



Modelling polarized atomic beam source (PABS)

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Objective: Creating software for PABS modeling

Tasks:

1. Development of an atomic beam initial condition generator based on the Monte Carlo method.

- 2. Creation of a numerical model of a multipolar magnetic system
- 3. Modelling of radio frequency transition blocks

Polarized atomic beam source (PABS)











SPI dissociator f = 70 MHz



Multipolar magnetic system





$$1. \quad \frac{d^{2}\vec{r}^{1}}{dt^{2}} = \frac{1}{m}B_{0}\left(\frac{N}{2}-1\right)\frac{(\mu_{e}+\mu_{d})}{r_{0}^{\frac{N}{2}-1}}r^{\frac{N}{2}-2}$$

$$2. \quad \frac{d^{2}\vec{r}^{2}}{dt^{2}} = \frac{1}{2m}\left(\mu_{d}-\frac{-A_{d}\mu_{c}+\mu_{c}^{2}B}{\sqrt{9A_{d}^{2}-2A_{d}\mu_{c}B+\mu_{c}^{2}B^{2}}}\right)B_{0}\left(\frac{N}{2}-1\right)\frac{r^{\frac{N}{2}-2}}{r_{0}^{\frac{N}{2}-1}}$$

$$3. \quad \frac{d^{2}\vec{r}^{3}}{dt^{2}} = \frac{1}{2m}\left(-\mu_{d}-\frac{A_{d}\mu_{c}+\mu_{c}^{2}B}{\sqrt{9A_{d}^{2}+2A_{d}\mu_{c}B+\mu_{c}^{2}B^{2}}}\right)B_{0}\left(\frac{N}{2}-1\right)\frac{r^{\frac{N}{2}-2}}{r_{0}^{\frac{N}{2}-1}}$$

$$4. \quad \frac{d^{2}\vec{r}^{4}}{dt^{2}} = -\frac{1}{m}B_{0}\left(\frac{N}{2}-1\right)\frac{(\mu_{e}+\mu_{d})}{r_{0}^{\frac{N}{2}-1}}r^{\frac{N}{2}-2}$$

A sextuple magnet used in ABS. An atom flying into a magnet with r = 0 at an angle α_0 is shown on the left; several lines of force are shown on the right

$$5. \quad \frac{d^2 \vec{r}^5}{dt^2} = \frac{1}{2m} \left(-\mu_d + \frac{A_d \mu_c + \mu_c^2 B}{\sqrt{9A_d^2 + 2A_d \mu_c B + \mu_c^2 B^2}} \right) B_0 \left(\frac{N}{2} - 1 \right) \frac{r^{\frac{N}{2} - 2}}{r_0^{\frac{N}{2} - 1}}$$

$$6. \quad \frac{d^2 \vec{r}^6}{dt^2} = \frac{1}{2m} \left(\mu_d + \frac{-A_d \mu_c + \mu_c^2 B}{\sqrt{9A_d^2 - 2A_d \mu_c B + \mu_c^2 B^2}} \right) B_0 \left(\frac{N}{2} - 1 \right) \frac{r^{\frac{N}{2} - 2}}{r_0^{\frac{N}{2} - 1}}$$

5

Radio - frequency transition cells





Polarization of the gas target



Pz	P _{zz}	Multipolar magnetic system 1		MFT1	Multipolar magnetic system 2		MFT2	
		Before	After	After	Before	After	After	m _i
0	+1	1> 2> 3> 4> 5> 6>	1) 2) 3)	On $2 \leftrightarrow 4$ $ 1\rangle$ $ 3\rangle$ $ 4\rangle$	1) 3) 4)	1> 3>	Off 1> 3>	+1 -1
-2/3	0	1> 2> 3> 4> 5> 6>	1) 2) 3)	On 1> 2> 3>	1) 2) 3)	1> 2> 3>	Off $1 \leftrightarrow 4$ $ 2\rangle$ $ 3\rangle$ $ 4\rangle$	0 -1 -1



JINR

The atomic beam is defined by an event generator that produces a particle with the following parameters:

1. Particle coordinates (z, r)



2. The projection of the total atomic spin

The polarization of the particle is defined according to a uniform distribution, so that the initial atomic beam is unpolarized. 3. The velocity of the particle along the OZ axis, v_r , and the velocity along the Or axis, v_z



Modelling multipolar magnetic system

15

10

5

0

-5

-10

10

R, mm



Z, mm

Modelling multipolar magnetic system (SPI ABS)





- 1 the first three sextupole lenses,
- 2 the wall,
- 3 the sextupole lens

 $P_{+\frac{1}{2}} = (91.3 \pm 1.4)\%$ Intensity $= \frac{N_{end}}{N_{start}} * 100\%$

Intensity = $(0.36 \pm 0.04)\%$

(Modelling polarizer (PolFusion ABS)





Checking the performance of the polarizer simulation



	P _{z, meas.}	P _{zz, meas} .	P _{z, sim.}	P _{zz, sim.}
	$+0.88 \pm 0.01$	$+0.88 \pm 0.03$	$+0.89 \pm 0.03$	$+0.90 \pm 0.03$
	-0.91 ±0.01	$+0.85 \pm 0.2$	-0.91 ±0.03	$+0.89 \pm 0.03$
ANKE PABS	$+0.005 \pm 0.003$	$+0.90 \pm 0.02$	-0.06 ± 0.08	$+0.90 \pm 0.04$
	$+0.005\pm0.003$	-1.71 ± 0.03	-0.08 ± 0.03	-1.58 ± 0.07
HERMES PABS	$+0.92 \pm 0.01$	$+0.88 \pm 0.02$	+0.94 ±0.021	$+0.89 \pm 0.03$
	-0.91 ±0.01	$+0.94 \pm 0.02$	-0.92 ±0.011	$+0.95 \pm 0.01$
	-0.02 ± 0.01	$+0.99 \pm 0.02$	-0.05 ± 0.08	$+0.96 \pm 0.05$
	-0.02±0.01	-1.77 ±0.02	-0.03±0.02	-1.64 ±0.04

Choosing the optimal PABS design (PolFusion)



						-
	P _{z. theor}	P _{zz, theor}	P _{z, sim.}	P _{zz, sim.}	Intensity, %	
Design No1	0	+1	+0.06 ±0.08	+0.89 ±0.02	0.20 ±0.02	
(6666 66)	- 1/3	+1	-0.26 ±0.06	+0.92 ±0.03	0.21 ±0.02	
	-1	+1	-0.92 ±0.02	$+0.92 \pm 0.02$	0.16 ±0.01	7
	0	+1	-0.46±0.06	+0.86±0.04	0.13±0.01	_ ~2
Design N_{2}	- 1/3	+1	-0.63 ±0.05	$+0.94 \pm 0.03$	0.14 ± 0.01	
(0040 40)	-1	+1	-0.95±0.02	$+0.95\pm0.04$	0.14 ±0.01	
During Mr2	0	+1	-0.50 ± 0.05	$+0.86 \pm 0.05$	0.22 ± 0.01	
Design №3 (8888 88)	- 1/3	+1	-0.58 ± 0.07	+0.88±0.03	0.20±0.01	-
	-1	+1	-0.89±0.03	$+0.89\pm0.04$	0.21 ± 0.01	



PABS optimization based on nozzle temperature





Graph of the dependence of pressure in the compression tube on the nozzle temperature: a - in the range from 70 to 110 K, b - in the range from 0 to 310 K.









Assumptions

When calculating the passage through the magnet, the following assumptions were made:

1. There are no edge effects at the boundary of the magnet, meaning that the particles travel uniformly and in a straight line towards the magnet.

2. The magnet is infinitely tall.

3. The change in the velocity of the atomic beam along the Z-axis is negligible: $v_z = const.$

1. The intensity calculated during the simulation aligns very closely with the intensity measured in experimental setups.

2. The degree of polarization calculated during the simulation, taking into account the margin of error, falls within the range of experimental data.

