



Politechnika Wroclawska

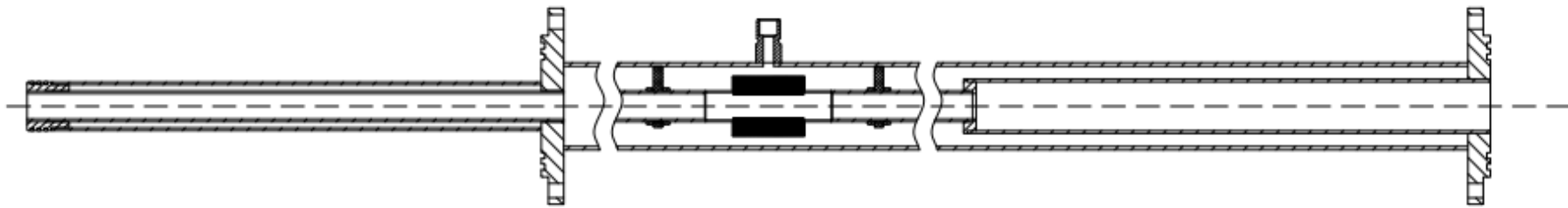
**MODELS OF CONTINUUM
DAMAGE MECHANICS
APPLICABLE IN CRYOGENIC
CONDITIONS**

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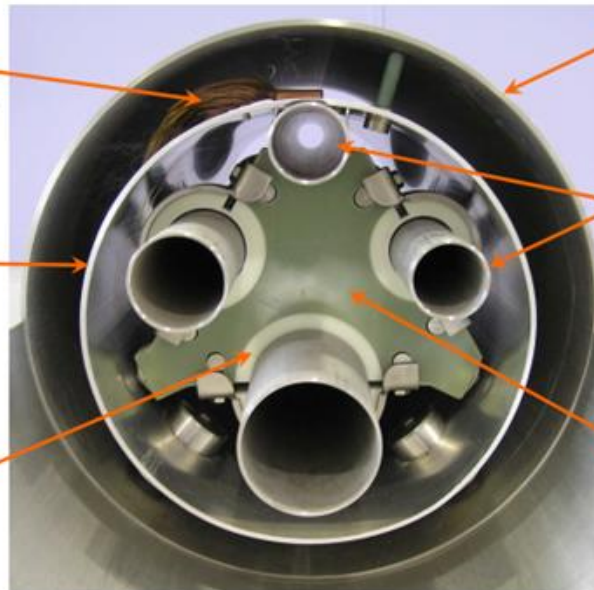
CONTINUUM DAMAGE MECHANICS



Thermal bridge
between radiation
shield and
80 K process pipe
(Copper)

Radiation shield
(Aluminium alloy
Al6060)

Spacer
(Glassboard)



Vacuum vessel
(Austenitic Stainless
steel 304, 1.4301)

Process pipes
(Austenitic Stainless
steel 304L, 1.4306)

Sliding support
(Epoxy G-10)



