# Magnetic calculations of the SPD detector solenoid 

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## Basic conditions

- Software - TELMA
> Number of detector coils - 3
- 150 turns in the central coil and 300 turns in the side coils
(+30 in latest version)
- Magnetic core material - Steel 3
- Current 5200 A


## General view of a magnet with power lines



The longitudinal component of the field on the axis


## Radial integral

Coils turns 300-150-300

The integral is calculated using the formula from the current $Z$ to $Z=100$ cm at different radii r

$$
\text { Int }=\left\{\left|\int_{z}^{100} \frac{B r(r, z)}{B z(r, z)} d z\right|\right\}
$$



## Improving uniformity with correction coils

## Aim of the work:

Find the configuration of additional correction coils on the edge of the main superconducting coil to improve the homogeneity of the longitudinal field component Bz on the axis and radius of 1 m of the solenoid. It is necessary to provide homogeneity of Bz not worse than $7-8 \%$ in the region $\mathrm{Z}=0-140 \mathrm{~cm}$ and $\mathrm{R}=0-100 \mathrm{~cm}$.

## Boundary conditions:

- Additional superconducting correction coils should have two layers.
- The correction coils cannot be located in the area between the main superconducting coils and the closing vertical magnetic core and go beyond the dimensions of the main coils.
- It is necessary to minimize the number of layers along the radius to simplify the design of the cryostat.
- The current in the main coils is equal to the current in the correction coils.


## Improving uniformity with correction coils



Table 1. Setting options for the case with two correction coils

|  | Coil B | Coil C |
| :--- | :--- | :--- |
| 1 | 2 layers of 60 turns | 2 layers of 60 turns |
| 2 | 2 layers of 20 turns | 2 layers of 50 turns |
| 3 | 2 layers of 50 turns | 2 layers of 50 turns |
| 4 | 2 layers of 40 turns | 2 layers of 40 turns |

Improving uniformity with correction coils


Figure 1. Distribution of $B z$ in the $Y Z$ section at $x=0$ for a $65 \times 2$ coil

Improving uniformity with correction coils


Figure 2: Graph of $B z(z)$ for a $65 \times 2$ coil

Improving uniformity with correction coils

Table 2. Maximum deviations of $B z(z)$ values from $B z(0)$ in \%

|  | $\mathbf{Y}=0$ | $\mathbf{Y}=0.5$ | $\mathrm{Y}=1$ |
| :---: | :---: | :---: | :---: |
| $65 \times 2$ | 12.2 | 10.8 | 3.74 |
| $60 \times 2+60 \times 2$ | 5.67 | 2.87 | 13.7 |
| $20 \times 2+50 \times 2$ | 9.7 | 8 | 3.94 |
| $50 \times 2+50 \times 2$ | 6.63 | 4.22 | 10.1 |
| $40 \times 2+40 \times 2$ | 8.25 | 6.31 | 5.77 |
| $80 \times 2+30 \times 2+30 \times 2$ | 3.87 | 3.38 | 15.8 |

## Improve uniformity by turning off the center coil

Turning off the central coil to reduce its contribution to the central region of the solenoid is considered as a potential option for improving field uniformity without the use of correction coils.

Despite the fact that the uniformity improves somewhat (up to $10 \%$ ), its value is still insufficient.

A significant disadvantage of this method of uniformity improvement is the reduction of the solenoid field and, as a consequence, the need to increase the current from 5200 A to 6500 A. In this case, the critical current of the superconductor does not have the necessary reserve at this field.

## Forces acting on doors and coils

| Magnetic force, air gap 1 mm before endcaps, $\mathbf{N}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | comp.Barrel <br> top <br> sector <br> (half <br> along Z) | Barrel top <br> sector | Endcaps <br> (half) | Endcaps | Center <br> coil (top <br> sector <br> $1 / 8)$ | Side coil <br> (top <br> sector <br> $1 / 8)$ |  |
|  | X (horiz.) | 0 | 0 | -12.4 | 0 | 0 | 0 |
| F, kN | Y (vert.) | -143.8 | -287.6 | 0 | 0 | 658.9 | 1185.9 |
|  | Z (long.) | 67.5 | 0 | -694.1 | -1700 | 0 | -594.1 |

## Forces acting on the barrel



Calculation of magnetic forces acting on the door. The grid step is 0.1 m.

The figure shows a map of the distribution of magnetic forces acting on one of the doors (end cap).

The force values were calculated for the centers of the corresponding $0.1 \times 0.1 \mathrm{~m}$ grid elements and are shown in color ranges of 200 N each.


# Calculation of magnetic forces distribution along endcup and barrel 

The magnetic forces acting on endcap plates had been calculated.

The magnetic forces acting on barrel plates are in process of calculation.

## Calculation of magnetic forces acting on the coils during displacement

Magnetic force on coils

|  | comp. | Left coil | Central coil | Right coil |
| :---: | :---: | :---: | :---: | :---: |
| F, kN | X (horiz.) | 0 | 0 | 0 |
|  | Y (vert.) | 0 | 0 | 0 |
|  | Z (long.) | 4748.0 | 0 | -4748.0 |
|  | X (horiz.) | 0 | 0 | 0 |
|  | Y (vert.) | 0 | 0 | 0 |
|  | Z (long.) | 4521.4 | -69.6 | -4743.4 |
|  | X (horiz.) | 0 | 0 | 0 |

In the latest STEP model, the number of turns was increased by $301+12$ in the side coils and +6 in the central one). Current reduced from 5200 A to 5000 A.

The difference between the distribution of the Bz component along $Z$ with a 5 mm barrel-endcap gap and without a gap


## Comparison of the distribution of the Bz component along $Z$ with a coil shift of 5 mm and without shift



## Comparison of the distribution of the Bz component along $Z$ with a shift of the coils and without a shift



## Comparison of the distribution of the Bz component along $Z$ with a shift of the coils and without a shift



## Comparison of the distribution of the Bz component along $Z$ with a shift of the coils and without a shift



## Thank you for attention

