Full configuration of the tracking system based on GEM detectors consists of 14 GEM detectors: 7 GEM detectors of the size $163 \times 45 \text{ cm}^2$ – above the vacuum beam pipe (top GEM detectors), 7 GEM detectors of the size $163 \times 39 \text{ cm}^2$ – below the vacuum beam pipe (bottom GEM detectors). The detectors form 7 planes through which the vacuum beam pipe passes. (Fig. 1)

BM@N GEM detectors were produced at CERN (PH Detector Technologies (DT) and Micro-Pattern Technologies (MPT) workshop).

8.1 Construction of GEM detectors

The GEM technology and the design of the BM@N GEM detectors are described in detail in [13]. Two different sector designs of BM@N GEM detectors are described in [14].

8.2 Front-end electronics

Front-end electronics are based on the charge sensitive preamplifier chip VA163 (IDEAS). A detailed description can be found in [15].

8.3 Mechanical support

For the precise installation of GEM detectors inside the SP-41 magnet, a mechanical support was developed. During development, it was necessary to take into account a number of parameters. All elements of the mechanical support must be made of non-magnetic material. The support frames that will be located next to the GEM detectors must be made of non-conductive material. Dimensions of GEM detector equipped with front-end electronics are $10 \text{ cm} \times 182 \text{ cm} \times 47 \text{ cm}$ (bottom GEM detectors) and $10 \text{ cm} \times 182 \text{ cm} \times 52 \text{ cm}$ (top GEM detectors). The weight of one GEM detector equipped with mechanics, front-end electronics and cables is 19.5 kg. The detectors must be oriented strictly vertically. The whole assembly of 14 GEM detectors must be able to be vertically adjusted by $\pm 10 \text{ mm}$ relative to the surface of the magnet coil. Each GEM detector must have a vertical alignment of $\pm 5 \text{ mm}$ with respect to the mechanical support. The installation accuracy of each detector relative to each other should not exceed 0.5 mm. It should be possible to move the whole assembly of 14 GEM detectors along the carbon beam pipe installed inside the SP-41 magnet without dismantling the detectors.

Mechanical support was designed and manufactured by LLC “Pelcom Dubna Machine-Building Plant”.

Assembly of a mechanical support and installation of detectors on it consists of the following steps: 1) bottom detectors are installed sequentially, starting from the detector closest to the target; 2) a carbon beam pipe is installed on top of the bottom detectors; 3) top detectors are installed sequentially, starting from the detector closest to the target. Photo of installation process is shown in Fig. 27.

After each detector is installed, the front-end electronics are checked, a gas line is connected and detector is filled with gas mixture, high voltage is applied to the detector, and a radioactive source test is carried out. Then geodetic measurements of the position of the detector in a given coordinate system are made. At the same time, the detector goes through the adjustment procedure. The final results of the detector position measurements include coordinates of the corners of the detector and the center of the semi-circular notch for the beampipe. These values are necessary to correct the position of the detectors during the reconstruction.

The position and configuration of GEM detectors in Run 8 is shown in Fig. 28, Fig. 29.

8.3.1 Sequence of detectors in Run 8

To determine the sequence of GEM detectors in the magnet, the detectors were compared with each other. The number of unused channels and inefficient areas in the detectors were compared. Thus, the detectors that had regions of low efficiency in the side parts of the detector were installed closer to the target, where these regions are less significant for track reconstruction. Also, the top detectors with vertical sectors alternate with detectors with horizontal sectors.

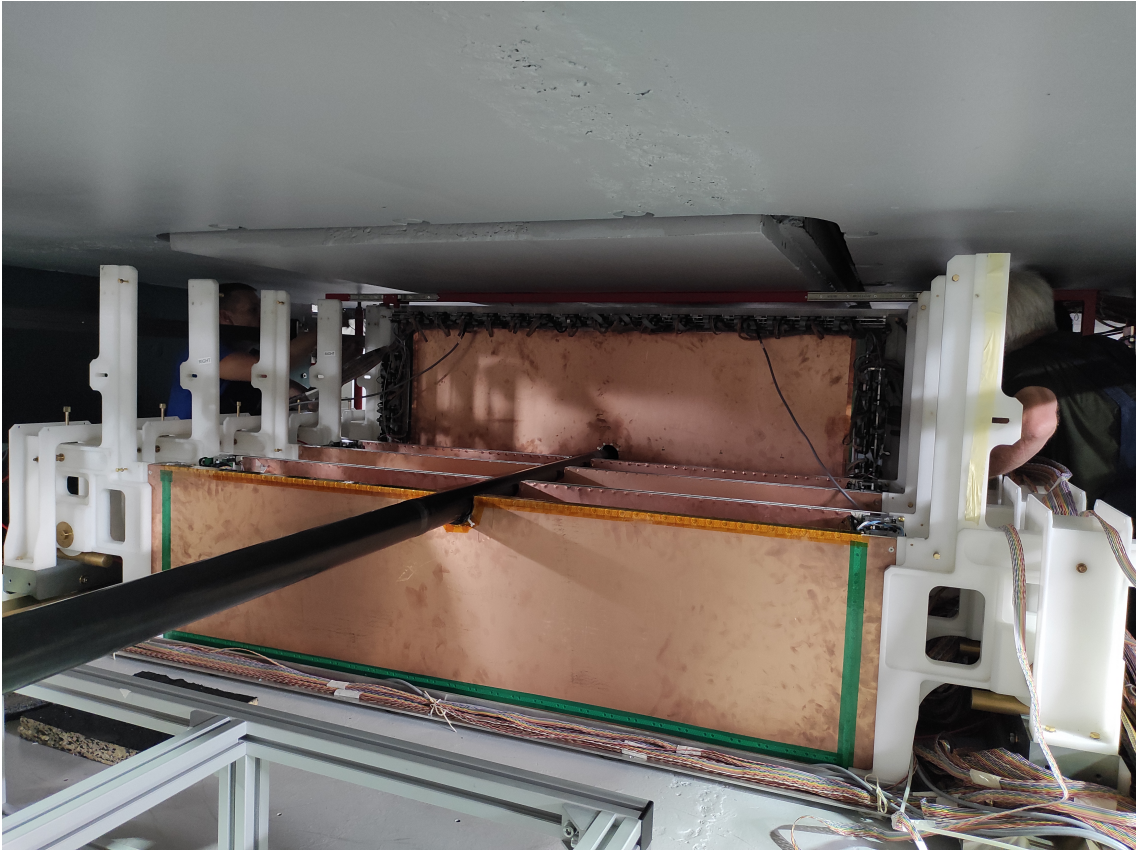


Figure 27: Photo of GEM detectors installation from back side of SP-41 magnet (in the direction opposite to the beam)

552 8.4 Gas system

553 GEM system was operated with gas mixture of Argon 80% and Isobutane (C_4H_{10}) 20%. The H_2O
554 and O_2 removal filter was connected in line after the gas mixer. The gas line was divided into two
555 identical lines for independent connection of the top and bottom GEM detectors. Two rotameters
556 were installed on the lines, allowing to regulate the gas flow. Each line connected a group of top or
557 bottom detectors in series, starting with the detector closest to the target. Small GEM detector
558 was connected last in the line for the bottom detectors. The gas flow rate in each line was 3 l/h.

559 8.5 Small GEM detector

560 Small GEM detector was used to monitor the position, shape and spot size of the beam passed
561 through the target and tracking system inside the analysing magnet. At the beginning of the Run
562 8, it was installed downstream the SP-41 magnet. And then, after adjusting the beam, it was
563 moved behind a large CSC, so as not to interfere with the installation of an aluminum beam pipe
564 downstream the SP-41 magnet. Small GEM detector is also consists of three GEM foils. The
565 size of the active area is 10 cm×10 cm. The readout has two coordinates and contains a set of
566 perpendicular strips of width ???. Number of channels of each coordinate is 256.

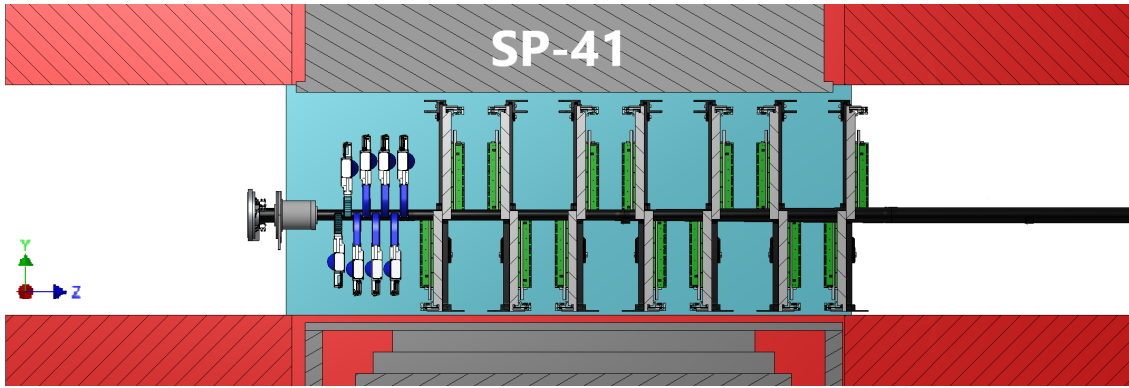


Figure 28: The position of GEM detector package relative to the magnet coil

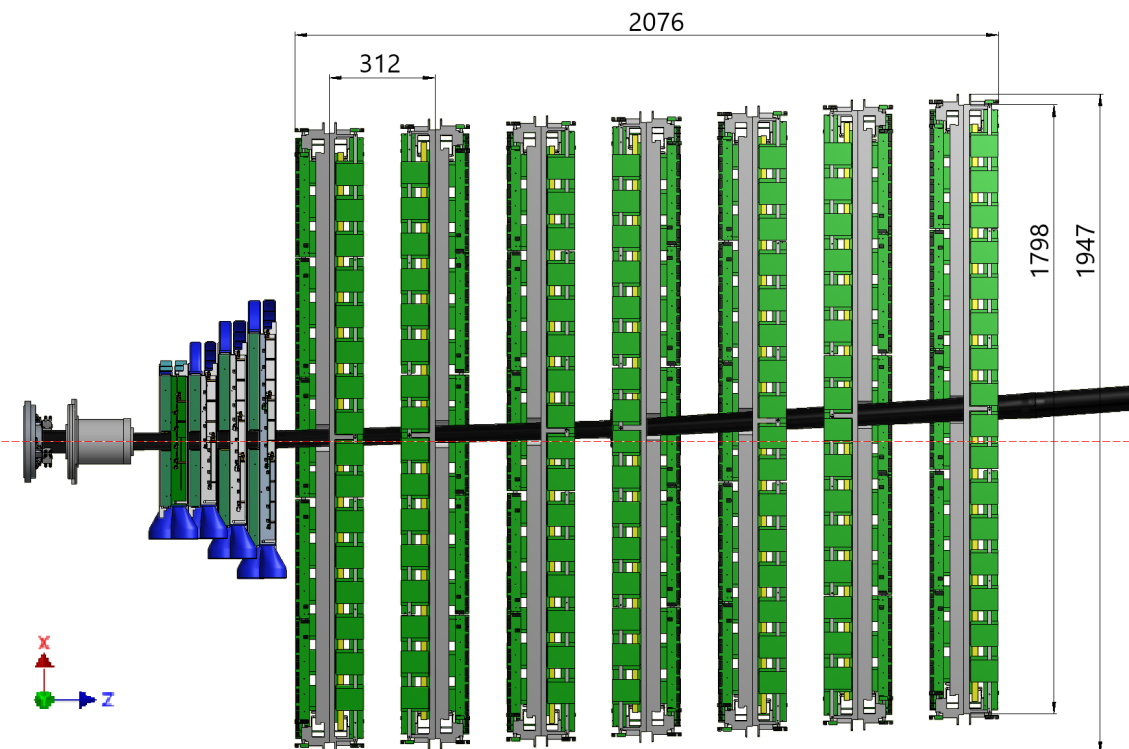


Figure 29: Displacement of detectors relative to each other due to beam pipe bending

568 **9 TOF**569 (*RumyantsevM.mikhail.rumyantsev@yandex.ru*)

570 For charge particle identification the two Time-of-flight systems are used in BM@N. The first
 571 TOF system is placed at about 4 meters from the target and looks like two arms to the left and
 572 right of beam axis (TOF-400). The second TOF wall (TOF-700) is located at a distance of **7 meters**
 573 from the target (fig 1). The arrangement of both systems provides continuous geometric acceptance
 574 and overlap with the external track systems. The basic requirements to the TOF system are:

- 575 - high granularity to keep the overall system occupancy below 15% and minimize efficiency
 576 degradation due to double hits;
- 577 - good position resolution to provide effective matching of TOF hits with tracks;
- 578 - high combined geometrical and detection efficiency (better than 85%);
- 579 - identification of pions and kaons with $0.1 < p_t < 3 \text{ GeV}/c$;
- 580 - identification of (anti)protons with $0.3 < p_t < 5 \text{ GeV}/c$

581 To achieve these goals, a strip-readable Multigap Resistive Plate Chamber (MRPC) detector
 582 was chosen for both TOF systems. This type of detectors is widely used for time-of-flight measure-
 583 ments (ref....). It showed good efficiency, high time resolution, the ability to work with particles
 584 flux up to tens kHz/cm^2 .