CONTINUUM DAMAGE MECHANICS

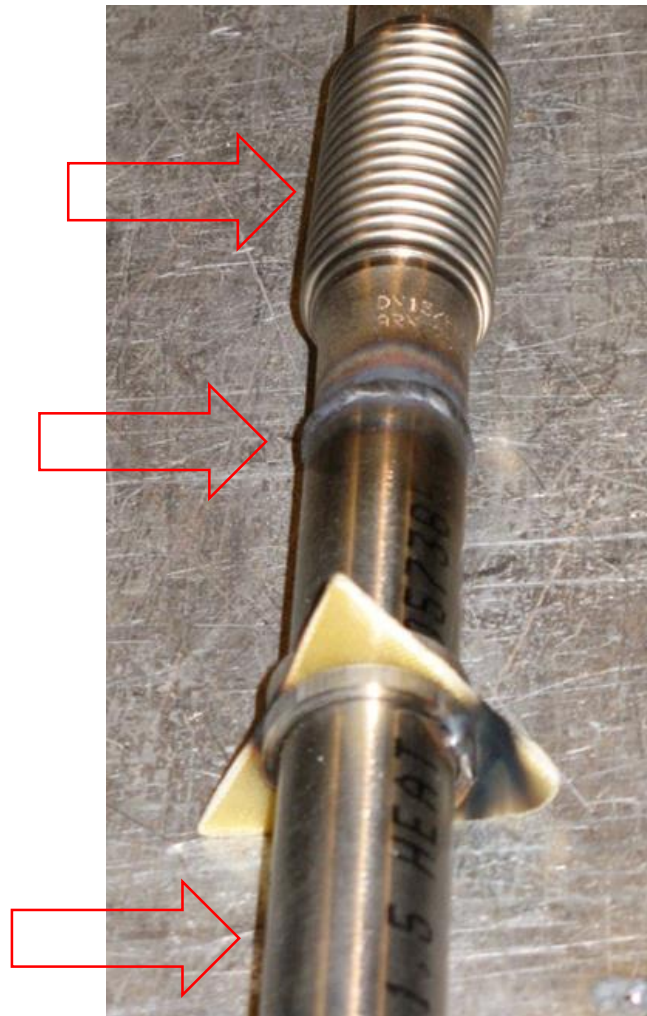
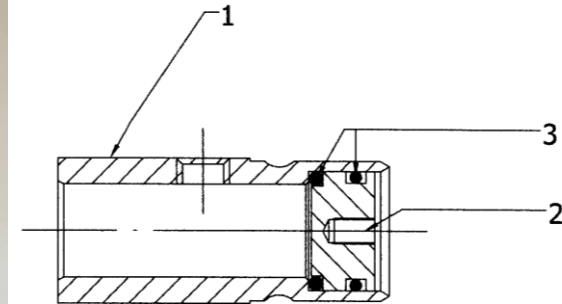
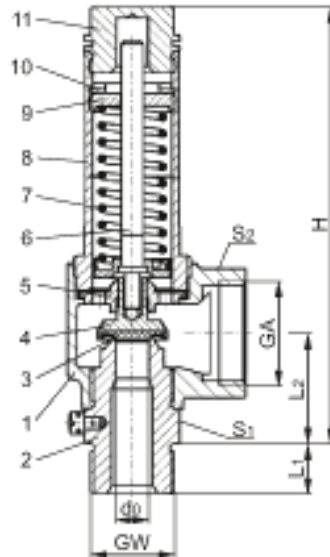


Table 1. Probabilities of defect occurrence (failure rates) of the most common defects

Defect	Failure rate	Source
Cold weld rupture	$2.53 \cdot 10^{-7} \text{ m}^{-1} \cdot \text{year}^{-1}$	1
Cold pipe leakage	$4.61 \cdot 10^{-6} \text{ m}^{-1} \cdot \text{year}^{-1}$	2
Cold pipe rupture	$4.54 \cdot 10^{-7} \text{ m}^{-1} \cdot \text{year}^{-1}$	2
Cold bellows rupture	$8.76 \cdot 10^{-5} \text{ year}^{-1}$	3
Vacuum jacket rupture	$8.77 \cdot 10^{-3} \text{ year}^{-1}$	4
Capillary break	$2.0 \cdot 10^{-8} \text{ year}^{-1}$	5

CONTINUUM DAMAGE MECHANICS

Dobór zaworów bezpieczeństwa



EN ISO 4126-1:2007 Safety devices for protection against excessive pressure - Part 1: Safety valves