3. The runtime complexity of the program is O(n).





Thank you for your attention!



pz p_{ZZ} (vector) (tensor) -2/3 0 0.5 m 0 +1-1/3 +1 -1 +1 -1/2 $\pm 1/2$ atomic beam d_{nozzle} = 2 mm **D**, 0.01 eV T_{nozzle} = 84 K $2 \cdot 10^{16}$ atoms/s RF_{power} = 300 W **Polarizing system:** Sextupoles + Quadrupoles + MFT + Sextupoles + MFT

























Сечение реакции

$$\begin{split} \sigma(\Theta, \Phi) &= \sigma_0(\Theta) \left\{ 1 + \frac{3}{2} \left[A_y^{(b)}(\Theta) p_y + A_y^{(t)} q_y \right] + \frac{1}{2} \left[A_{zz}^{(b)}(\Theta) p_{zz} + A_{zz}^{(t)}(\Theta) q_{zz} \right] \right. \\ &+ \frac{1}{6} \left[A_{xz}^{(b)}(\Theta) p_{xx-yy} + A_{xz-yy}^{(t)}(\Theta) q_{xx-yy} \right] \\ &+ \frac{2}{3} \left[A_{zz}^{(b)}(\Theta) p_{yx} + A_{xz}^{(t)}(\Theta) q_{xz} \right] \\ &+ \frac{9}{4} \left[C_{y,y}(\Theta) p_y q_y + C_{x,z}(\Theta) p_x q_x + C_{x,z}(\Theta) p_x q_z \\ &+ C_{z,x}(\Theta) p_z q_x + C_{z,z}(\Theta) p_z q_z \right] \\ &+ \frac{3}{4} \left[C_{y,zz}(\Theta) p_y q_{zz} + C_{zz,y}(\Theta) p_{zz} q_y \right] \\ &+ C_{y,zz}(\Theta) p_y q_{xz} + C_{z,yz}(\Theta) p_z q_{yz} + C_{yz,z}(\Theta) p_y q_z \\ &+ \frac{1}{4} \left[C_{y,xx-yy}(\Theta) p_y q_{xx-yy} + C_{xx-yy,y}(\Theta) p_{xx-yy} q_y \\ &+ C_{zz,zz}(\Theta) p_{zz} q_{xz} + C_{xz,zz}(\Theta) p_{xz} q_{zz} \right] \\ &+ \frac{1}{3} \left[C_{zz,xx-yy}(\Theta) p_{zz} q_{xx-yy} + C_{xx-yy,zz}(\Theta) p_{xx-yy} q_{zz} \right] \\ &+ \frac{3}{4} \left[C_{xy,yz}(\Theta) p_{xy} q_{yz} + C_{yz,xy}(\Theta) p_{yz} q_{yz} \right] \\ &+ \frac{3}{6} \left[C_{xy,yz}(\Theta) p_{xy} q_{xz} + C_{yz,xy}(\Theta) p_{yz} q_{xy} \right] \\ &+ \frac{3}{6} \left[C_{xy,yz}(\Theta) p_{xy} q_{yz} + C_{yz,xy}(\Theta) p_{yz} q_{xy} \right] \\ &+ \frac{1}{6} \left[C_{xz,xx-yy}(\Theta) p_{xz} q_{xx-yy} + C_{xx-yy,xz}(\Theta) p_{xx-yy} q_{xz} \right] \\ &+ \frac{1}{6} \left[C_{xz,xx-yy}(\Theta) p_{xy} q_{xy} + C_{xz-yy,xz}(\Theta) p_{xx-yy} q_{xz} \right] \\ &+ \frac{1}{36} \left[C_{xz,xy}(\Theta) p_{xy} q_{xy} + C_{xy,xy}(\Theta) p_{xx-yy} q_{xz-yy} \right] \\ &+ \frac{1}{2} \left[C_{x,xy}(\Theta) p_{xy} q_{xy} + C_{xy,x}(\Theta) p_{xy} q_{x} + C_{z,xy}(\Theta) p_{x} q_{xy} \right] \\ &+ \frac{1}{2} \left[C_{x,xy}(\Theta) p_{xy} q_{xy} + C_{xy,x}(\Theta) p_{xy} q_{xy} + C_{xy,x}(\Theta) p_{xy} q_{x} + C_{z,xy}(\Theta) p_{x} q_{xy} \right] \\ &+ \frac{1}{2} \left[C_{x,y}(\Theta) p_{x} q_{xy} + C_{xy,x}(\Theta) p_{xy} q_{x} + C_{z,xy}(\Theta) p_{x} q_{xy} + C_{xy,x}(\Theta) p_{xy} q_{x} + C_{x,xy}(\Theta) p_{xy} q_{x} + C_{xy,x}(\Theta) p_{xy} q_{x} + C_{xy,x$$