585 **9.1 TOF400**

586 The TOF400 system consists of two parts placed left and right to the beam. Every part consist
 587 of two gas boxes (modules) with 5 MRPCs each (fig...). The active area of the MRPCs **overlap on**
 588 **50 mm** inside the box. Gas box made from aluminum frame covered by aluminum honeycomb for
 589 reduction of radiation length. Overlap of gas boxes ensures crossing of active area of detectors 50
 590 mm also. Active area of every part is $1.10 \times 1.3 \text{ m}^2$ and defined to satisfy the geometrical acceptance
 591 of the GEM tracking detectors. The main parameters of the TOF400 are present in Table 7.

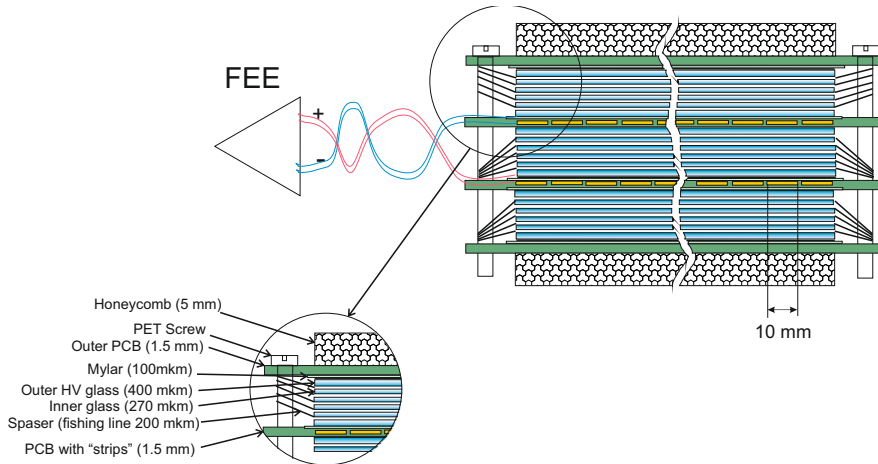


Figure 30: Schematic view of the MRPC detector for TOF400 system

592 A scheme of MRPC for TOF400 system is shown on Fig. 30. The detector consists of three
 593 stacks of 5 gas gaps each. Float glass with a thickness of $420 \mu\text{m}$ for external electrodes of the
 594 stack and $240 \mu\text{m}$ for internal ones was used as resistive electrodes. The fishing line as a spacer
 595 defines the $200 \mu\text{m}$ gap between all resistive electrodes. The outer part of external glass electrodes
 596 is covered by conductive paint with surface resistivity about $2\text{-}10 \text{ M}\Omega/\square$ to apply high voltage. All
 597 internal glasses are floating. The pickup electrodes look like strips and made on the PCB board.
 598 The main feature of the proposed triple-stack MRPC is that readout strips are located only in the
 599 inner stack. This ensures that the construction is symmetric, and speed of signals on the anode

600 and cathode are the same, what prevent the dispersion of the signal. Differential analog signal
 601 from strip is transferred by twisted pair cable to front-end electronics. Signal is reading out from
 602 both ends of the strip. It provides better time resolution and determination of the coordinate of a
 603 particle along the strip. For stiffening structure we glue paper honeycomb with a thickness of 10
 604 mm on outer part of the external PCBs. Dimension of active area of one MRPC is 300*600 mm².
 605 It has 48 readout strips, 10 mm wide and 300 mm long. To reduce crosstalk the gap between strips
 606 is 2.5 mm. Thus the pitch of electrodes in this case is 12.5 mm.

607 The charge sensitive NINO chip was used for TOF400 [15]. The chip has 8 channels and processed
 608 on 0.25 μm technology. Each channel includes ultra-fast preamplifier with a peaking time less
 609 than 1 ns, discriminator with a minimum detection threshold of 10 fC and output stage which
 610 provides LVDS output signal. The duration of the LVDS signal is proportional to the charge
 611 of the input signal, so it can be used for so-called amplitude-time correction. The 24-channel
 612 amplifier-discriminator base on NINO chip was developed in LHEP JINR [16]. Measurements with
 613 a test signal from the generator showed an intrinsic time resolution of the amplifier of 7 ps. The
 614 amplifier are placed as close to the MRPC as possible on front cover of the gas box. The signal
 615 from the preamplifier can be transmitted over a distance of up to 10 m via a special cable without
 616 loss of time resolution. Additional features of the FEE are the ability to remotely control the
 617 threshold, measure the supply voltage and temperature on the board via the RS485 interface.

618 72-channel time-to-digital converters (TDC72VHL [17]) based on HPTDC chip [18] were developed
 619 in LHEP JINR for digitization of LVDS signals and data acquisition. The TDC72VHL operates in
 620 ultra high resolution mode with a binning of 23.4 ps. This allows to measure the leading and trailing
 621 edges of the input LVDS signal with high accuracy, but there is significant integral non-linearity at
 622 the TDC. This nonlinearity causes strong degradation of time resolution. The method of uniform
 623 filling the time gap with random events (code density test) was used for calibration (consideration
 624 of nonlinearity) of TDC module. The intrinsic time resolution of an individual TDC72VHL channel
 625 averaged 20 ps after applying the calibrations.

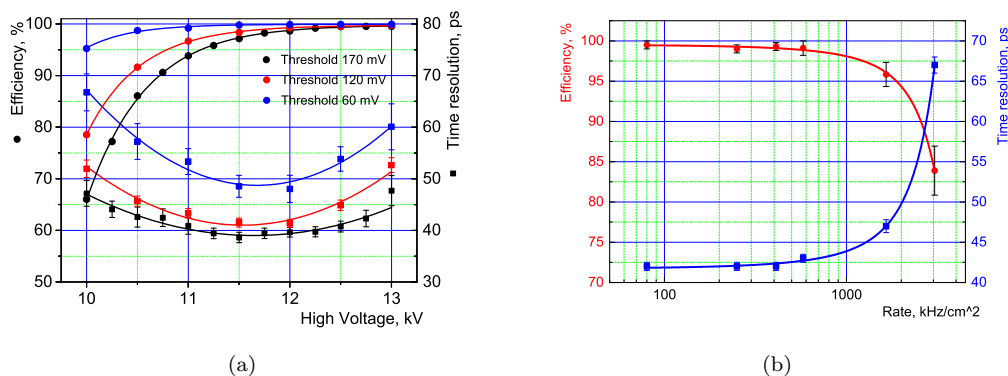


Figure 31: Performance of the MRPC designed for TOF400 system. The detector efficiency and time resolution as function of applied of HV for different NINO thresholds are shown on the left. The right shows the dependence of the detector performance on the particle flux for 11.5 kV and 120 mV threshold.

626 The prototype of full scale MRPC with full readout chain was tested on the Nuclotron beam
 627 at LHEP. The deuteron beam was transferred to the experimental setup “Test MPD” [19]. The fast
 628 Cherenkov counter [20] with time resolution of 37 ps was used as a start detector. The result of
 629 measuring the efficiency and time resolution are present on the Fig. 31a . All results include
 630 contributions from the front end and data acquisition electronics. The efficiency is higher than
 631 98% and time resolution is below 50 ps for different threshold of NINO. A voltage of 11.5 kV and a
 632 threshold of 120 mV were chosen as the operating point. Results of high rate test are presented on
 633 Fig. 31b. MC simulations show that the particle flux on the TOF400 does not exceed 1 kHz/cm²,
 634 so a time resolution of less than 50 ps and an efficiency of more than 95% are expected.

9.2 TOF700

636 The TOF700 wall placed at about 7 meters from the target and made of MRPC of different size,
 637 in an individual gas box each. The wall size of 3.2x2.2 m² is defined to satisfy the geometrical
 638 acceptance of the outer tracking detectors (DCH). The detectors are mounted on two subwalls in

639 two layers on each to provide a geometric overlap between the detectors. Both sub walls can move
 640 relative to each other to provide access for installation and maintenance. Two types of detectors
 641 are used for TOF700: a "cold" MRPC with an active area of $30.3 \times 56 \text{ cm}^2$ (16 strips of 18×560
 642 mm^2) for the area with a low particle flux and a "warm" MRPC with an active area of 16×35.1
 643 cm^2 (32 strips $10 \times 160 \text{ mm}^2$) for the area near the beam line. The main parameters of the TOF700
 644 are present in Table 7.

645 A schematic cross-section of a "cold" MRPC is shown in Fig. 32. It consists of two identical
 646 stacks with five gaps each. Each stack is formed by six glass plates 0.67 mm thick with the bulk
 647 resistivity of $2 \times 10^{12} \Omega \times \text{cm}$. The gap between the glasses 0.3 mm is fixed by spacers (fishing-lines).
 648 Graphite conductive coating with surface resistivity of $1 \text{ M}\Omega/\square$ is painted to outer surfaces of
 649 external glass plates to distribute both the high voltage and its ground. The anode readout plate
 650 is a $100 \text{ /}\mu\text{m}$ one-sided printed PCB and is placed between stacks. Unipolar signals are taken
 651 from both ends of the reading strips, which makes it possible to determine the coordinate of the
 652 particle along the strip. Each detector is placed in an individual gas box. The bottom cover is
 653 made of PCB 2.5 mm thick and is designed to take out a signal from the box volume to readout
 654 electronics. The frame of the box is made of aluminum 2.5 mm thick. The top cover is made of 1.5
 655 mm thick aluminum sheet. The box covers are reference plan for a unipolar signal. Warm MRPC
 656 is built in the same way as cold mRPC. However to increase the ate capability the gas gaps and
 657 the thickness of the glass plates are reduced (0.22 mm and 0.55 mm respectively). To compensate
 658 for the loss of the signal amplitude due to the increasing of the anode strip-cathode capacity, the
 659 number of gaps in the chamber was increased from 10 to 12 (six gaps per stack).