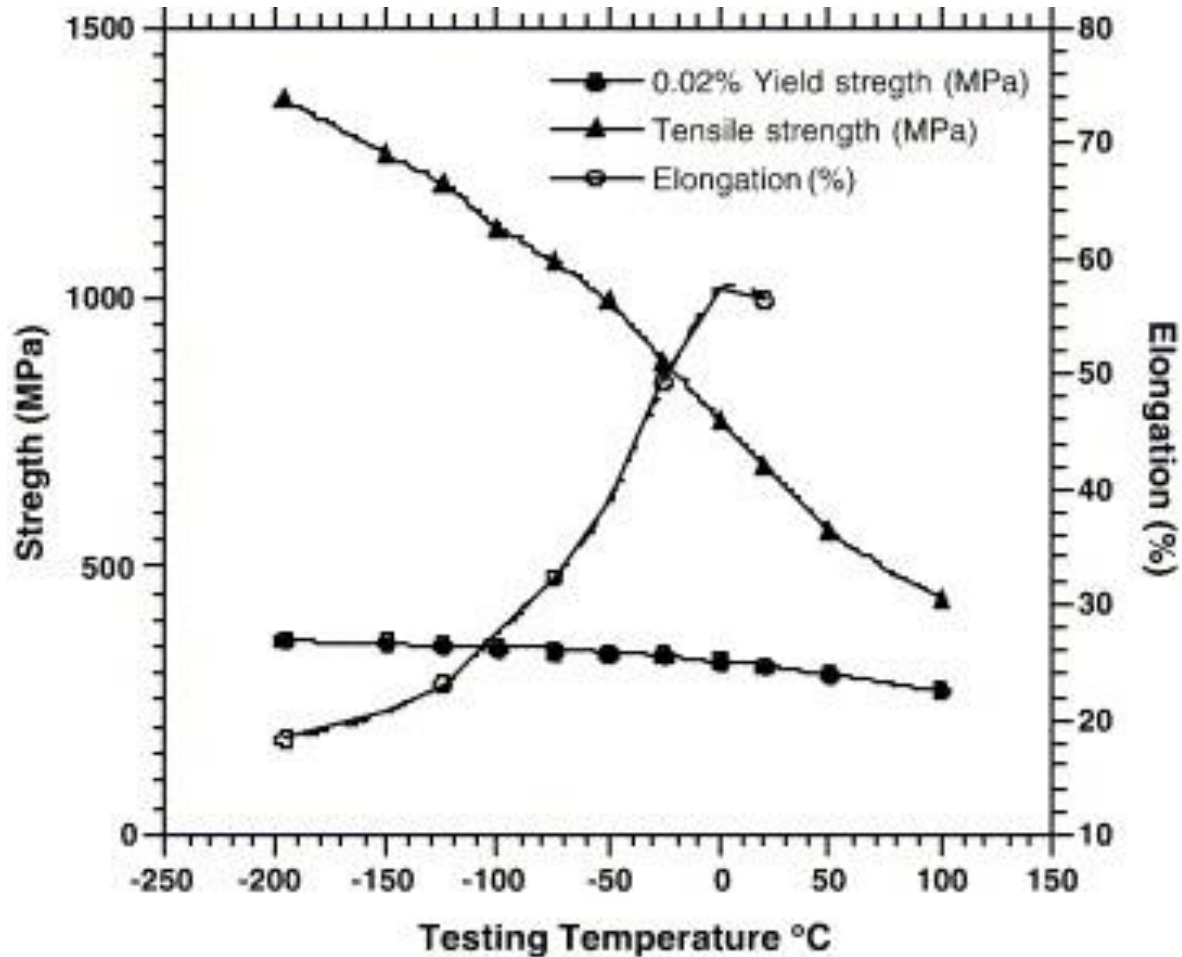
$$\dot{m} = 0.2883 \cdot C \cdot K_{dr} \cdot K_b \cdot \sqrt{\frac{p_0}{v}}$$

$$C = 3.984 \sqrt{\kappa \left(\frac{2}{\kappa + 1} \right)^{\frac{\kappa + 1}{\kappa - 1}}}$$

$$K_b = \sqrt{\frac{\frac{2\kappa}{\kappa - 1} \left[\left(\frac{p_b}{p_0} \right)^{2/\kappa} - \left(\frac{p_b}{p_0} \right)^{(k+1)/k} \right]}{\kappa \left(\frac{2}{\kappa + 1} \right)^{(k+1)/(k-1)}}$$