 $p_z(q_z), p_{zz}(q_{zz}) \neq 0$

$$\begin{split} \sigma(\Theta, \Phi) &= \sigma_0(\Theta) \left\{ 1 \quad + \quad \frac{3}{2} \left[A_{zz}^{(b)}(\Theta) p_{zz} + A_{zz}^{(t)}(\Theta) q_{zz} \right] \\ &+ \quad \frac{9}{4} C_{z,z}(\Theta) p_z q_z + \frac{1}{4} C_{zz,zz}(\Theta) p_{zz} q_{zz} \right\} \end{split}$$

$$\begin{aligned} (p_{i,j} \neq 0, \ q_{i,j} = 0): \\ \sigma(\Theta, \Phi) &= \sigma_0(\Theta) \ \cdot \ \{1 + 3/2 \ A_y(\Theta) \ p_y + 1/2 \ A_{xz}(\Theta) \ p_{xz} \\ &+ 1/6 \ A_{xx-yy}(\Theta) \ p_{xx-zz} \\ &+ 2/3 \ A_{zz}(\Theta) \ p_{zz} \} \end{aligned}$$



Астрофизика

- Big bang
- Hydrogen burning
- Helium burning
- Advanced burning
- (carbon/neon/oxyge n/silicon)
- s-process (neutron sources)
- p-process

Теория ядерного взаимодействия

- Широкий спектр моделей
- Сложности при описании прямых/непрямых измерений

Термоядерная энергетика

- Использованиее поляризованного топлива
- Увеличение сечения
- Управление угловым распределением вылета продуктов реакции
- Реакторы с малым выходом нейтронов

Прикладные аспекты

- Наработка трития и гелия-3
- ЗНеориентированная технология газоразрядных детекторов
- Источник нейтронов для наработки медицинских изотопов 100Mo(n,2n)99Mo



Big Bang нуклеосинтез — Первичное распределение изотопов D/H



Вклад ошибки в первичное распределение

Global BBN Analysis: Tsung-Han Yeh, Keith Olive, Brian Fields (2021)

Anton Rozhdestvenskij





Ofelia Pisanti, Gianpiero Mangano, Gennaro Miele, and Pierpaolo Mazzella Primordial Deuterium after LUNA: concordances and error budget (2020) Отношения сечений процессов d(d, n)³Не к d(d, p)³Н из экспериментов (точки) и теории (сплошная линия).

Необходимы новые измерения сечения реакции неполяризованного dd-синтеза по обоим каналам!

Теоретическое предсказание:

K. Arai, S. Aoyama, Y. Suzuki, P. Descouvemont, and D. Baye Phys. Rev. Lett. 107, 132502 (2011)

Э Термоядерный синтез и прикладные аспекты

- Увеличение сечения реакции
- Контроль над направлением разлета продуктов реакции
- Подавление нейтронного канала



Exp.: Ch. Leemann et al., Helv. Phys. Acta **44**, 141 (1971) Theor.: G. Hupin et al. Nature Com. **10**, 321 (2019)

Распределения источников нейтронов в координатах (R, Z) для (а) неполяризованного случая и (б) случая полной параллельной поляризации.



W.Yang, G.Li, X.Gong, X.Gao, X.Li, H.Li... Effect of the Fusion Fuels' Polarization on Neutron Wall Loading Distribution in CFETR (2021) https://doi.org/10.1080/15361055.2021.1969064 (China Fusion Engineering Test Reactor (CFETR))