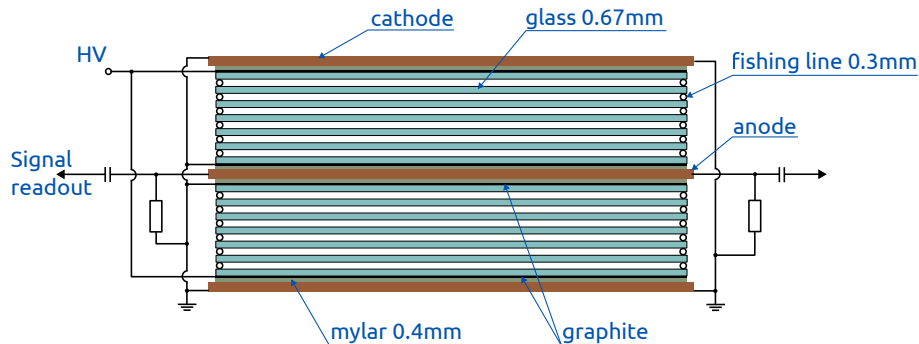


Figure 32: Schematic view of the MRPC detector for TOF700 system

660 The AddOn board base on NINO chip developed for the HADES experiment was chosen as
 661 front-end electronics (FEE) for TOF700. Signals from the MRPC to the FEE (32RPC) are received
 662 over 50 ohm coaxial cables using MMCX connectors. The LVDS output signals are transmitted
 663 to the digitizing module using DHR-78F connectors. A 64-channel VME TDC64VHLE time-
 664 to-digital converter based on the HPTDC chip is used for digitization. With a special module
 665 (PWR&CTRL) it is possible to remotely control the power supply, the discrimination threshold
 666 and hysteresis value on the FEE.

667 Prototypes of "cold" and "warm" detectors were tested on the secondary muon beam of the
 668 U-70 accelerator at IHEP. The test was carried out on the "MUON" facility with a particle flux
 669 of about $1 \text{ kHz}/\text{cm}^2$. A fast scintillation counter with its own time resolution of 40 ps was used as
 670 T0. The test results of both prototypes are shown in the figure 33. The intrinsic time resolution
 671 of the MRPCs with electronics is better than 45 ps with an efficiency of 98% and 95% for "cold"
 672 and "warm" chambers respectively.

673 9.3 Services system

674 Both TOF400 and TOF700 systems use the same a non-flammable Freon rich gas mixture contain-
 675 ing $90\% \text{ C}_2\text{H}_2\text{F}_4 + 5\% \text{ i-C}_4\text{H}_{10} + 5\% \text{ SF}_6$. A simple open-loop gas system was designed for the
 676 BMN experiment. This system is based on the MKS 1479A controllers for measuring and adjusting
 677 the absolute flow of components with an accuracy of 0.3% . The flow rate of the gas mixture can
 678 be adjusted in the range from 6 l/h to 90 l/h , but the typical value is 21 l/h , which corresponds
 679 to the exchange of 2 volumes per day. Also, one additional channel is available for purging the
 680 system with nitrogen for cleaning and drying. A special PC program has been written to control
 681 the parameters of the gas system via the Ethernet interface.

682 The MRPC detector operates at very high voltage of 12 kV and 15 kV for TOF400 and TOF700
 683 respectively. On the other hand, the dark currents of the detector are quite small at the level of

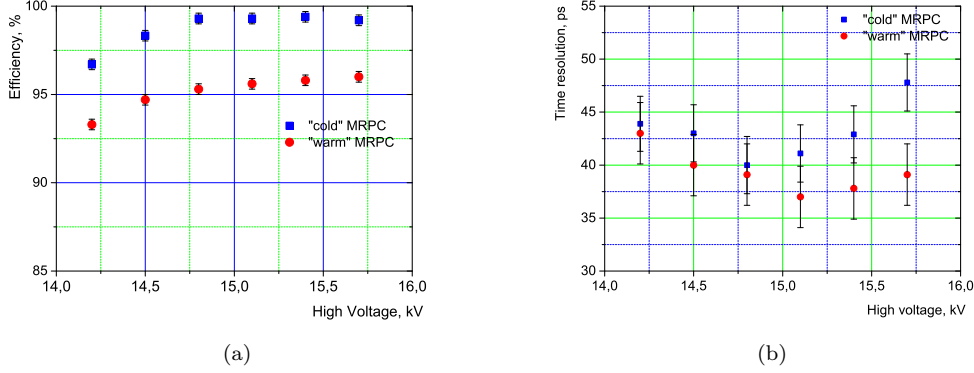


Figure 33: Performance of the MRPC designed for TOF700 system. The detectors efficiency are shown on the left and time resolution are shown on the right.

	TOF400	TOF700
MRPC active area	30x60 cm ²	30.3x56 cm ² "cold" 16x35.1 cm ² "warm"
FEE on one MRPC	96	32 for "cold" 64 for "warm"
Number of MRPC	20	30 "cold" 40 "warm"
Total active area	2 Arms x 1.1x1.3 m ²	3.2x2.2 m ²
Total number of FEE	1920	3520

Table 7: Main parameters of TOF system.

684 tens of nA. Also, the detector is very sensitive to voltage ripples due to the large capacitive coupling
685 between the high-voltage layer and the readout strips. Therefore, the high-voltage system is subject
686 to high requirements for voltage stability and current measurement accuracy. The high-voltage
687 power supply systems for both TOF are based on commercially available ISeg modules and a
688 specially designed HVSys power supply. All elements of the system have the ability to remotely
689 control via Ethernet interface.

690 To monitor of stability of operation of the TOF systems all controlled parameters are sent to
691 the Slow Control System. The data is displayed on the website of the experiment via Grafana.
692 The operator can see the value of the high voltage and current on the detectors, the set voltages
693 and thresholds of the amplifiers, the gas flow and the weight of the gas in cylinders, and other
694 parameters. In case of an emergency, the operator receives a message that allows to respond in
695 time. All data is stored in a database and can be used for further analysis.

696 **10 Outer tracker**

697 The purpose of the outer tracker is to provide link between tracks measured in the central tracker
 698 and hits in the ToF-400 and ToF-700 detectors. In the Run 8 outer tracker consisted of two large
 699 aperture drift chambers (DCH), four CSC (cathode strip chamber) with the size of the active area
 700 of $1129 \times 1065 \text{ mm}^2$ and one plane of $2190 \times 1453 \text{ mm}^2$ CSC (see Fig. 1).

701 **10.1 DCH**

702 The drift chambers [16] have an octagonal shape with a transverse width of 2.9 m. (Fig. 34).

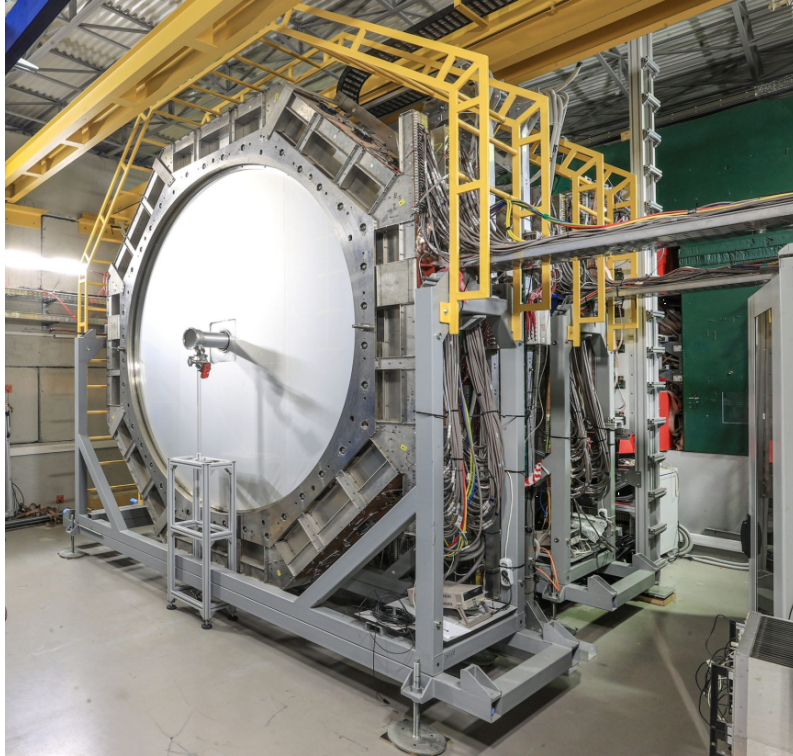


Figure 34: DCH integrated into BM@N experimental setup.

703 Their fiducial area is about 4.5 m^2 . Every drift chamber (DCH) consists of 4 double coordinate
 704 planes with the following parameters: the wire inclination angles of 0° , 90° , $\pm 45^\circ$, the wire pitch
 705 of 10 mm, the outer dimensions of the sensitive area of $Y_{\text{out}} \pm 1.2 \text{ m}$, $X_{\text{out}} \pm 1.2 \text{ m}$, the beam
 706 hole radius of $R = 160 \text{ mm}$, 256 wires per coordinate plane, 2048 wires per chamber.

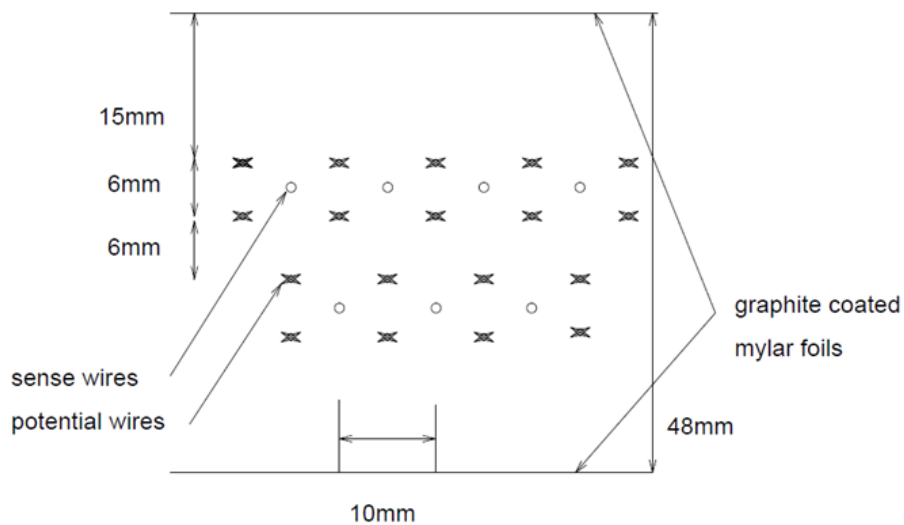


Figure 35: Drift cell geometry of the DCH.

707 To minimize multiple scattering effects, the wire chambers are constructed with minimal amount
708 of material along the beam direction. A schematic view of the geometry of one view is shown in
709 Fig.35. Sense wires have a diameter of $20\ \mu\text{m}$ and made of gold-plated tungsten. The electric field
710 is created by applying a negative voltage on two planes of gold-plated Ti-Cu wires located on each
711 side of the sense wire planes, at a distance of 3 mm. The field wires have a diameter of $120\ \mu\text{m}$.
712 The spacing between sense and field wires on a plane is 10 mm. Thin Mylar foils ($22\ \mu\text{m}$) coated
713 with graphite are used to shape the electric field in the drift cell and also to act as separating walls
714 between two consecutive views.

715 A readout time measurement accuracy of about 1 ns with no deadtime is achievable with
716 specially designed amplifiers and TDC circuits [17]. The anode signals in the wire chambers
717 are amplified, discriminated and transformed to logic pulses in electronic circuits located on the
718 chambers. The output pulse is a logic 50 ns wide ECL pulse with 50 ns deadtime following the
719 pulse, achieved by a delay element.

720 The granularity of DCH is sufficient to perform measurements of interactions with light ions
721 (up to Ar). The DCH wire occupancy in interactions of middle and heavy nuclei is too high to
722 perform efficient track separation. Thus, the DCH will be replaced by cathode strip chambers
723 (CSC) to perform track measurements in middle and heavy nucleus collisions.

724 10.2 CSC

725 The full configuration of the outer tracking system for heavy ion program will consist of four
726 planes of $1129\times 1065\ \text{mm}^2$ CSC (cathode strip chamber) and two planes of $2190\times 1453\ \text{mm}^2$ CSC.
727 The CSC detectors are situated outside the magnetic field with the aim to make precise link to
728 the tracks, reconstructed in the GEM detectors inside the analyzing magnet. Tracks refined in
729 CSC are used to improve particles momentum reconstruction and to find corresponding hits in the
730 time-of-flight systems ToF400 and ToF700.