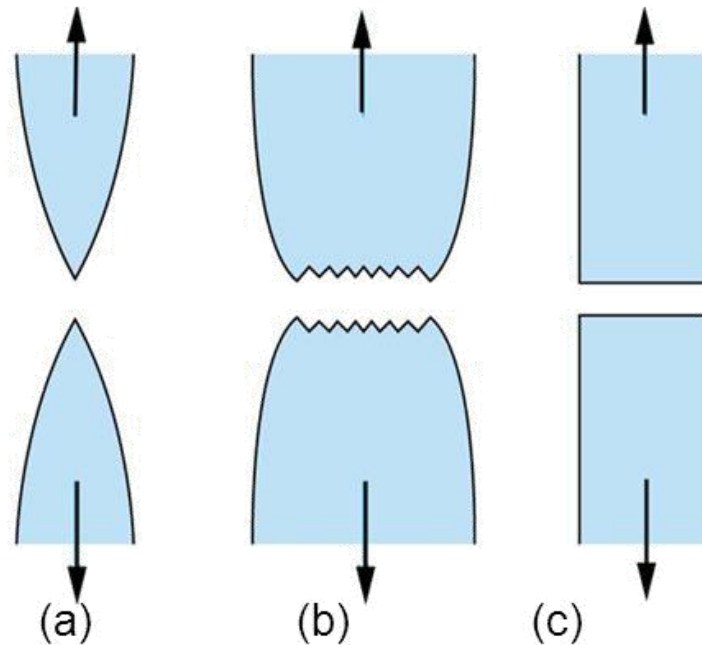
CONTINUUM DAMAGE MECHANICS





CONTINUUM DAMAGE MECHANICS

Continuum Damage Mechanics (CDM) falls within the group of inelastic materials, and deals with materials that undergo structural weakening as a result of microcrack formation (brittle damage) or of void growth and coalescence (ductile damage)

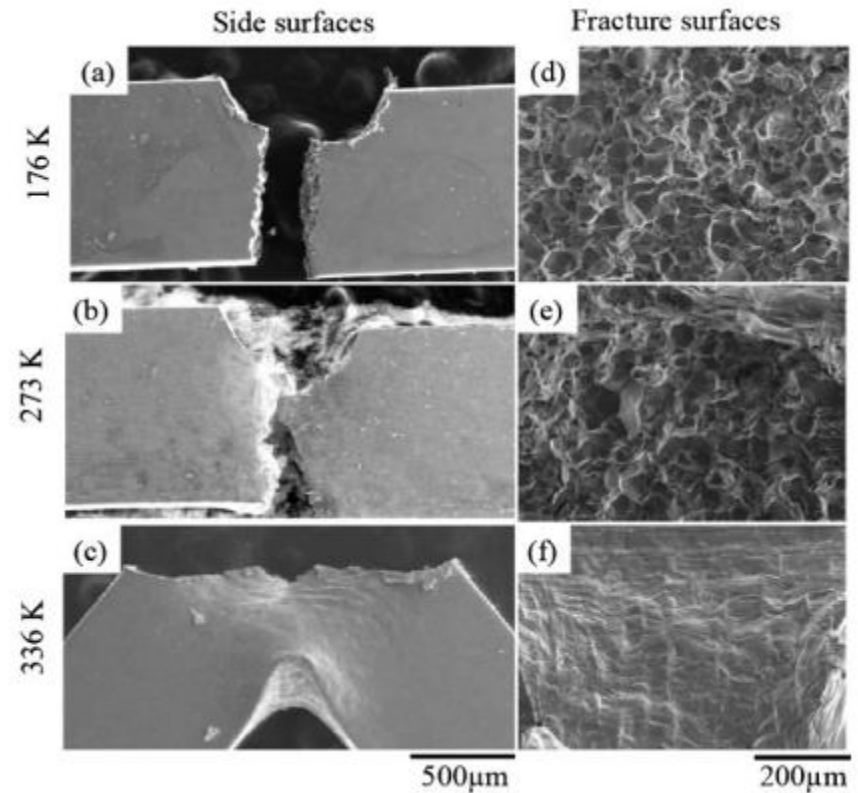
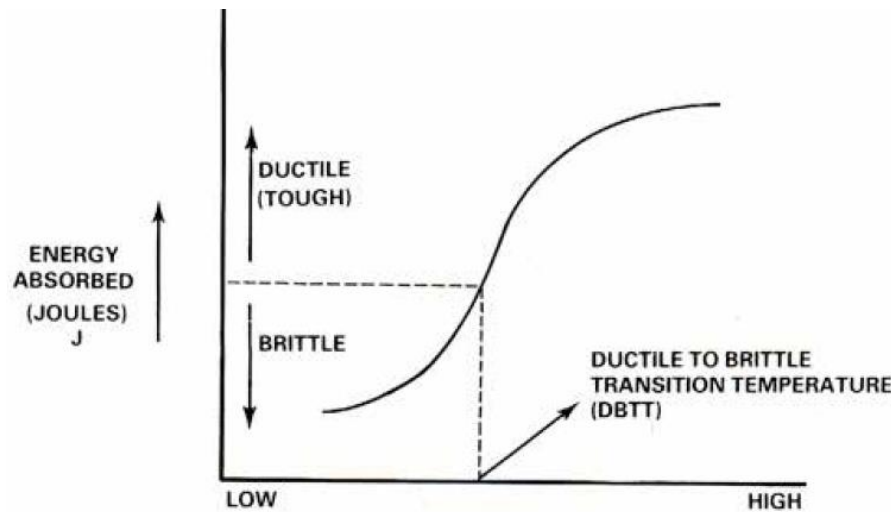