731 The first CSC detector with the size of the active area of $1129\times 1065\ \text{mm}^2$ was designed and
732 assembled at LHEP JINR in 2018. It consists of an anode plane located between two cathode
733 planes (see Fig. 36). The anode plane is a set of gilded tungsten wires with the diameter of $30\ \mu\text{m}$
734 which are fixed on the plane with a step of 2.5 mm. The gap between the anode plane and
735 each cathode plane is 3.8 mm. Two-coordinate readout of the signal is performed on two cathode
736 PCB boards using sets of parallel metal strips. The inclination angles of the cathode strips to the
737 vertical axis are 0 degrees (X coordinate) and 15 degrees (Y coordinate). The pitch of the X and
738 Y strips is 2.5 mm. PCBs are glued to the support honeycomb. Due to a large multiplicity of
739 charged particles in Au-Au collisions, readout layer is divided into outer (cold) and inner (hot)
740 zones.

741 First beam tests of the $1129\times 1065\ \text{mm}^2$ CSC were performed in 2018 at the argon beam
742 with kinetic energy of 3.2 AGeV and the krypton beam with kinetic energy of 2.3 AGeV at the
743 Nuclotron. The CSC was installed upstream the ToF-400 time-of-flight detectors. The main goal
744 of the tests was to study the performance of the CSC detector and the FEE and readout electronics
745 as a part of the BM@N experimental setup. The signal clusters were reconstructed as groups of
746 adjacent strips with amplitudes of signals above the threshold. For the reconstructed clusters, the
747 center of gravity, the width and the total charge were calculated. The average cluster width is 6
748 strips which is equal to 15 mm. The gap size between the anode and cathode is reduced to 3 mm
749 instead of 3.8 mm in order to improve the spatial resolution in multitrack events.

750 All four CSC detectors with the size of the active area of $1129\times 1065\ \text{mm}^2$ and one detector
751 CSC with the size of $2190\times 1453\ \text{mm}^2$ were integrated into the BM@N setup in the physical run
752 2022-2023 with the Xenon beam at the kinetic energy of 3.8 AGeV at the Nuclotron

753 Two CSCs of the size $2190\times 1453\ \text{mm}^2$ have been designed to cover the ToF-700 system on both
754 sides and replace the existing drift chambers (DCH). The design of these cathode strip chambers
755 is shown in Fig. 37. One cathode plane consists of 8 PCBs, each PCB is divided into hot and cold
756 zones. The hole in the center of the chamber is designed for the vacuum beam pipe. The gap size
757 between the anode and cathodes is planned to be 3 mm. Two-coordinate readout of the signal
758 is performed using sets of parallel metal strips with the inclination angle of 0 degrees for the X
759 coordinate and 15 degrees for the Y coordinate. The pitch of the X and Y strips is 2.5 mm.

760 10.2.1 Front-end electronics

761 Front-end electronics is based on the same charge sensitive pre-amplifier chip VA163 as used for the
762 GEM detectors. The multiplexed data from each board are transmitted through the twisted pair

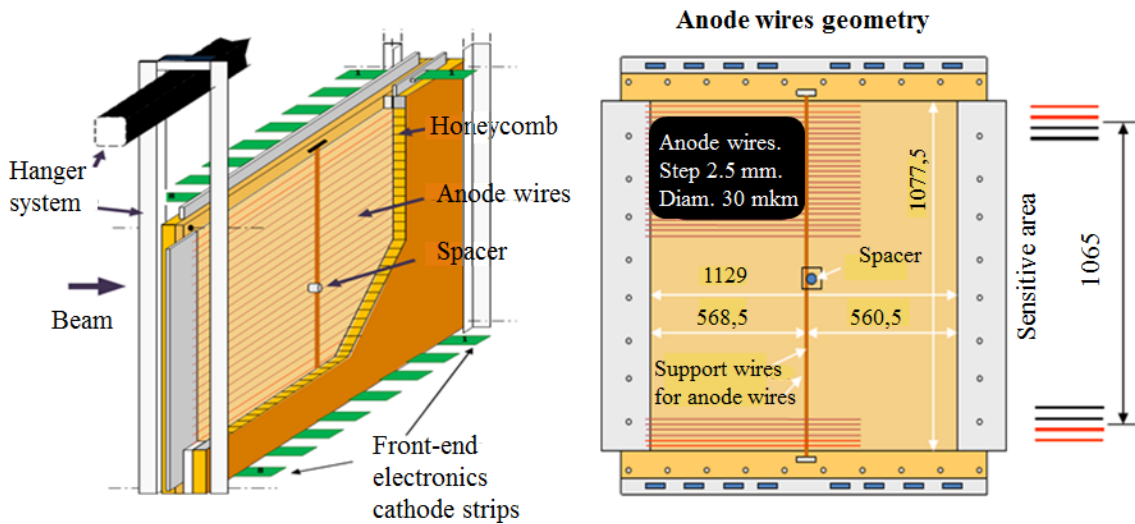


Figure 36: Schematic view of the $1129 \times 1065 \text{ mm}^2$ CSC

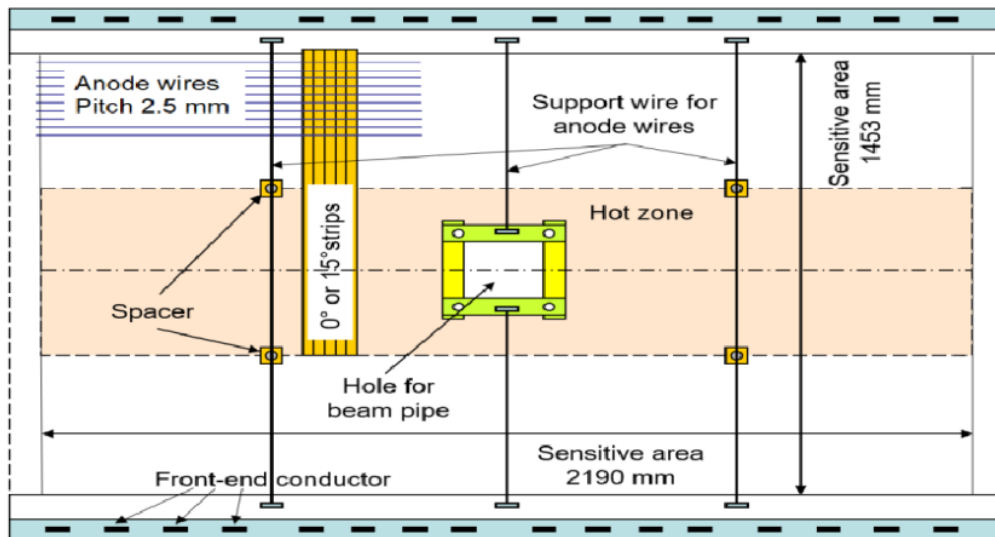


Figure 37: A technical drawing of the cathode strip chamber of the size $2190 \times 1453 \text{ mm}^2$ (15-degree strips are not shown in this picture).

763 flat cable to the 12-bit analog-to-digital converter (ADC) readout by the BM@N data acquisition
 764 system.

765 The full configuration with 6 CSC detectors equipped with the electronics based on VA-163
 766 chips (35000 readout channels) is planned to be integrated into the BM@N experimental setup at
 767 the 2023.

768 10.2.2 Gas distribution system

769 The outer tracker were operated with $\text{Ar}(75\%) + \text{C}_4\text{H}_{10}(25\%) / \text{C}_3\text{H}_8\text{O}$ (vapor) gas mixtures.
 770 The gas system (Fig. 38) consists of two parts: 1) the mixer system which delivers a mixture of
 771 gases in a required ratio and pressure to downstream elements; 2) the distribution system, which
 772 delivers the gas in well defined quantities to the individual detectors.

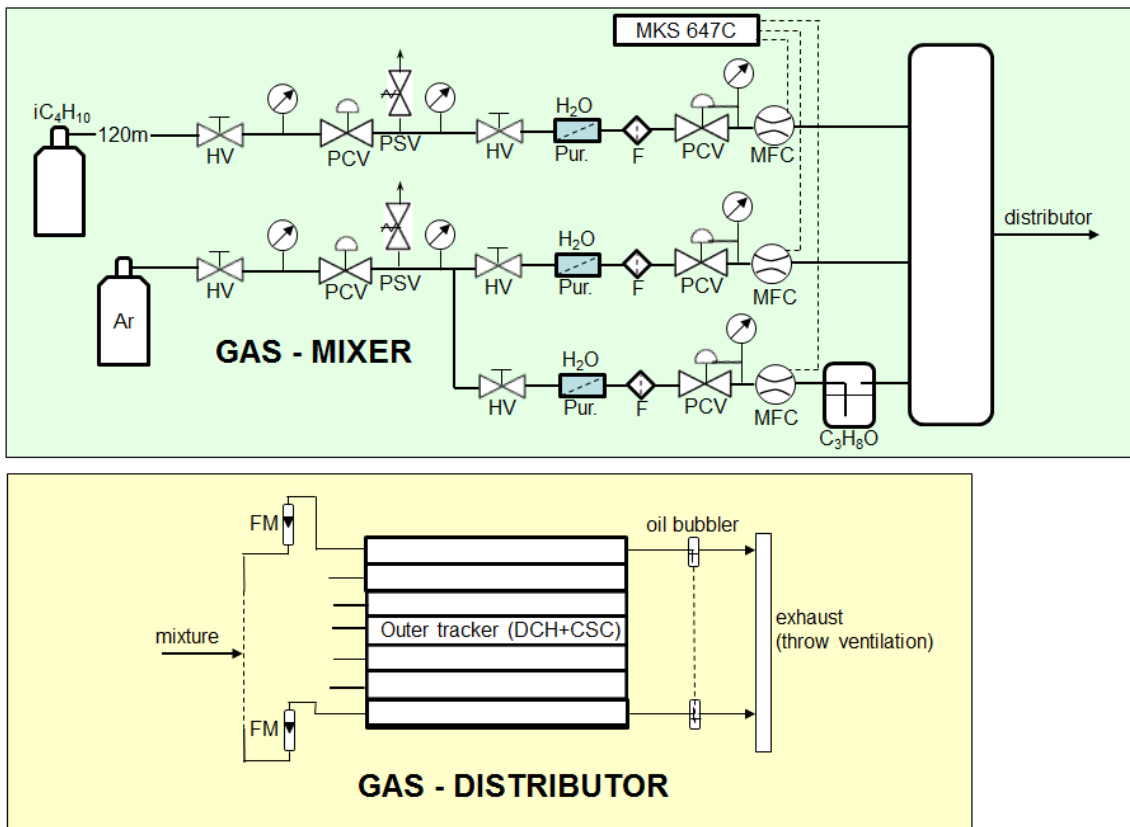


Figure 38: The gas line for the outer tracker. The layout of the mixer module: HV – on/off valve, PCV – pressure control (constant) valve, PSV – pressure safety valve, Pur. – Purifier (H₂O and O₂), F – filter, MFC – mass flow controller (MKS Instruments firm), MKS 647C – power supply and readout (MKS Instruments firm). Component layout of the distributor module: FM – flowmeter (manually flow adjustment), oil bubbler – pressure and air protection.

11 Forward Spectator Detectors

The new forward detectors for measuring the energy (FHCAL) and charges (FQH, ScWall) of projectile spectators produced in the nucleus-nucleus collisions in the BM@N experiments have been developed and constructed during last few years. They are located at the very end of the BM@N facility (see Fig. 1). These detectors are used to determine the centrality and orientation of the reaction plane. Moreover, ScWall and FQH can be used also to study the charge distributions of spectator fragments produced in the nucleus-nucleus interactions. The rapidity coverage of these forward detectors is shown in Fig. X1.

(fig. X1 -- one picture for all detectors ?)

11.1 Forward Hadron Calorimeter (FHCAL)

The forward hadron calorimeter FHCAL has a granular structure in the transverse and longitudinal planes. It consists of 54 separate modules which provides transverse granularity of the FHCAL. Internal part of the FHCAL consists of 34 small modules with transverse sizes of $15 \times 15 \text{ cm}^2$ and a length equivalent to 4.0 nuclear interaction lengths. These modules are identical to the modules of the forward hadron calorimeters of the Multi-Purpose Detector (MPD) experiment at the NICA accelerator complex [8]. Two outer lateral parts of the calorimeter consist of 10 large modules on each side with transverse sizes of $20 \times 20 \text{ cm}^2$ and a length equivalent to 5.6 nuclear interaction lengths. These modules were initially constructed for the hadron calorimeter of the Compressed Baryonic Matter (CBM) experiment (FAIR, Darmstadt, Germany) [9] and are temporarily used in the hadron calorimeter of the BM@N experiment in accordance with mutual agreement between BM@N and CBM collaborations. Schematic view of the FHCAL is shown in Fig. 39, left. At the center of the calorimeter there is a hole with transverse size $15 \times 15 \text{ cm}^2$. Noninteracted beam ions pass to a beam dump located behind the calorimeter through this hole. It is necessary to protect internal modules of the calorimeter against high radiation dose and strong activation in experiments with heavy ion beams.

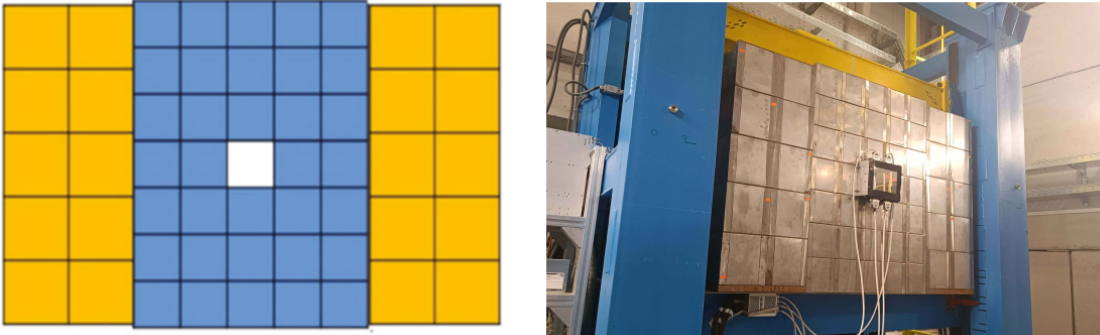


Figure 39: Schematic view of the FHCAL, left. Photo of the FHCAL with FQH installed on the the movable platform (blue) at the BM@N, right.

FHCAL modules have sampling structure and consist of lead/scintillator layers with a sampling ratio of 4:1 (the thickness of the lead plates and scintillator tiles are 16 mm and 4 mm, respectively) and provide compensation condition ($e/h=1$) for the hadron calorimeter [??]. Small modules have 42 lead/scintillator layers and large modules have 60 such layers. To get rather hard rigidity of the lead plates they are made of lead-antimony alloy. An assembly of 60 (42) alternating layers of scintillator and lead plates are tightened into one package with a 0.5 mm thick stainless steel band using a special tensioning mechanism. The tape is welded with spot welding to the steel plates inserts installed in the beginning, middle and end of the package (Fig. 40). Behind the tightening mechanism the block of boron polystyrene with thickness 10 cm is installed in large modules. Once the package is assembled, it is closed by an upper box of 0.5 mm thick stainless steel sheet.

The scintillator plates are made from polystyrene-based plastic scintillators produced by Uni-plast (Vladimir, Russia). Light from each scintillator plate is collected by wavelength shifting optical fiber KURARAY Y-11(200) glued into groove with depth 1.2 mm on the surface of the scintillation plate and transported to the end of module. The grooves in scintillators of large modules have circular form, while grooves in scintillators in small modules are spiral. Outside of the scintillator plate fibers are placed in thin black plastic pipes to be optically shielded and are

814 stacked in parallel on the top surface of the module package. All scintillators with glued fibers are
 815 wrapped in Tyvek reflector.

816 The end of each fiber glued in the scintillator plate is coated with reflective paint. At the
 817 end of the module the optical fibers from each of the six consecutive scintillation plates in the
 818 module are glued into individual optical connectors, which are placed on a panel mounted in the
 819 module box. Thus, each of large modules has ten longitudinal sections and each of small modules
 820 has seven sections. The longitudinal segmentation provides high homogeneity of light collection
 821 along modules, a large dynamic range of the calorimeter response and makes it possible to perform
 822 energy calibration of FHCAL with cosmic muons [10].

823 This panel with ten optical connectors for large module (seven optical connectors for small
 824 module) has an additional optical connector for LED light distribution system. LED pulses are
 825 distributed with ten (seven) optical fibers into each section optical connector. Light pulses from
 826 the LED allow to control the operation of the photodetectors used for light readout.

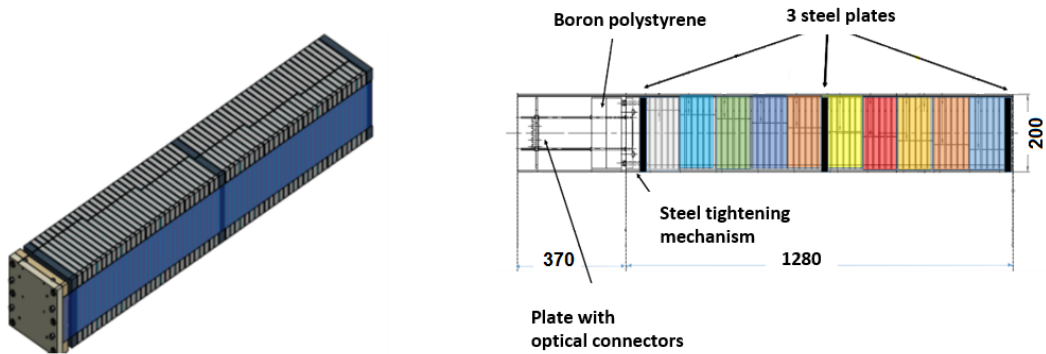


Figure 40: Left - 3D view of the large calorimeter module in assembly. Right - scheme of large module, here 10 sections are shown in different colors.

827 The weight of each small module is about 200 kg and weight of large module is about 500 kg.
 828 Total weight of the FHCAL is about 17 tons. It is mounted on the special platform shown in blue
 829 color on Fig. 39, right, which is able to move FHCAL in X-Y directions.

830 11.1.1 FHCAL photodetectors, FEE and readout electronics

831 ~~At present~~, Hamamatsu MPPC S12572-010P with $3 \times 3 \text{ mm}^2$ sensitive area are used as photodetec-
 832 tors for light detection from the sections of the FHCAL. These photodetectors have gain 1.35×10^5
 833 and photon detection efficiency about 10% at peak sensitivity wavelength 470 nm. Due to very
 834 small pixel pitch - 10μm - the total number of pixels is 90000 which is important to provide
 835 the linear response in wide dynamic range of the signal. FHCAL Front-end-electronics (FEE) is
 836 composed of two separate PCBs. Ten (seven) photodetectors are installed on a first PCB directly
 837 connected with light connectors at the end of each large (small) module, Fig. ??, left. A temper-
 838 ature sensor is mounted near photodetectors on aluminum heat sink. The second PCB contains
 839 signal preamplifiers with differential ADC driver output and individually adjustable voltage regu-
 840 lation circuits for the photodetectors, Fig. ??, center. This board has also LED flash generation
 841 circuit with synchronization input and analog sum signal output. All FEE boards are remotely
 842 controlled via specially designed HVSys System Module manufactured in JINR (Dubna, Russia).

843 There are 438 calorimeter sections, which are needed to be readout. Eight ADC64s2 [??]
 844 boards, produced at JINR (Dubna, Russia) are used for signal readout. They have 64 channel
 845 12-bit ADCs with sampling rate of 62.5 MHz and memory depth of up to 1024 points per channel.
 846 The ADC64s2 boards have Lemo connectors for trigger and Xoff signals, and are capable of time
 847 synchronization via White Rabbit network, providing per-channel zero suppression function with
 848 adjustable threshold and can operate in self-triggered or externally triggered modes. FHCAL ADCs
 849 are fully integrated into the BM@N data acquisition system which provides trigger signals, busy
 850 logic, White Rabbit network and data readout. Power for FHCAL ADCs is provided by a remotely
 851 controlled power supply units placed in Wiener crate.

852 Custom 12-channel analog sum modules (adders) with individually adjustable attenuation have
 853 been constructed. These adders are used to sum up the analog outputs from FHCAL modules. They
 854 are used when performing standalone cosmic calibrations in central DAQ. The adders can be used
 855 for integration into the BM@N trigger system.

856 **11.1.2 FHCAL calibration with cosmic muons, energy resolution and linearity of the**
857 **response**

858 Since muon beams are unavailable at the BM@N setup, energy calibration of the FHCAL can only
859 be performed using cosmic particles. Longitudinal and transverse segmentation of the calorimeter
860 allows for track reconstruction [10], which was used to compensate for track length variation in
861 the scintillator tiles due to varying track orientation of the cosmic particles. Cosmic calibrations
862 parameters show 40 - 50 photoelectrons per one muon per one section.

863 A detailed study of the linearity of response and energy resolution for array of 9 large modules
864 has been performed on protons with kinetic energy range 1 - 9 GeV at the CERN T9 and T10
865 beamlines [11]. The good linearity and $0.54/\sqrt{E}$ energy resolution was obtained.

866 **11.2 Forward Quartz Hodoscope (FQH)**

867 The FHCAL beam hole is covered with beam hodoscope - Forward Quartz Hodoscope (FQH). The
868 main goal of the FQH is measuring charges of spectator fragments which miss the calorimeter in
869 order to estimate the collision centrality with combined FHCAL and hodoscope response. The FQH
870 consists of 16 strips - cherenkov detectors - with sizes of $16 \times 1 \times 0.4\text{cm}^3$ (see Fig. 41, left) inside
871 light tight box. Each FQH detector has light readout with two individual silicon photo-multipliers
872 mounted on opposite sides of the strip (see Fig. 41, right).

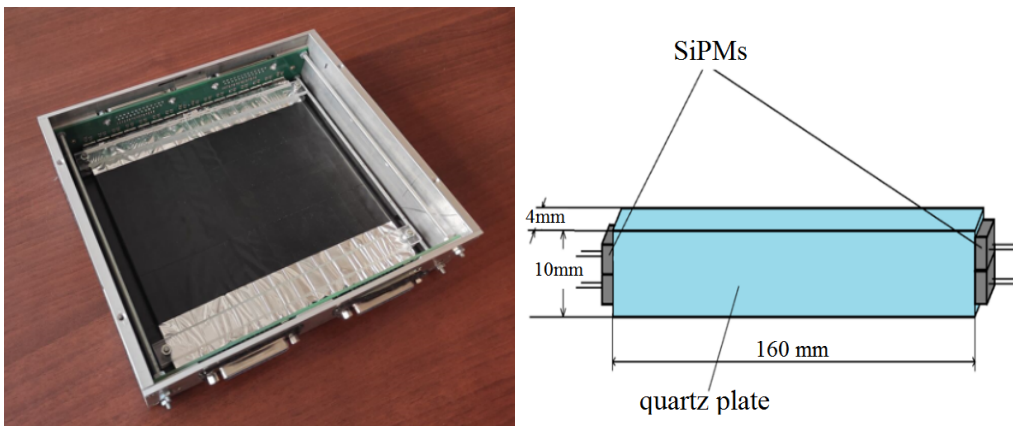


Figure 41: Left: photo of Forward Quartz Hodoscope - FQH (inside view). Right: picture of the FQH strip with SiPM photodetectors mounted.