Ductile:
warning before
fracture

Brittle:
No
warning



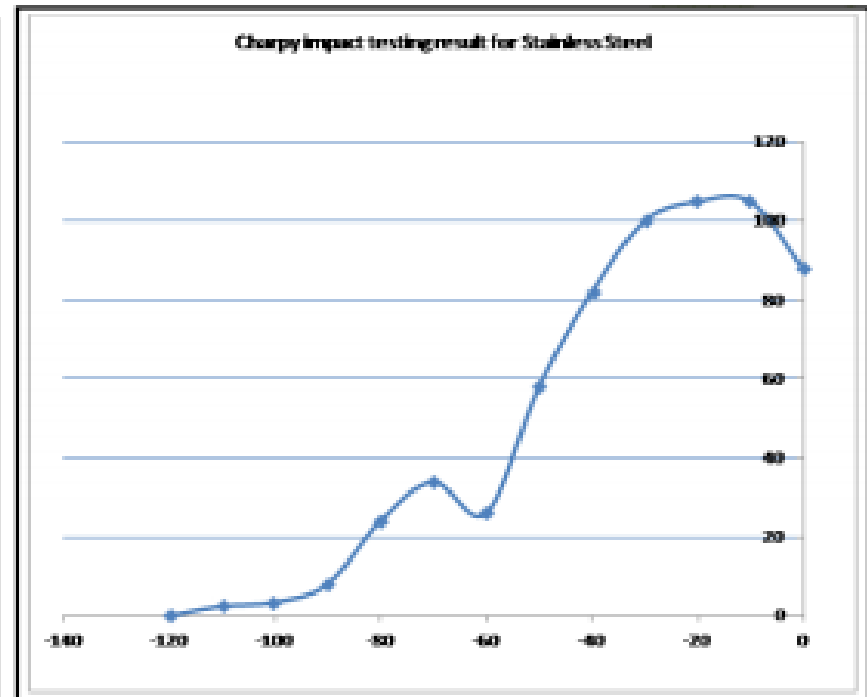
CONTINUUM DAMAGE MECHANICS





CONTINUUM DAMAGE MECHANICS

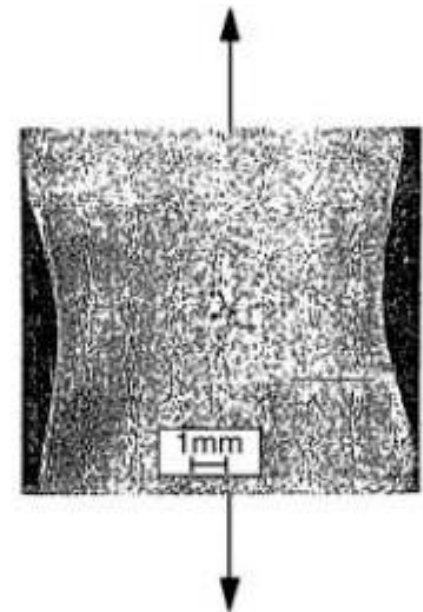
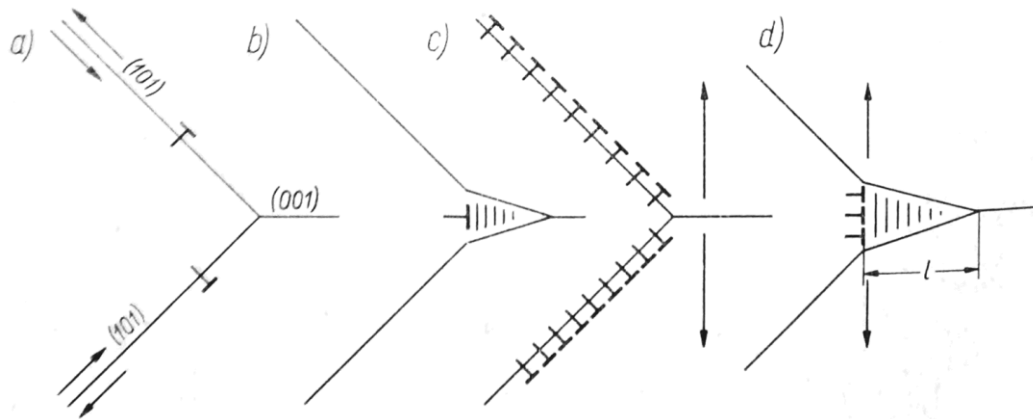
Sr. No	Temperature (In °C)	Energy absorb by specimen (in joule)
1	-120	-
2	-110	2.5
3	-100	3.5
4	-90	8
5	-80	24
6	-70	34
7	-60	26
8	-50	58
9	-40	82
10	-30	100
11	-20	105
12	-10	105
13	0	88



CONTINUUM DAMAGE MECHANICS

Reducing the strength of the material with respect to the theoretical strength is linked with the presence - in fact unavoidable - two types of defects:

1. Geometrical stress concentrators - sharp gaps and notches
2. Stress concentrators in the form of dislocations