873 One Front-End-Electronic (FEE) board reads eight channels. Total number of FEEs are four
874 for full FQH. The FQH installed in front of the beam hole of FHCAL is shown in Fig. 39 (right).
875 Four FEE boards of FQH are connected to the control box with amplifiers installed at bottom side
876 of FHCAL.

877 Hamamatsu MPPCs S14160-3015PS with $3 \times 3 \text{ mm}^2$ sensitive area and PDE of 32% are used
878 as photodetectors. Four TQDC-16 boards [?] with total 64 channels are used to read-out the
879 two-gain outputs from each photodetector. The gains are 1x and 4x. Low gain channel is used
880 for maximum dynamic range up to the highest ion charge expected. High gain channel is used for
881 low-Z fragments. Charge calibration of FQH strips is performed with pure beam ions.

882 **11.3 Scintillation Wall (ScWall)**

883 The ScWall is the large area detector aimed for measuring the charged particles in forward rapidity.
884 It consists of array of scintillating plates placed in the aluminum box. The polystyrol-based scintil-
885 lators are manufactured at “Uniplast” (Vladimir, Russia). ~~There are two sizes of scintillators: big~~
886 ~~cells of $15 \times 15 \times 1\text{cm}^3$ at peripheral area and small ones of $7.5 \times 7.5 \times 1\text{cm}^3$ in the central part.~~
887 ~~The view of the ScWall is shown in Fig. 42. The full detector size is $270 \times 120\text{cm}^2$. The ScWall has~~
888 ~~40 inner small cells and 138 big outer cells. In order to avoid heavy-ion beam radiation damage~~
889 ~~the very central part has $15 \times 15\text{cm}^2$ beam hole (see Fig. 42).~~

890 The light in the cells is collected by WLS Y11(200) S-type (Kuraray) [?] fibers mounted
891 in 1.5mm deep grooves (see Fig. 43) and detected by SiPM Hamamatsu S13360-1325CS with
892 $1.3 \times 1.3\text{mm}^2$ active area, gain of 7×10^5 and PDE of 25%. The measured light yields of big cells
893 and small cells are about 32 p.e./MIP and about 55 p.e./MIP, respectively [?]. The full area of
894 ScWall is divided into 12 read-out zones and performed with ADC64s2 board combined with FEE

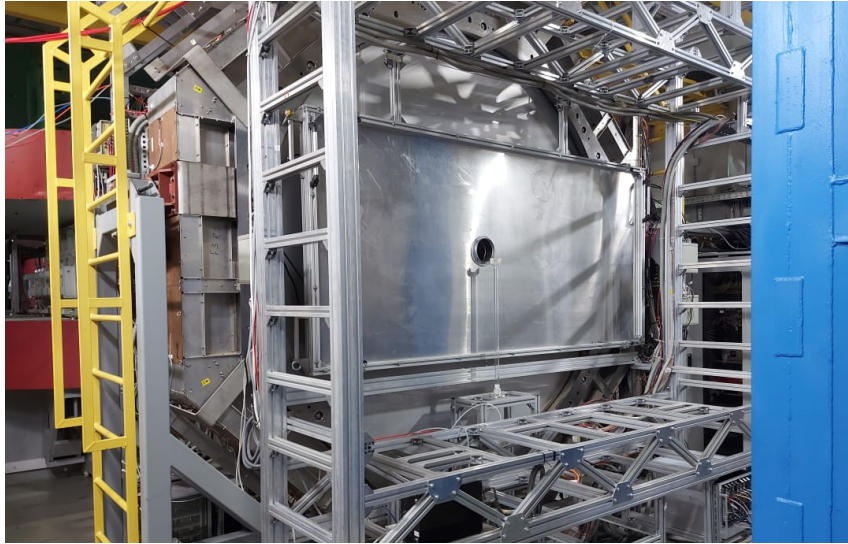


Figure 42: The view of ScWall detector with the beam hole.

boards. Three ADC64s2+FEE boxes are used to read full ScWall. The calibration of ScWall cells
 has been performed on cosmic muons as well as on $Z=1$ charge particles coming from the ion-ion
 reaction.

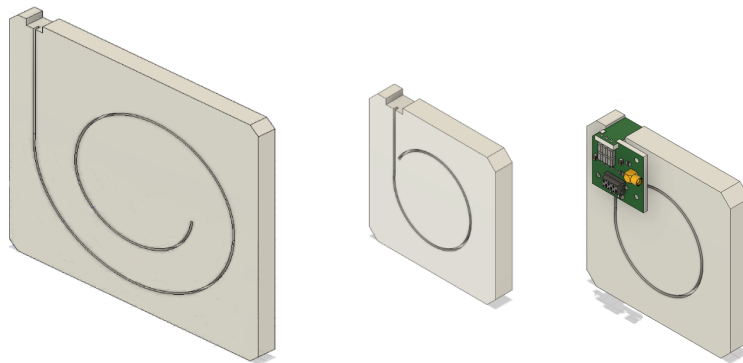


Figure 43: From the left to the right: schematic view of large ScWall cell, schematic view of small ScWall cell, schematic view of small cell assembly with SiPM on PCB board with connectors.

11.4 Slow Control for forward detectors

The FHCAL, FQH and ScWall have SiPMs as light detectors. In order to control and monitor bias voltage (HV) applied to SiPMs and the temperature the new Slow Control system has been developed. The hardware part of Slow Control is designed and constructed by “HVsys” (JINR, Dubna). HV power supply modules have multi-channel HV supplies with micro-controller interface. Schematic view of Slow Control system is shown in Fig. 44. Each HVsys system module has a unique IP-address for communication through individual proxy-server. Communication of HVsys box with FEE micro-controllers is done with RS-485 interface. All proxy-servers have connections to GUI panel to control and monitor status and to perform temperature correction for all SiPMs. The software part of the Slow Control is written on python3 [12].

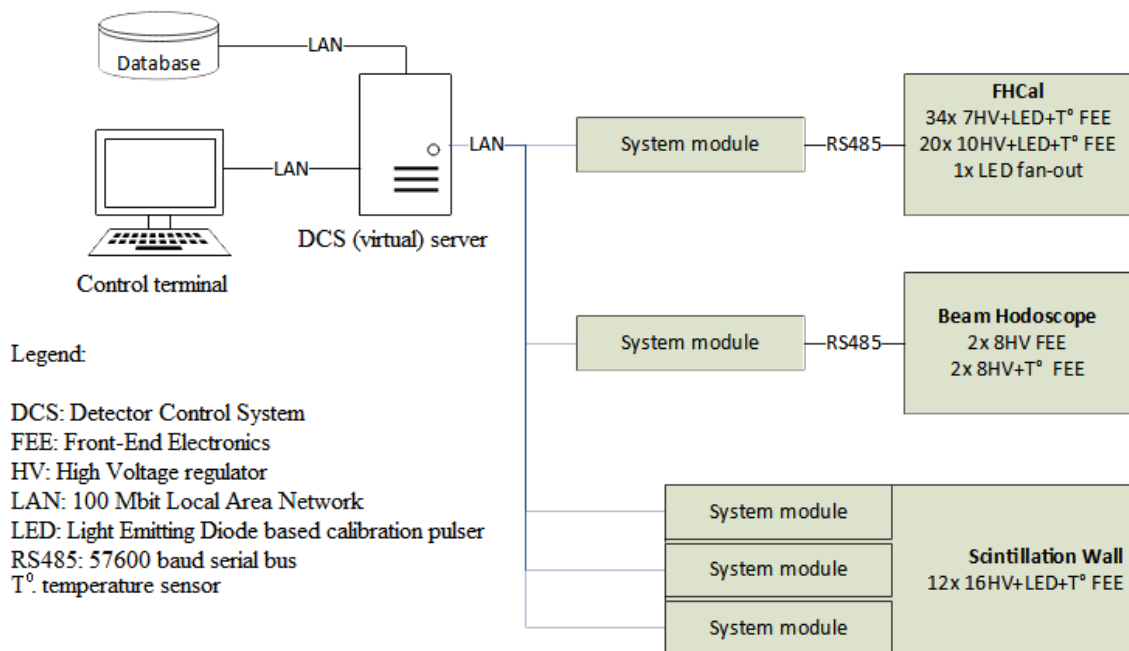


Figure 44: The Slow Control system for forward detectors at BM@N.

908 **12 Trigger**

909 BM@N trigger consists of hardware and software parts. The hardware part includes detectors on
 910 fast plastic scintillators, low- and high- voltage power suppliers, programmable trigger logic unit
 911 T0U, trigger control unit CAEN N6742. The software part include a graphic trigger interface,
 912 trigger performance and beam quality control.

913 A beam trigger BT formed by the signal coincidence from beam couters BC1, BC2 under
 914 condition the signal absence from the veto counter VC:

$$BT = BC1 \times BC2 \times VC(veto)$$

915 A minimum bias trigger MBT asks only for a low amplitude signals in forward counter FD,
 916 which corresponds to the beam particle interaction in a space between BC2 and FD counters:

$$MBT = BT \times FD(veto)$$

917 The interaction trigger called Central Collision Trigger (CCT) composed of the minimum bias
 918 trigger and the multiplicity in the barrel detector:

$$CCT = MBT \times BD(> N)$$

919 All the triggers mentioned above (BT, MBT, CCT) are send in the output data stream with
 920 the corresponding scaling factor.

921 Trigger decision formed by the programmable logic controller T0U and its logic organisation is
 922 shown in Fig. 45.

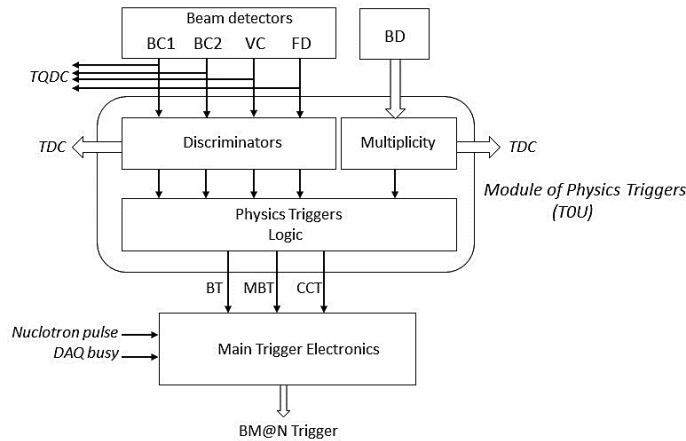


Figure 45: Trigger logic.

13 BM@N DAQ: Hardware Architecture

The core function of the DAQ system is realization of data transfer from the detector to the storage system. It includes the data flow from readout electronics to the First Level Processor (FLP) fabric, to the Event Building (EB) and to the Storage System. Main DAQ components are readout electronics modules, clock and time synchronization system, trigger distribution system, data transfer networks, data processing servers and online storage system (*link-to-tdr*). The general architecture is sketched in Fig. 46.

Detector Readout Electronics (DRE) boards record detector signals. There are two main types of DRE boards grouped by function: Timestamping Time to Digital Converters (TDC), Waveform Digitizers or Amplitude to Digital Converters (ADC).

13.1 TDC DRE board

TDC DRE board performs time-stamping of discrete signals (hits) with typical accuracy of $20ps$. It is based on HPTDC chip. Hit timestamps are kept for $51\mu s$ in ring type memory. The total trigger latency should not exceed this value. ADC DRE board is a waveform digitizer. It quantize analogue input signal and samples it at fixed time intervals. Zero suppression logic is based on baseline estimation and threshold value. Signal shaping can be performed in digital form with FIR filters. It allows to reduce the number of waveform points required for digital signal representation with minimum loss of accuracy. The ring type memory allows the read back of last $32\mu s$ of waveforms. It sets the limit on trigger latency to this value. TQDC DRE board combines both TDC and ADC functions.

13.2 MSC16VE module

MSC16VE is 16-channel multievent scaler (Fig. 48). Each channel input has 50Ω impedance and accept signals of $\pm 2.5V$ range and discrimination threshold can be adjusted in $\pm 1V$ range. Module has 4 LVTTTL count enable (CE) inputs. Ethernet 1000BASE-X connection is used for data readout and module control. Module MSC16VE has three main logic parts: input part, multi-event data readout and hardware histograms. Input part has crosspoint switch that allows any input channel to be processed by any multi-event counter and histogram. CE and Gate logics have 16 independent Look-Up Tables (LUT) each. Gate logic determines reset conditions for hardware histograms. Multi-event counters data continuously splits into numbered time slices and pushes to data encoder and further to Ethernet. Time slices length is adjustable with minimum length of $64 ns$ and $8 ns$ step. Data encoder perform zero suppression and data packing. Hardware histograms are used for online monitoring of input hits. Time series histograms store hits distribution in time. Time interval histograms store time interval between two adjacent hits in channel. Both hardware histograms readout by request from control software.

13.3 Timing System

White Rabbit provides sub-nanosecond accuracy and picosecond precision of time synchronization for distributed systems. DRE boards digitize detector signals using common notion of time and frequency provided by the White Rabbit (WR) network. The time reference is provided by GPS/GLONASS receiver and backup precision frequency reference (Rubidium clock). Digitizer boards require precise reference clock for high precision measurements. Timestamping TDCs used in T0, TOF400, TOF700 detector electronics have time resolution of $25ps$, DCH-100ps. DRE boards include White Rabbit Node Core and tunable crystal oscillators that are synchronized to reference clock with $10ps$ accuracy. WR node core provides local clock and timestamp at 125 MHz. The timestamp is specified as TAI (International Atomic Time). It is an absolute number of seconds and nanoseconds since 01.01.1970. Frequency dividers synchronized by 1 PPS (Pulse per Second) signal are used to produce digitizer clocks: 41.667 MHz for HPTDC ASICs and 62.5 MHz for waveform digitizers.

13.4 Trigger distribution system

BM@N trigger system has tree structure and 3 trigger levels: L0, L1 and L2.

972 **13.4.1 General architecture of trigger distribution system**

973 L0 is fast trigger signal for front-end electronics with latency of $150ns$. L1 trigger signal is readout
 974 trigger candidate generated by TRC module (see 13.4.2), according to its internal logic. Formation
 975 time of L1 trigger is adjustable and was $\tilde{1}\mu s$ in BM@N run 8. L2 trigger, produced by UT24VE
 976 module (see 13.4.3), starts data readout for all subsystems. All signals are transmitted via coaxial
 977 cables in LVTTTL standard. Trigger-Busy handshake algorithm for L2 trigger was implemented to
 978 guaranty all triggers delivery to all subsystem. This algorithm is shown in the Fig. 49. Rising edge
 979 of trigger signal (1) leads to rising edge of busy signal (2). After that trigger signal is deasserted (3).
 980 Upon completion of data collection, the subsystems deassert busy signals (4). Typical subsystems
 981 busy time shown in the Fig. 50.

982 **13.4.2 TRC – Trigger Control**

983 TRC (TRigger Control) module was designed for BM@N run 8. Main goal of this module is
 984 production of readout trigger candidates (L1) according to its configurable logic. T0 unit is used
 985 as source for input signals (“physical” triggers BT, CCT, MBT, etc.). Each of 16 input channels has
 986 individual settings: input delay, hits downscaling factor and before/after protection. Before/after
 987 protection logic used for pile-up rejection and secondary hits rejection during detectors dead time.
 988 L1 trigger candidate output delay can be adjusted in range of $8 ns$ to $100 \mu s$. TRC module produces
 989 L0 trigger for GEM, CSC, FSD and BT front end electronics, as they required fast (less then 300
 990 ns) data latch signal. Different conditional counters for input physical triggers are implemented
 991 in TRC module.

992 **13.4.3 LTU - Logical Trigger Unit**

993 LTU is main module for L2 trigger generation and distribution system. The module ensures the
 994 operation of Trigger-Busy handshake algorithm (Fig. 49) and can process up to 16 busy channels.
 995 Busy signals can be received from DRE modules or hierarchically lower LTU modules. Time
 996 intervals between accepted triggers and busy signals duration are histogrammed in LTU internal
 997 memory. Various trigger counters are also implemented in module.

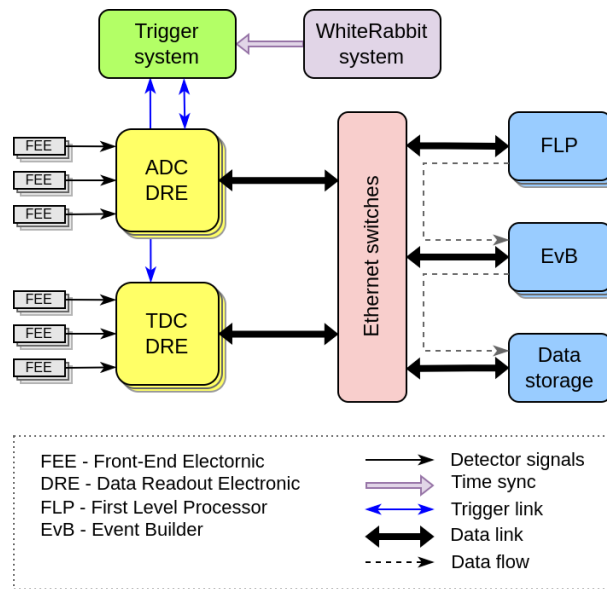


Figure 46: General architecture of DAQ system

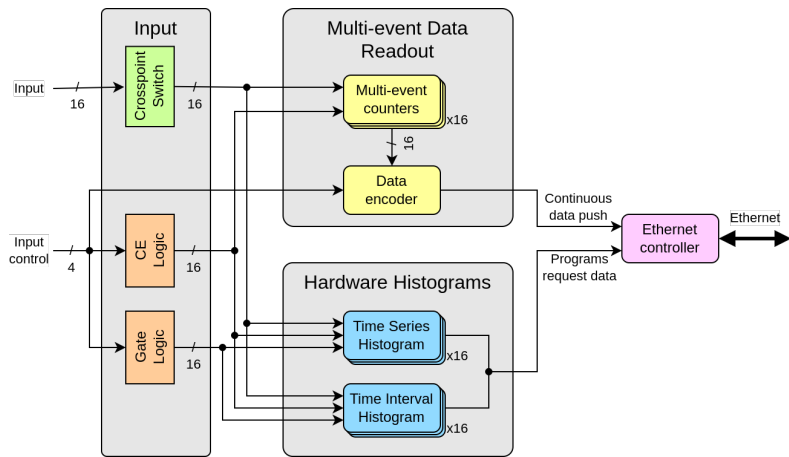


Figure 47: MSC16VE module.

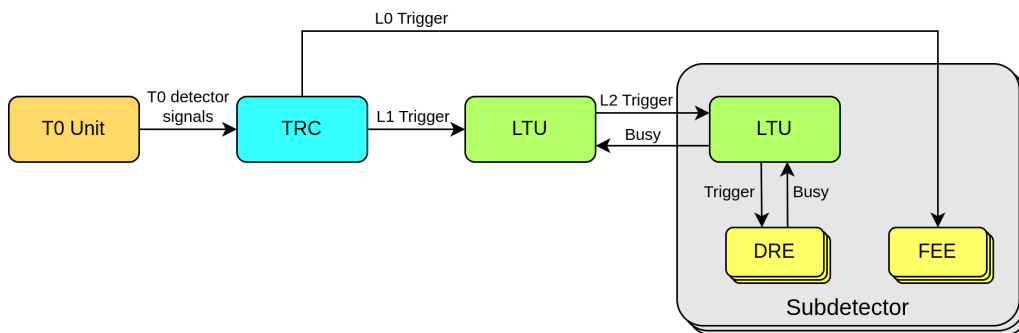


Figure 48: BM@N trigger architecture.

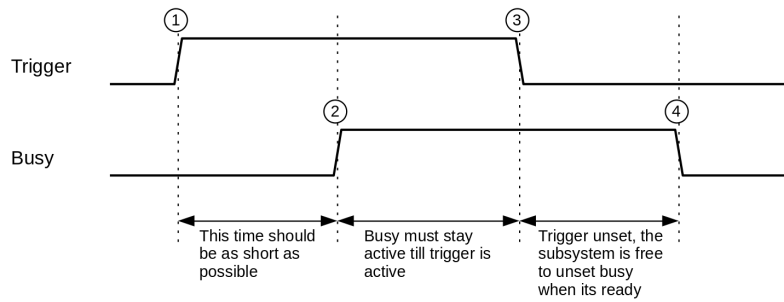


Figure 49: Trigger handshake chronogram.

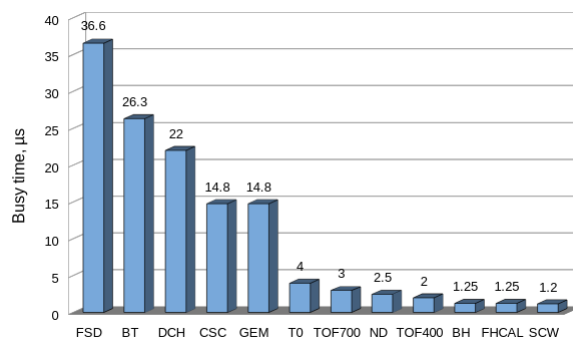


Figure 50: The average busy time for all subsystems.

13.5 DAQ data flow

All BM@N subdetectors except DCH use Ethernet to transfer data from readout electronics to First Level Processors. Primary FLP task is to receive data stream in real time, buffer, validate, format and enqueue data blocks to event building network. FLP decouples fast microsecond-scale synchronous data acquisition process from slower seconds-scale software data processing by buffering data in computer RAM. Data transfer path from readout electronic module to event building network and storage system is shown on Fig. 51 for typical 64-channel ADC based waveform digitizer module ADC64VE.

Electronic modules designed by DAQ team share common communication architecture. Network connectivity is provided by hardware IP stack (HWIP), a programmable logic code synthesized for onboard FPGA processor. Taking into account limited memory and logic resources of FPGA chips available, and implementation complexity of TCP protocol, custom data transfer protocol MStream has been designed for data streaming over 1 Gb/s or 10 Gb/s Ethernet networks. It uses UDP over IP as transport layer, and implements ordered and reliable data packet delivery using acknowledgments.

FLP receive data stream in real time. Dedicated servers with dual 18-core CPUs, equipped with dual 100 Gb/s Ethernet adaptors, are running Fedora-36 Linux OS. Tuning for real-time operation is necessary to ensure continuous data transferred without interruptions [18]. It includes CPU frequency and supply voltage management, network adapter interrupt coalescence mitigation and system task scheduler adjustments.

BM@N readout electronics deliver 6 GB/s of raw data over 200 streams in peak at 10 kHz trigger rate. Single data stream has 500 MB/s maximum sustained throughput when using 10 Gb/s Ethernet. Run 8 operation has shown that single manually tuned FLP server is capable of hosting 10-12 data stream receivers with minimal contribution to overall busy time.

Software event building in BM@N is part of asynchronous processing, it does not affect readout busy time under normal operation. Event builders are cascaded in multiple layers for load distribution, and last layer writes data files to storage system.

Event Builder programs associated with data intensive subdetectors run on dedicated hardware servers, while event builders for low data rate subdetectors run in KVM virtual environment, as well as readout control programs. It allows to utilise computer resources efficiently.

13.6 DAQ storage system

DAQ storage system is comprised of 10 servers with NVMe solid state devices for low latency I/O operations and 12 servers with hard disks for high volume storage. It is distributed software defined object storage cluster under control of Ceph software ([19]). Cluster management and interface functions are implemented on 6 dedicated single-CPU servers. Configurable ‘CRUSH map’ algorithm defines data object to storage device mapping. Ceph cluster has self recovery functions and it performs periodic data read check on regular intervals to ensure data integrity. It is highly available and reliable system with no single point of failure.