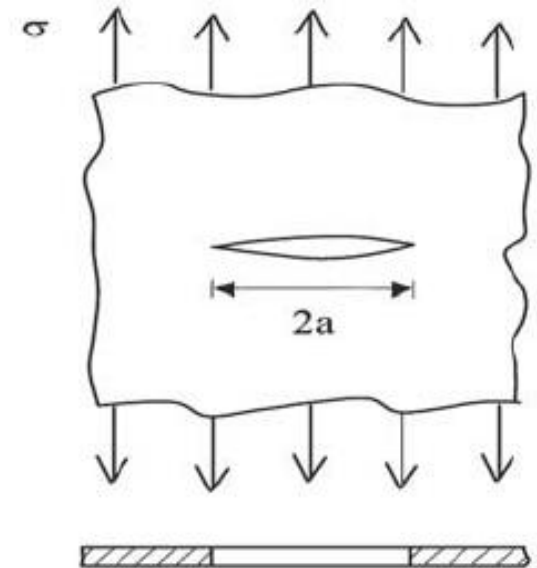
CONTINUUM DAMAGE MECHANICS

Griffith Theory of Brittle Fracture

- The critical stress required for crack propagation in a brittle material is given by:

$$\sigma_c = \left(\frac{2E\gamma_s}{\pi a} \right)^{1/2}$$

- - E = modulus of elasticity
 - γ_s = specific surface energy
 - a = half the length of an internal crack
- Applies only in cases where there is no plastic deformation present.





CONTINUUM DAMAGE MECHANICS

Verification other mathematical models eg:

- Irwin Model
- Dugdale-Barenblatt Model
- Czerepanow Model
- Orowan Model
-

Or using a proper numerical analysis (uncoupled/coupled) for cryogenics temperatures (correction factors for material data?)



CONTINUUM DAMAGE MECHANICS

THANK YOU