Storage devices are organised in pools with different data redundancy algorithms. Pools allocated on NVMe devices have triple replication provide 100 TB usable space, and are used as block storage for virtual machine cluster. Hard disk pool has 2.2 PB usable capacity. It use erasure coding replication with 40% overhead. POSIX compatible filesystem interface CephFS is used for experimental data storage. Server hardware characteristics are shown in Table 8.

Qty	Function	Specifications	Network
20	Compute node	Dual 18-core 3 GHz CPU, 384 GB RAM	Dual 100 Gb/s
10	NVMe storage server	10 × 3.5TB NVMe	Dual 100 Gb/s
8	HDD storage server 1	24 × 12TB HDD, 1.8TB SSD cache	Dual 100 Gb/s
4	HDD storage server 2	24 × 18TB HDD, 3TB SSD cache	Dual 100 Gb/s
6	Control server	4-core CPU, 64 GB RAM	Dual 25 Gb/s
1	Bootstrap server	4-core CPU, 16 GB RAM, 4 × 300GB HDD	Dual 1 Gb/s

Table 8: Characteristics of BMN DAQ server equipment.

13.7 Virtual computing cluster

Programs performing readout control functions, detector slow control, software and infrastructure monitoring and other services are run on KVM virtual machines or LXC containers that reside on

1044 highly available cluster. Approx. 100 virtual machines in total reside on 10 compute nodes. Cluster
 1045 has backup and snapshot rollback mechanisms that are necessary for safe software administration
 1046 and recovery in case of errors. Virtual cluster is also used as offline computing farm for batch and
 1047 interactive analysis when no data taking is in progress.

1048 13.8 BM@N DAQ IT Infrastructure

1049 DAQ server equipment is located in 4 racks in MDC (modular data center), Fig. 53 49 servers
 1050 occupy 81 units of rack space in total. Table ?? shows server types and functions.

1051 Virtual machine cluster is comprised of 10 compute nodes running Proxmox VE version 7
 1052 software. Other 10 compute nodes are dedicated servers for FLP and event builders and run
 1053 Fedora-36 OS. Storage servers run CentOS 8 Stream OS.

1054 Basic network infrastructure services (RADIUS, DHCP, DNS) are provided by virtual cluster
 1055 with redundancy. During cold startup, while virtual cluster is not yet ready, basic services are
 1056 provided by bootstrap server. By design DAQ system is not dependant on any external network
 1057 or software services and autonomous operation is possible.

1058 Core of data network is two-level Ethernet fabric with Clos architecture that has two switches
 1059 on spine level and multiple switches on leaf level Fig. 52. Ethernet VPN (EVPN) virtualisation
 1060 technology is used to allow flexible traffic management, high availability and efficient link utilisation.
 1061 Underlay network provide connectivity between fabric nodes, it is formed by leaf and spine
 1062 switches connected with L3 routed links, topology is managed by OSPF dynamic routing protocol.
 1063 Overlay network that carry user traffic is realised with MP-BGP protocol at control plane and
 1064 VXLAN encapsulation at data plane.

1065 DAQ network supports jumbo ethernet frames up to 9000 bytes to maximise throughput of
 1066 data transfer from readout electronics. Network supports Any-Source Multicast that is necessary
 1067 for automatic discovery of readout electronics modules and software components of distributed
 1068 DAQ system.

1069 Two spine and four leaf switches are located in racks of MDC. Other leaf switches and access
 1070 switches of slow control systems are located in electronics racks in experimental area. Two core
 1071 routers of DAQ technological network are located in building 201 and provide connectivity to
 1072 campus network with 200 Gb/s bandwidth.

1073 Compute and storage servers, readout electronics and additional level of 1 Gb/s access switches
 1074 for slow control systems are connected to fabric leaf switches. Critical components have dual
 1075 connections to pairs of leaf switches for high availability using LACP link aggregation protocol.

1076 DAQ network has shown no critical problems during BMN data taking Run 8. Ethernet switch-
 1077 ing fabric bandwidth is adequate for peak traffic conditions and has no negative impact on data
 1078 taking performance. No significant packet drops or errors were registered by monitoring system
 1079 on network fabric switches that could indicate network saturation and packet buffer overflows.
 1080 Considering both trigger rate and event size increase on next data taking run, it is possible to
 1081 double fabric bandwidth by additional leaf to spine connections.

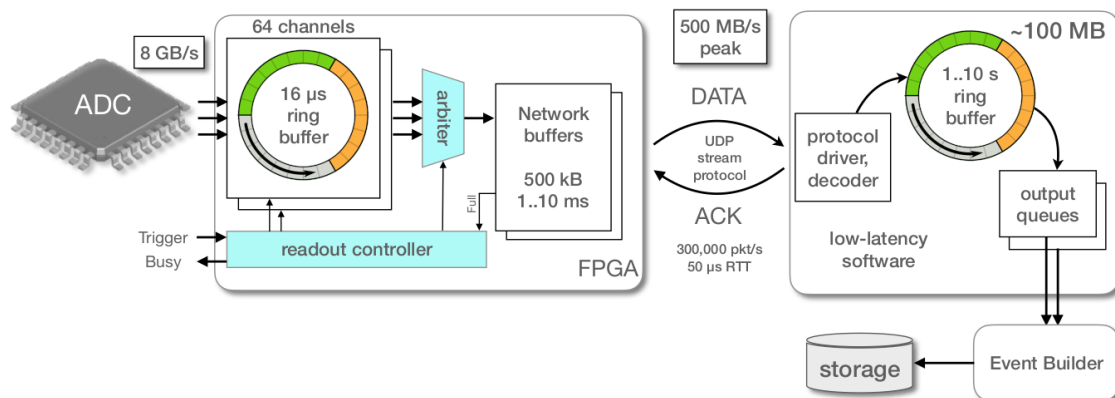


Figure 51: Data transfer from detector to storage system.

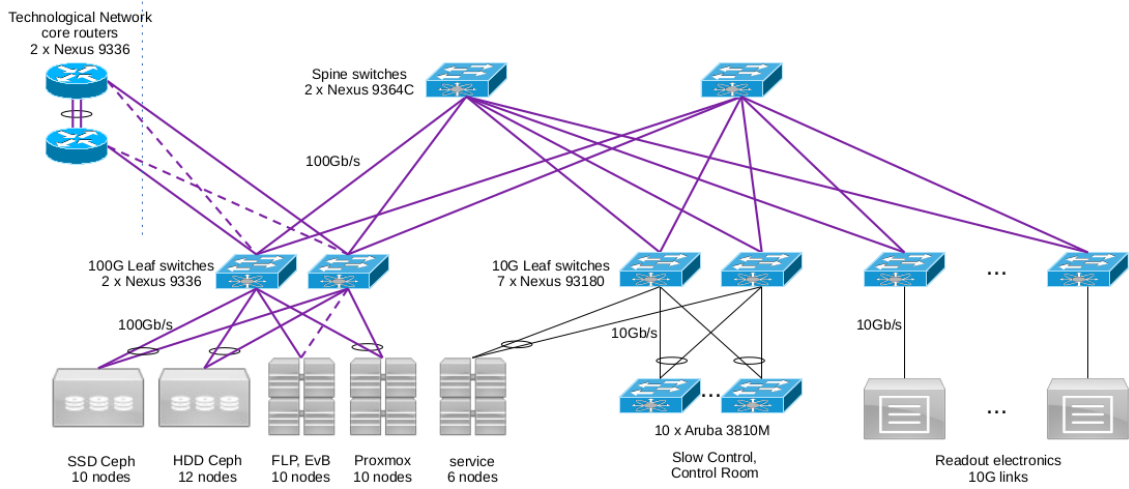


Figure 52: BMN DAQ Network.



Figure 53: BM@N Modular Data Center server racks.

1082 **14 Slow Control System**

1083 Main objectives of Slow Control System (SCS) include hardware status monitoring, archiving
 1084 the operational properties of the facility, user-friendly graphical interface and alarm management
 1085 system. The SCS was built around “TANGO Controls” [20] - an open-source toolkit, widely used
 1086 in scientific experiments.

1087 Slow Control data from experiment subdetectors such as: high voltage, low voltage, vacuum,
 1088 gas flow and mixture etc. are aggregated by SCS. Those are then stored in the “historical database”
 1089 - a PostgreSQL database with TimescaleDB extension [21]. It is implemented as distributed cluster
 1090 with backup and load balancing

1091 The user interface for live monitoring and retrieving past data is developed with Grafana [22]
 1092 – an open-source analytics and interactive visualization web application. A mnemonic scheme of
 1093 the experiment displaying hardware status and alarms (Fig. 54) was also implemented with it.

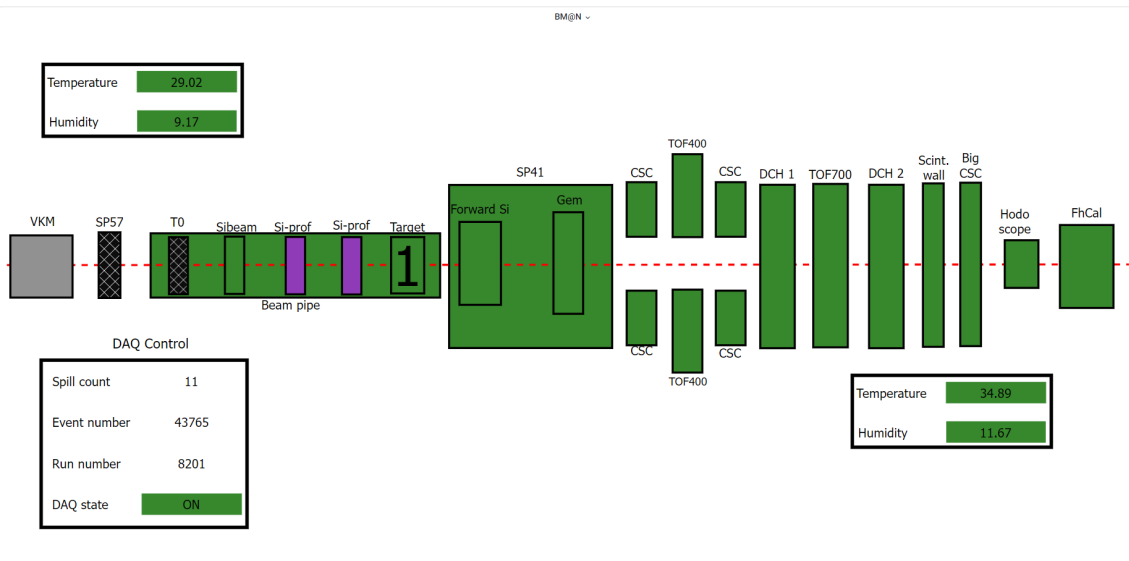


Figure 54: Slow Control System Main View.

1094 TANGO Database, hosting the configuration of the whole system, and TANGO Historical
 1095 Database are running on the BM@N virtual machine cluster. While programs, controlling and/or
 1096 monitoring real hardware are running either on virtual cluster or on dedicated PCs of different
 1097 subdetectors.

1098 **15 Summary**

1099 The detailed description of BM@N spectrometer is given. In this configuration t the fall of 2022 and
1100 the beginning of 2023 a big data set was recorded during 3 moths period. About 500M events with
1101 the different trigger condition are available for a physical analysis. A preliminary ananalysis of about
1102 1% of data shows a signals particles decays with strange quarks (K_S^0, Λ). The signature of charge
1103 pions, kaons and protons is visible if the time flight system TOF400/TOF700 is involved in the
1104 data analysis. The resolution in particle momentum, the width of the invariant mass distributions
1105 are in agreement with the expected values estimated by MC simulation. The BM@N collaboration
1106 acknowledges the efforts of the staff of the accelerator division of the Laboratory of High Energy
1107 Physics at JINR that made the data taking possible and successful. The BM@N collaboration
1108 acknowledges support

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